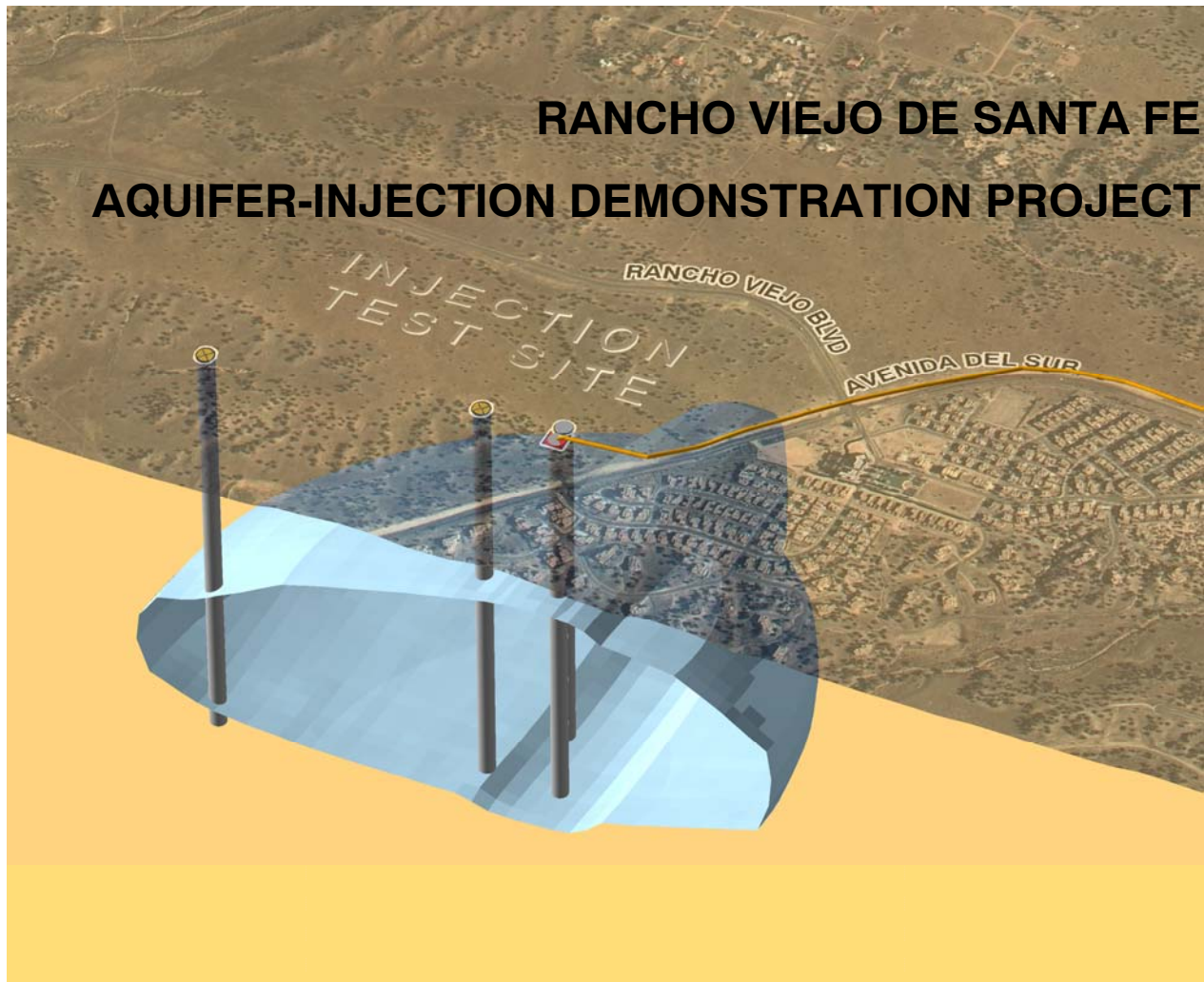
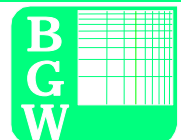


Prepared for:
RANCHO VIEJO DE SANTA FE, INC.
55 Cañada del Rancho
Santa Fe, NM 87508



OCTOBER 2007

BALLEAU GROUNDWATER, INC.
901 Rio Grande Blvd. NW, Suite F-242
Albuquerque, New Mexico 87104
(505) 247-2000



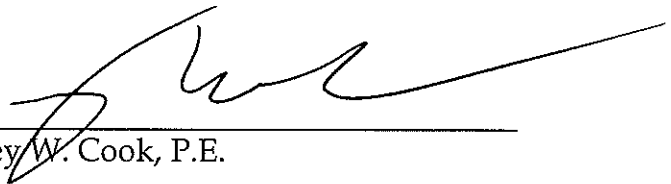
Prepared for:
RANCHO VIEJO DE SANTA FE, INC.
55 Cañada del Rancho
Santa Fe, NM 87508

**RANCHO VIEJO DE SANTA FE
AQUIFER-INJECTION DEMONSTRATION PROJECT**

BALLEAU GROUNDWATER, INC.
901 Rio Grande Blvd. NW, Suite F-242
Albuquerque, New Mexico 87104
(505) 247-2000

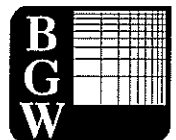


Steven E. Silver



Casey W. Cook, P.E.

Date 11/6/07



**RANCHO VIEJO DE SANTA FE
AQUIFER-INJECTION DEMONSTRATION PROJECT**

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RANCHO VIEJO DE SANTA FE
AQUIFER-INJECTION DEMONSTRATION PROJECT

SUMMARY

Rancho Viejo de Santa Fe, Inc. in cooperation with Governor Richardson's Water Innovation Fund, undertook an injection demonstration project in years 2006 and 2007. The project purpose was to demonstrate feasibility of long-term injection of water to the Tesuque Formation through a well.

An injection well and three observation wells were drilled into the Tesuque aquifer in 2006 for the project. Pilot Observation Well A penetrated the basal Bishops Lodge Member of the Tesuque Formation at 1,800 feet. Geophysical logs and cuttings from the four new wells and from an exploratory well drilled in 2001 one-mile east show a regional westward dip of geologic bedding and that a persistent 150-foot-thick clay lies below the water table across the test site. The Community College District pumping well drilled in 2002 is screened below the clay in Tesuque beds correlative with injection and observation wells.

Individual pumping tests of injection and observation wells indicate a non-radial flow response consistent with flow in stacked ribbon-like sand channels bounded by low-permeability deposits. Testing at the pumping well in 2002 indicates near-radial flow with close-in boundaries.

For the injection demonstration, the pumping well was equipped with a pump, control valves, and a flow meter. A three-inch pipeline was installed to convey water one mile west to the injection site. The injection well was equipped with a flow meter,

control valves and a restricting orifice set about 30 feet below static water level to retain-positive pressures in the drop pipe. The pumping and injection wells and eight observation wells and well nests were monitored for response during the test. Wells and piping were sanitized and flushed clean prior to injection. Water quality of the pumping and injection sites are of similar chemistry.

The injection demonstration started on August 29, 2006 and ended on February 27, 2007. Groundwater was extracted at the pumping well and injected at the injection well at an average rate of 50 gallons per minute, a total of about 39 acre feet. Drawdown at the pumping well was 67 feet at the end of the six months. At the injection site, water level buildup in the semi-confined injection zone ranged 85 feet at the injection well to 11 feet at the 2000-foot distant Observation Well C. No aquifer response was seen at water table monitoring points. About one-third of available capacity in the injection well was utilized for the six-month test. After shutdown, water-level recovery was monitored for six months.

The areal influence of six-month injection pressure build-up of about one foot extends to two miles in Tesuque Formation aquifer material consisting of channel sand deposits partially compartmentalized by geologic barrier structures.

The six-month test and six-month recovery response is analyzed with a generalized radial flow calculation and a numeric model. The generalized radial flow calculation utilizes a flow dimension to represent aquifer heterogeneity, variable geometry or boundaries, allowing for substantial geometric deviation from the Theis assumption of two-dimensional radial flow.

Generalized radial flow analysis of injection site buildup and recovery yield a low-flow dimension ($n = 1.1$ to 1.3) compatible with an aquifer composed of stacked linear channel sands bounded by fine-grained over-bank deposits. At the pumping site

the flow dimension indicates nearly radial flow ($n = 1.7$ to 1.8) with close-in boundaries likely to be mapped faults east and west of the pumping wells.

The numeric model incorporates ribbon-like sand channel features and fault boundaries to simulate the aquifer system with more spatial detail than available in the generalized radial flow calculation. The model simulates the observed head response, confirming that the understanding of the aquifer is reasonable. The model is suitable to adapt for simulating effects of future injection projects that may become of interest to water planners in Santa Fe County.

The injection well and Tesuque aquifer at the test site is capable of accepting 150 gallons per minute (240 acre feet per year) for an extended period with no adverse effects to well efficiency or aquifer performance.

INTRODUCTION

Rancho Viejo de Santa Fe, Inc. manages water and sewerage operations at a major housing area in the Community College District (CCD) south of Richards Avenue in Santa Fe County, New Mexico. On April 25, 2005, Rancho Viejo authorized Balleau Groundwater, Inc. to provide hydrologic support for an aquifer-injection demonstration project. The purpose of the project was to demonstrate the feasibility of injecting water for an extended period into the Tesuque Formation aquifer through a well. Governor Richardson's Water Innovation Fund contributed part of the funding. The project entailed drilling and constructing an injection well and three observation well/piezometer nests, testing short-term performance of each well, followed by pumping and injecting groundwater for six months with water-level monitoring in ten test and observation wells, and analyzing water-level response with a generalized radial flow (GRF) calculation and a numerical groundwater flow model. This report describes each of these tasks and provides conclusions on the feasibility of injecting water as demonstrated and on the hydrologic nature of the Tesuque Formation aquifer in the demonstration area of response.

The project was approved by New Mexico Office of the State Engineer and Santa Fe County for pumping at CCD production well (CCD-P1) and by New Mexico Environment Department for injecting groundwater into injection well (CCD-I1). Agency approval documents are attached as Appendix A.

HYDROGEOLOGIC SETTING

The study site is located south of the City of Santa Fe in the CCD of Santa Fe County, New Mexico (Figure 1). The site overlies part of the Santa Fe embayment of the Española structural geologic basin, a shallow, transitional basin between the deeper San Luis Basin to the north and Albuquerque-Belen Basin to the south. The basins are part of the Rio Grande Rift. General geology of the study site and surrounding area is shown in Figure 2.

Numerous studies have been made of the structure and stratigraphy of the Española Basin near Santa Fe (Spiegel and Baldwin, 1963; Kelley, 1978; Hearne, 1985; Koning and Hallett, 2001; Phillips and Grauch, 2004). The major basin-fill unit at the study site is the Tertiary Santa Fe Group, consisting of the Ancha and Tesuque Formations.

The Miocene- to Pliocene-age Tesuque Formation consists of unconsolidated to semi-consolidated sands, silts, clays and minor gravels derived from the Sangre de Cristo Mountains to the east (Spiegel and Baldwin, 1963). Transport and deposition of Tesuque sediments was generally by west-flowing fluvial systems draining to the Rio Grande, but sediment transport at the study site is thought to have been by north-flowing drainages (personal communication, J. Hawley to C. Cook, 2006).

Groundwater below the study site is stored in and moves through sand and gravel beds enclosed in silt and clay of the Tesuque Formation. Thickness of the Tesuque Formation is up to several thousand feet. About 1,600 feet of Tesuque thickness at the injection site was characterized by drilling and logging pilot well CCD-OWA. The Tesuque Formation is overlain by about 200 feet of unsaturated Ancha Formation. The Tesuque Formation forms a wedge in the Santa Fe area that thickens

north of the site and pinches out to the south (Koning and Hallett, 2001). Figure 3 shows the elevation of the base of the Tesuque Formation overlying pre-Santa Fe Group formations (Espinaso Formation below the study site) from aeromagnetic data.

Water-level elevations are shown in Figure 4 based on regional water-level data contoured for this study. Groundwater flow below the site is generally west or southwestward from mountain-front recharge at the foot of the Sangre de Cristos to discharge points at La Cienega Springs and the Santa Fe River. Depth to water ranges 250 to 300 feet across the test site. The hydraulic gradient across the site is about 100 feet/mile. Tesuque Formation hydraulic conductivity (K) can range from a few tenths to several feet per day, but the characteristic average range north of Santa Fe is 0.5 to 2 feet/day (Hearne, 1985). Local geologic controls on groundwater flow include depositional pinchout of channel sands, flow across dipping beds, and faults mapped west and east of the pumping well (Figure 2).

DRILLING AND TESTING

An injection well (CCD-I1) and three observation wells (Observation Well A (CCD-OWA), Observation Well B (CCD-OWB) and Observation Well C (CCD-OWC)) were drilled from January to May 2006 by Rodgers and Co. Inc. for the injection demonstration project. Well locations are shown on Figure 1. Table 1 summarizes well construction for injection, production and outlying monitor-well sites. Figure 5 presents a well cross-sectional diagram. Well completion reports (BGW 2007a, b, c, d) document well drilling, construction and testing. An overview of drilling and testing the four injection-test wells, as well as the CCD pumping and exploratory wells drilled in years 2001 and 2002, is provided below.

In the period 2001 to 2002, Layne Western drilled a pilot exploratory well (CCD-X1) and a pumping well (CCD-P1) for Rancho Viejo about one mile east of the injection well site (Figure 1). Details of well drilling, construction and testing are documented in well completion reports (BGW 2001, 2002). A summary of well construction is provided in Table 1. CCD-X1 was drilled and geophysically logged to 1,500 feet. Subsurface sediments are interpreted as distal piedmont-slope lithofacies (LFA 5 as defined by Hawley and Haase, 1992) derived from the Sangre de Cristo Mountains with lesser amounts of fine-grained basin floor sediments (LFA 3 and 9) (Hawley and Cook, 2003). A correlative 150-foot-thick clay bed is logged above the screened interval at the site. A temporary deep zone and final intermediate zone were tested and found to have local permeability 1.5 to 2.1 ft/day. The exploratory well is completed with an intermediate depth screen and with nested deep and shallow piezometers, all below the 150-foot-thick clay.

Well CCD-P1 was drilled to 1330 feet and completed with a 570-foot-long screen to total depth. A four-day pumping test with one month of recovery indicates transmissivity (T) of local tested formation is 800 ft²/d (K = 1.4 ft/d) surrounded by low-permeability (T = 150 ft/d) material at distance. The long-term (several months) recovery trend indicates regional T of 500 ft²/d (Hawley and Cook, 2003).

The vertical hydraulic gradient between the CCD-P1 screen center and the CCD-X1 shallow piezometer, both below the well-defined clay bed is 0.04 ft/ft downward.

Water-level monitoring at exploration well CCD-X1 and production well CCD-P1 from years 2002 to 2006 (Figure 6) shows generally stable water levels with a slight declining trend at a rate of 0.3 ft/yr. The trend may reflect drawdown from City of Santa Fe wells. The deep piezometer is thought to have clogged perforations, therefore the water-level rise in that piezometer is not considered to reflect aquifer conditions. Background static water-level measurements at the pumping site were stopped in May

2006 prior to airlift testing and redevelopment of the pumping well. For the six-month recharge demonstration test, CCD-P1 was pumped to provide a source of injection water, and the CCD-X1 well nest served as an observation point for adjacent ($r = 63$ feet) aquifer response.

CCD-OWA was drilled as a pilot well for the injection site by Rodgers and Co. to 1800 feet depth from February 3 to 20, 2006. The borehole penetrated 90 feet of the basal Bishops Lodge member of the Tesuque Formation. Dr. John Hawley of Hawley Geomatters and Dr. Dan Koning of New Mexico Bureau of Geology & Mineral Resources provided logging and interpretation of drill cuttings (Appendix B). Subsurface sediments at CCD-OWA are similar to CCD-X1: sandy, distal piedmont-slope lithofacies (LFA 5) with inter-bedded fine- to coarse-grained basin floor sediments (LFA 3 and 9). Drill cuttings and geophysical logs (Figure 7) indicated several prospective zones of good permeability below a correlative 150-foot clay layer from depths 450 to 600 feet. The correlative 150-foot thick low-resistance clay layer above the screen zone is logged across the site. Three zones below the clay were screened with five-inch diameter slotted casing (Table 1; Figure 5). Two-inch diameter piezometers were installed in the CCD-OWA borehole annulus opposite the deep and intermediate screen settings. Each zone was tested in isolation at about 30 gallons per minute (gpm) for three to four hours. Isolation was accomplished with inflatable packers and by backfilling and sealing previously tested zones. Test-data charts and a summary table of test data and interpretation are included as Appendix C. The testing shows that local Tesuque Formation sand permeability decreases with depth from about 3.8 feet per day (ft/d) in the shallow zone to 0.6 ft/d in the deep zone. The tests also show that pressure change is transmitted between screen zones, apparently through the bentonite seals placed in the wellbore above the backfilled deep and intermediate screens. The vertical gradient below the 150-foot-thick clay at the well is 0.005 ft/ft upward between the shallow and deep screens, although the gradient may be affected by seal leakage.

The geophysical and test data from CCD-OWA and from the exploratory well drilling in year 2001 were used to plan construction of the injection well (CCD-I1). CCD-I1 was drilled to 1320 feet from March 6 to 13, 2006 and geophysically logged. Figure 7 shows the correlation of the distinctive clay and other beds between CCD-X1 and the injection and observation wells. Hawley (2006) (Appendix B) correlates a pebbly sand bed between the pumping and injection sites near the bottom of the CCD-OWA and CCD-X1 boreholes that indicates a regional westward dip of up to three degrees. CCD-I1 screen interval of 590 to 1310 feet was selected to include high-permeability zones tested at CCD-OWA and to correlate with about 300 feet of beds screened by CCD-P1 (Figure 7). The CCD-I1 screen extends about 400 feet above the correlative zone, and the CCD-P1 screen extends about 300 feet below. The well was completed on March 22, 2006 with 12-inch diameter stainless steel wire-wrap screen and with nested shallow and deep two-inch diameter piezometers. Figure 5 shows a schematic of well construction. The vertical hydraulic gradient across the clay bed at CCD-I1 is 0.06 ft/ft upward.

A seven-day pumping test was conducted at CCD-I1 in May 2006 after observation wells CCD-OWB and CCD-OWC were completed. During the test, CCD-OWA, CCD-OWB, and CCD-OWC and CCD-P1 served as observation wells. Charts and a table summarizing test results are included in Appendix C. The test showed that the local aquifer consists of channel sands with $K = 1.5 \text{ ft/d}$ enclosed by fine-grained deposits of low permeability, as indicated by steep late-time recovery trends. Test data are analyzed by the theoretical curves for flow dimensions reflecting one, two, or three dimensional flow systems corresponding to linear, radial or spherical flow patterns (Walker and Roberts, 2003) and gradations among the three types. The method is discussed in more detail in the "Analysis of Test Data" Section. The flow dimension of the CCD-I1 channel sand is $n = 1.1$ to 1.3 , approximating a linear channel. Response at CCD-P1 about one month after test shutdown indicates a regional transmissivity (T) of

100 ft²/d and a flow dimension of 2.3. The parameters are compatible with a fault-type boundary between the test and observation wells and induced leakage at late time.

Well CCD-OWB was drilled and logged to 1400 feet from March 28 to April 3, 2006. The well is located 474 feet west of the injection well. Five-inch diameter steel screen with 0.020-inch slots was set 610 to 1330 feet in beds correlative with the CCD-I1 screened interval. A shallow piezometer is installed with perforations about 120 feet below the water table, above the 150-foot-thick clay bed. Vertical gradient across the clay bed at the well is 0.01 ft/ft downward.

CCD-OWB was tested for about four hours at 30 gpm on May 9, 2006. CCD-OWA, CCD-OWC and CCD-I1 were observed for water-level response. Test charts and a summary table are included in Appendix C. Testing shows the well is completed in channel sands with $K = 2.2$ ft/d, enclosed by fine-grain deposits as indicated by steep late-time recovery. Observation well data show a radial-flow response ($n = 2$) compatible with Theis (1935).

CCD-OWC was drilled and logged to 1400 feet depth from April 17 to 22, 2006. The screen interval (680 to 1360 feet) was selected in beds correlative with CCD-I1 and CCD-OWB screens. A two-inch piezometer is installed about 200 feet below the water table, above the clay bed. Vertical gradient across the clay bed at the well is 0.03 ft/ft downward. The downward gradient at wells CCD-OWB and CCD-OWC may result from depressurization of the deeper Tesuque beds by nearby wells, such as the New Mexico State Penitentiary well and the Valle Vista Subdivision Community well, or by pressure built up at the water table from City of Santa Fe sewer effluent. The injection well and CCD-OWA with upward vertical gradients appear to be relatively isolated from these effects due to distance or compartmentalization.

Well CCD-OWC was tested at 36 gpm for four hours on May 11, 2006. Water levels were observed in CCD-I1, CCD-OWA and CCD-OWB, but showed no response to pumping at CCD-OWC. The test data are consistent with an aquifer composed of channel sands with $K = 1 \text{ ft/d}$ enclosed by fine-grained over bank deposits with one-tenth of the sand permeability, based on steep recovery trends at late time. The slope of drawdown implies a flow dimension of $n = 2.3$, compatible with leaky radial flow.

Charts and a test summary for all injection and observation single-well tests are attached as Appendix C.

Wells CCD-OWA, CCD-OWB and CCD-OWC are completed with locking steel protective covers set into a concrete pad. The injection well was left without a protective cover to accommodate valves and piping for the recharge demonstration. The wells have been continuously equipped with logging transducers since May 2006 to the present.

PUMPING AND INJECTION TEST DESIGN

The recharge demonstration test plan was designed for pumping 40 acre feet (AF) of Tesuque Formation groundwater from well CCD-P1 at 50 gallons per minute (gpm) for six months, piping the water one-mile west and injecting into the Tesuque Formation through Well CCD-I1. URS Engineering, Inc. in Phoenix, Arizona designed the pump installation and hydraulic conveyance system to control and transport water to the injection well. Engineering schematics and diagrams of the planned control and conveyance system are attached as Appendix D. The as-built system differs somewhat from the planned schematics. Photographs of the piping and valve installation at the

pumping and injection wellheads are in Figures 8 and 9. Photographs of the test installation and the observation wells are in Appendix E.

The pumping well is equipped with a 15-horsepower 70-gpm capacity pump set to 450 feet deep. Discharge rate is controlled to 50 gpm at the pumping wellhead with an adjustable flow control valve (FCV). Well discharge can be directed into the pipeline or, for flushing and cleaning, to waste at a local arroyo by adjusting the setting of two gate valves. A surge/pressure relief valve installed upstream of the gate valves protects the pipeline from overpressure.

Water is conveyed about one mile west to the injection site by a buried three-inch PVC pipe. The pipeline alignment is shown in Figure 10.

At the injection wellhead, a pair of gate valves allows water from the pipeline to be flushed to waste at a nearby arroyo, or to enter the injection well. An adjustable pressure reducing valve (PRV) maintains a constant pressure on the three-inch drop pipe set to 330 feet depth into the injection wellbore. A 0.48-inch diameter orifice installed at the bottom of the drop pipe restricts flow to maintain a full pipe to surface and prevent cascading water and air entrainment in injected water.

Flow at the pumping and injection wells is measured with McCrometer digital flow meters at each wellhead and recorded on dataloggers. Analog pressure gages are installed upstream and downstream of the FCV at the pumping well and the PRV at the injection well. Logging water-level transducers were deployed in the pumping and injection wells, five observation wells and several of the piezometers for monitoring water levels during the injection and recovery periods. Water levels in uninstrumented piezometers and three outlying wells were measured periodically with a well sounder. Observation wells are listed in Table 2 and shown in Figure 10.

Prior to installing the pumping and injection system, Rodgers and Co. chlorinated, swabbed and pumped well CCD-P1 to sterilize and rehabilitate the screen constructed five-years earlier. Rodgers and Co. also brushed and washed down the inside of the injection well casing above static water level to prevent contamination from leftover drilling materials on the wellbore. Rodgers installed the pump, injection drop pipe and valving at both wellheads. Rodgers Plumbing installed the three-inch transmission pipeline. The pipeline was flushed, then filled with chlorinated water for several days for sterilization before the start of injection. Cleaning, flushing and sterilizing the piping was considered part of the test protocol.

INJECTION DEMONSTRATION

The injection demonstration test started August 29, 2006 and ended February 27, 2007. Prior to start up, the pumping well and pipeline were purged and the control and conveyance system was tested. URS developed a start-up procedure (URS, 2006). Rodgers and Co. operated the pump and the valves. BGW directed the test and monitored wellhead pressure and water flow rates. At start up, water was pumped from CCD-P1 through the pipeline to waste in an arroyo near the injection well until clear and free of air. At 3:00 p.m., the gate valves at the injection wellhead were repositioned to direct water into the injection drop pipe and start the test. The drop pipe filled to surface in two minutes. Rodgers adjusted the FCV and PRV to achieve the target flow rate of 50 gpm. Pressure on the injection drop pipe was 20 psi at start of injection, but was increased to about 50 psi by the end of the six-month test to maintain constant pressure difference across the 0.48-inch orifice. BGW field notes and field sheets with periodic readings of flow, pressure and water levels are attached as Appendix F.

Figure 11 shows pumping and injection flow rates and water levels in the pumping and injection wells. Flow was maintained near the target 50 gpm, except for a few excursions above and below the target early in the test. Small changes in flow rate are reflected in water level response at both wells. We interpret same-time differences in pumping and injection rate to be meter error. Over the test period, the totalizing flow meter indicated that 12.6 million gallons (38.8 AF) of water was pumped and injected at an average rate of 50 gpm. The rate averaged 50.4 gpm for the first three months of the test, and 49.7 gpm for the last three-months, accounting for some late-time flattening of drawdown and build-up trends.

Figures 12 through 15 show hydrographs of water levels during six months of injection and six months of recovery at all monitored wells and piezometers. The pumping well drew down about 67 feet and nearby CCD-X1 about 52 feet at the end of the test (Figure 12). At the injection site (Figure 13), water-level buildup ranged from 83 feet at CCD-I1 to about ten feet at CCD-OWC 2,000 feet distant. CCD-OWA shallow and intermediate screens show identical response. The CCD-OWA deep screen response is probably influenced by leakage through the wellbore seal. Shallow piezometers at CCD-OWB and CCD-OWC (Figure 14) show a rise early in the test a few tenths of a foot, then stabilize. The response is more likely from flow through annular bentonite seal than from groundwater flow through the 150-foot clay aquitard. The shallow piezometer at the injection well, where the annular seal is a more-secure concrete bentonite, shows no response. CCD-X1 shallow piezometer, perforated about 200 feet above the pumping well screen, drew down about 15 feet from vertical leakage through intervening Tesuque beds. Four monitored outlying wells show no observable response to pumping or injection (Figure 15). None showed any effects of shutdown.

The injection well capacity was not fully used (83-foot buildup out of 294 feet available, or 28 percent). Addition available head below land surface implies that 150 gpm could be injected for a multi-year period.

Figure 16 shows distance-buildup relationship among the four wells at the injection site at several times. A low-permeability zone is apparent between wells CCD-OWA (96-foot distance) and CCD-OWB (470-foot distance). We interpret the zone as fine-grained overbank deposits enclosing the more permeable stacked channel sands at CCD-OWA and the injection well.

Displacement of groundwater by six months of injection is calculated to reach about 70 feet from the injection screen, assuming average specific yield of 15 percent. Displacement of formation water into the pumping well screen from six months of withdrawal is about 80 feet in radial extent.

Figure 17 shows water-level elevation and water temperature at the pumping and injection wells. Water temperature is measured by the transducers, set to 430 feet in the pumping well and 335 feet in the injection well. Initial water temperature in the pumping well was about 61°F, but had been raised prior to start of test by system testing, purging and troubleshooting. Temperature in the pumping well increased from 61°F to 69°F as warmer water from up to 1300-foot deep heats cooler shallow water. Injection well water temperature rises from 61°F to 69°F upon injection. Diurnal air temperature fluctuations are reflected in injection temperatures until early October, when insulated enclosures were installed at the pumping and injection wellheads (see photos in Appendix E). At the onset of cooler fall and winter temperatures, injected water temperature begins a steady decline from 68.5°F to about 65.5°F by end of test. The three-degree temperature change caused injected water viscosity to increase by about four percent, thus increasing water-level buildup proportionally ($0.04 \times 83 \text{ ft} = \sim 3 \text{ feet}$) in the wellbore. An increase of about 2.5 feet can be seen in the difference of water-level buildup between the injection well and CCD-OWA (Figure 18). At 96 feet from the injection well, CCD-OWA water levels are not affected by water temperature.

We conclude that the buildup difference is from temperature change and not from loss of screen or formation efficiency.

Figure 18 shows water-level buildup difference in the injection well deep piezometer and the injection screen. The deep piezometer was installed in the gravel pack alongside the screen to observe changes in water-level difference with the injection screen that might signal screen clogging. During the six-month injection phase, the difference in water levels was consistently about 2.7 feet. We conclude that no observable screen clogging occurred as a result of six months of water injection.

Figure 19 shows drawdown difference of CCD-P1 and CCD-X1 intermediate screen. A difference of about 15 feet is maintained for the six-month test, indicating that screen and nearby formation efficiency did not diminish.

Water was sampled from CCD-P1 at the end of the four-day test in 2002, and from CCD-I1 after the May 2006 seven-day test. A repeat sample from CCD-P1 was pulled for analysis on February 26, 2007 prior to shutting down the six-month test. Certificates of Analyses for the three samples are included as Appendix G.

Sampling at the pumping and injection sites from earlier multi-day tests show water quality at the sites is similar. Total dissolved solids (TDS) are 182 and 167 mg/l at the pumping and injection sites. Major ions are present in similar concentrations. Arsenic is the same at 10 parts per billion (ppb).

The CCD-P1 sample from the end of the six-month test showed slightly less TDS (145 mg/l) and substantially lower arsenic (4.9 ppb). The six-months of pumping have tapped into a slightly fresher water source than sampled initially. Water quality had no effect on the injection performance.

ANALYSIS OF TEST DATA

Six months of pumping and injection response and six months of recovery data are analyzed with GRF calculations and with a numerical model. The GRF calculation employs the formulas developed by Barker (1988) and Walker and Roberts (2003) to characterize aquifer geometry. The parameters resulting from the GRF calculations are used, in conjunction with a geologic and structural conceptual model of the aquifer system, to develop a three-dimensional numerical model with further spatial information. Both methods of test-data analysis are described below.

Generalized Radial Flow

Barker (1988) developed a GRF model to describe groundwater flow in a fractured rock system. GRF provides type-curves for analysis that are not limited to two-dimensional radial flow (e.g. Theis, 1935). The model employs a non-integer flow dimension ($1 \leq n \leq 3$) that describes the rate at which cross-sectional flow area changes with respect to distance from a source or sink (e.g., a well). Ideally, flow dimension $n = 1$ describes parallel flow inside a one-dimensional prism, $n = 2$ describes concentric two-dimensional radial flow (well function of Theis, 1935), and $n = 3$ is spherical three-dimensional flow to a point. Flow dimensions with values between the idealized integers are conceptualized to contain proportional elements of two or more ideal geometries. The GRF analytical model uses the usual parameters T and S to characterize the well screen zone, then adds a separate parameter of flow dimension to define the curve to be matched to field data, allowing for substantial geometric deviations from the Theis assumption of two-dimensional radial flow. Walker and Roberts (2003) expanded the GRF model concept to apply to general hydrogeologic systems, wherein flow dimension can represent aquifer heterogeneity, variable geometry, or boundaries, with values less than one (a container) and greater than three

(an external source). BGW adapted equations (4) through (6) of Walker and Roberts (2003) into a spreadsheet model for matching characteristic GRF curves against test data. The principle of superposition is used to simulate effects of the pumping/injection well pair, and to calculate recovery curves. Figures 20 through 31 show drawdown/buildup and recovery data with matching GRF curves for pumping, injection and observation wells. Table 3 contains a summary of curve-match results. Results are discussed below.

Buildup at the injection well and at CCD-OWA 96 feet distant have comparable GRF late-time curve matches (Figures 20 and 21), with $T = 210$ and $340 \text{ ft}^2/\text{d}$, Storativity (S) about 0.0004, and $n = 1.3$ and 1.1. A GRF curve with $T = 1050 \text{ ft}^2/\text{d}$ matches early CCD-OWA buildup. The flow dimension near one is interpreted to indicate the wells are completed in a linear flow system consisting of stacked linear channel sands bounded by low-permeability overbank deposits. Near-screen effective permeability within the sands is about $1.5 \text{ ft}/\text{d}$ ($1050 \text{ ft}^2/\text{d} \div 720 \text{ feet}$), but regional effective permeability is $1/3$ to $1/2 \text{ ft}/\text{d}$. Pumping at CCD-P1 appears to cause a flattening of the injection build-up trend 10 to 15 days after the start of the test, when the influence of the one-mile separation is seen. The flattening is less than theoretical due to the common interval of pumping well and injection well screen being about one-third the combined screened interval.

Wells CCD-OWB and CCD-OWC response during injection (Figures 22 and 23) matches GRF curves with parameters $T = 1050 \text{ ft}^2/\text{d}$, $S = 0.003$ and 0.002 , and $n = 1.2$ to 1.3. Flow dimension is consistent with stacked linear channel sands with leaky boundaries. Regional effective T as observed in these outlying wells is three to four times higher than that observed at CCD-OWA, the latter reflecting the low-permeability barrier seen in the distance-relationship between CCD-OWA and CCD-OWB (Figure 16).

Figures 24 and 25 show GRF curve matches to the pumping well and CCD-X1 drawdown. Matching parameters at late-time are $T = 185$ and $150 \text{ ft}^2/\text{d}$, $S = 0.00065$ and 0.0008 and $n = 1.7$ and 1.8 , respectively. Early time data are affected by residual drawdown from pre-test pumping for system testing and troubleshooting. Flow dimensions are somewhat less than radial flow ($n = 2$), and may reflect a leaky boundary at the fault mapped one-quarter mile west of the wells. Effective permeability is about $1/3 \text{ ft}/\text{d}$ ($185 \text{ ft}^2/\text{d} \div 530 \text{ ft}$), similar to that at the injection well. The values of T compare favorably to the four-day pumping late-time drawdown T of $150 \text{ ft}^2/\text{d}$ in Hawley and Cook (2003). The regional late-time recovery $T = 500 \text{ ft}^2/\text{d}$ in Hawley and Cook (2003) is not apparent in the six-month test data because coalescing pumping and injection cones flatten water levels.

GRF curves matched to recovery data at six wells are shown in Figures 26 through 31, and summarized in Table 3. GRF recovery curves were generated using superimposed curves with common parameters. In most cases, the recovery GRF parameters are similar to those derived for the injection/pumping period. The notable exception is the pumping and exploratory wells, which show a significant reduction in flow dimension (from $1.7/1.8$ to 1.4). The change may signal the influence of a more-distant flow boundary, such as the bedrock fault mapped one mile east of the pumping well (Figure 2), or depositional pinchout of the Tesuque at the Santa Fe Embayment margins (Figure 3).

The GRF curve-match parameters are used to help conceptualize the flow system for a three-dimensional numerical groundwater model. The analysis is interpreted to reflect the behavior of separate channel sands with K in the range of one to $2 \text{ ft}^2/\text{d}$ enclosed by lower K material in the range of one-fifth to one-tenth those values. The sands have lateral dimensions on the scale of hundreds of feet and long dimensions of several miles.

Numerical Model

A groundwater model was developed to simulate the flow system at the pumping and injection test site with spatial detail not available from the GRF analysis. An illustration of the conceptual hydrogeologic system is in Figure 32. The model is developed with the finite difference MODFLOW packages of Harbaugh and others (2000). Appendix H contains a technical memorandum detailing model conceptualization, construction, calibration and fit to test data. The numerical model provides a framework for further simulation of development scenarios for water injection operations. The key points of the technical memorandum are summarized below.

The model was developed to fit Hawley's geologic concept of stacked, linear, high-permeability sand channels with a north-south orientation enclosed by over bank and other deposits of lower permeability. The GRF curve match for the seven-day CCD-I1 test (Appendix C) and from the six-month injection period show a predominately low-dimension linear flow response of aquifer water levels to a stress, consistent with that geology. The model grid and cross sections are shown in Figures 33 and 34. Regional hydraulic conductivity is simulated at 0.25 to 0.5 feet/day. Linear channel sands are simulated with a north-south trending zone of model cells at $K =$ one-half to one foot/day. Enclosing fine-grain deposits are hundredths of ft/d conductivity. Faults one-quarter mile west and one mile east of the pumping well are included as leaky barriers. Regional dip structure is west and north, compatible with geophysical and lithologic correlations (Figure 7) and aeromagnetic data (Figure 3). Injection and production well screens are simulated in the corresponding layers on a 100-foot layer discretization.

Observed and simulated heads at OWA, OWB, OWC and CCD-X1 are shown in Figures 35 through 38. The model is a reasonable simulation of test results, with simulated head within 5 to 10 percent of observed head and r-squared values over 0.95.

Figure 39 shows the simulated injection and pumping pressure response at several times during the test. An animation of the pressure response can be viewed at <http://balleau.com/results.php?category=tools>. At the injection site, water first pressurizes the high permeability channel before leaking into surrounding beds. The two cones of production and injection coalesce at 35 to 40 days from start of test. The fault simulated between the pumping and injection sites causes the pumping pressure gradient to steepen westward. The six-month radius of influence of injection reached to about two miles with one foot of buildup in channel sands and in other sediments (Figure 33). The test-response area continued to expand throughout the one year of monitoring.

The flow dimension of the model-simulated response is calculated in Appendix H using the derivative of the simulated pressure change in a method described by Walker and Roberts (2003). The pumping and injection well effects are excluded to avoid that artificial boundary, and to characterize only the aquifer properties. Model-calculated flow dimensions vary, generally increasing through time to reflect heterogeneity and scale-dependent factors built into the model that the analytical GRF curves do not represent. The model response is in the flow dimension range of less than 1.0 to near 3.0, averaging near the analytical values between 1.0 and 2.0. The increasing flow dimension illustrates the evolution from response in channel sands to more three-dimensional volumes of the aquifer space.

CONCLUSIONS

1. An injection well and three observation well nests were drilled in year 2006 for a recharge demonstration project undertaken cooperatively by Governor Richardson's Water Innovation Fund and Rancho Viejo de Santa Fe, Inc.
2. Drill cuttings and geophysical logs indicate the Tesuque Formation aquifer penetrated by the test wells are correlative, consisting of distal piedmont-slope fluvial sands and gravels interbedded with silt and clay.
3. Pilot Observation Well A penetrated the Bishops Lodge Member base of the Tesuque Formation at 1800 feet.
4. Lithologic and geophysical log correlations among the injection test wells and the associated Community College District exploratory well drilled in year 2001 indicate that beds dip up to three degrees west across the study site.
5. The Community College District pumping well and injection well one-mile apart are screened in correlative Tesuque beds with the pumping well screen extending below and injection screen extending above the common screened interval.
6. Individual pumping tests of injection and observation wells indicate a non-radial flow response. The response is compatible with an aquifer composed of a series of stacked linear channel sands, enclosed by fine-grained deposits.
7. A six-month injection demonstration with one-year monitoring of response, involved withdrawing 50 gallons per minute of groundwater at the pumping well site, piping it one mile west and injecting it to the injection well. A total of 38.8 acre feet was pumped and injected from August 2006 to February 2007.

8. End-of-test water-level buildup ranged from 83 feet at the injection well to 11 feet at the 2000-foot distant observation well. Drawdown at the pumping well was about 67 feet. The shallow water table above a 150-foot thick clay showed no observable response. At the end of the full year of monitoring, water levels were back to two feet residual buildup at the injection well and three feet residual drawdown at the pumping well.
9. No clogging of the injection screen, gravel pack or formation was observed during the six-month test. Effects of injection water temperatures, which alter viscosity, were seen.
10. A clean, sterile, positive-pressure operation free of gas or air contributed to the injection efficiency.
11. Water sampling indicates water quality at the pumping and injection sites is similar. Six months of pumping produced water with lower total dissolved solids and arsenic (about five parts per billion). Water quality had no impact on the injection test.
12. Generalized radial flow calculations to match data show that non-radial flow with leakage characterizes the response at the injection site (flow dimension = 1.1 to 1.3). The pumping site is characterized by nearly radial flow with a close-in boundary (flow dimension = 1.7 to 1.8).
13. Water was displaced 80 feet radially into the pumping well and 70 feet radially from the injection well.
14. The test site flow system is simulated with a numerical model that incorporates linear channel features and fault barriers. The numerical model simulates the observed response. The model is suitable to adaptation for projecting scenarios of future injection project effects.

15. The injection well and Tesuque aquifer at the test site is capable of accepting 150 gallons per minute (240 acre feet per year) for an extended period with no adverse effects to well efficiency or aquifer performance.

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TABLES

RANCHO VIEJO

WATER PLAN

TABLE 1. SUMMARY OF WELL CONSTRUCTION

Well	Completion Date	X (ft) ¹	Y (ft) ¹	Land Elevation ¹ (ft msl)	Total Depth Drilled (ft)	Screen Interval (ft)	Screen Length (ft)	Casing Diameter (in)	Pre-Test Static Water Level ² (ft)	Water Level Elevation (ft msl)	Vertical Head Difference ³ (ft)	Vertical Gradient (to Screen Centers) ³ (ft/ft)
CCD-X1	21-Dec-01	1714736	1673013	6556.6	1500	690 - 890	200	6	244.3 ⁴	6312.3	15.0	0.06
Shallow Piezometer						530 - 540	10	2	229.3 ⁴	6327.3		
Deep Piezometer ⁵						1137 - 1157	20	2	231.2 ⁴	6325.4		
CCD-P1	26-Jan-02	1714675	1672996	6555.4	1330	740 - 1310	570	12	248.4 ⁴	6307.0	--	0.04 ⁶
CCD-I1	22-Mar-06	1709338	1671966	6479.9	1320	590 - 1310	720	12	293.6	6186.3	-20.5	-0.06
Shallow Piezometer						350 - 370	20	2.5	314.1	6165.8		
Deep Piezometer						690 - 710	20	2.5	294.1	6185.8		
CCD-OWA	20-Feb-06	1709334	1672062	6482.5	1800	580 - 620	40	5	294.2	6188.3	-4.7	-0.005
Intermed. Piezometer						1020 - 1140	120	2.5	293.7	6188.8		
Deep Piezometer						1500 - 1580	80	2.5	289.5	6193.0		
CCD-OWB	3-Apr-06	1708866	1672010	6473.3	1400	610 - 1330	720	5	296.3	6177.0	6.6	0.01
Shallow Piezometer						370 - 390	20	2.5	289.7	6183.6		
CCD-OWC	27-Apr-06	1707268	1671862	6418.0	1400	680 - 1360	680	5	249.6	6168.4	15.3	0.03
Shallow Piezometer						430 - 450	20	2.5	234.3	6183.7		
La Cienega Well	Unknown	1725342	1674127	6787.0	230	Unknown	--	4	227.4	6559.6	--	--
El Rancho Well	Unknown	1713589	1670440	6538.0	230	Unknown	--	4	214.0	6324.0	--	--
Rancho Viejo Obs. Well	Unknown	1716280	1662000	6536.0	700	250 - 700 ⁷	310 ⁷	4	203.3	6332.7	--	--
SFCC Well	Unknown	1714799	1674217	6579.0	460	Unknown	--	5	238.1 ⁸	6340.9	--	--

¹ Coordinates are New Mexico State Plane Central NAD83 / NGVD 29

² Measured August 2006 unless otherwise noted; depth below ground level

³ Negative number indicates upward gradient

⁴ Measured 5/2/2006 before pumping well was airlift tested and developed

⁵ Piezometer clogged

⁶ CCD-X1 Shallow Piezometer to CCD-P1 vertical gradient

⁷ Screened intervals are 250-300, 280-420, 540-610, and 650-700 feet

⁸ Measured 9/5/2006, after start of test

RANCHO VIEJO

WATER PLAN

TABLE 2. SUMMARY OF INJECTION DEMONSTRATION TEST AUGUST 2006 TO FEBRUARY 2007,
WITH RECOVERY TO SEPTEMBER 2007

Well	Distance from Pumping Well (ft)	Distance from Injection Well (ft)	Pre-Test Static Water Level ¹ (ft)	End-of-Test Depth to Water ² (ft)	End-of-Test Water Level Change ³ (ft)	End-of-Recovery Depth to Water ⁴ (ft)	Residual Water Level Change ³ (ft)
CCD-X1	63	5499	244.3 ⁵	297.8	53.5	247.9	3.6
Shallow Piezometer			229.3 ⁵	243.9	14.6	232.7	3.4
Deep Piezometer ⁶			231.2 ⁵	231.8	0.6	231.6	0.4
CCD-P1	0.5	5435	248.4 ⁵	315.6	67.2	251.8	3.4
CCD-I1	5435	0.5	293.6	208.9	-84.7	291.4	-2.2
Shallow Piezometer			314.1	314.2	0.1	314.3	0.2
Deep Piezometer			294.1	208.5	-85.6	291.6	-2.5
CCD-OWA	5422	96	294.2	219.0	-75.2	291.2	-3.0
Intermed. Piezometer			293.7	218.8	-74.9	290.5	-3.2
Deep Piezometer			289.5	218.4	-71.1	286.5	-3.0
CCD-OWB	5892	474	296.3	279.2	-17.1	292.9	-3.4
Shallow Piezometer			289.7	287.4	-2.3	290.3	0.6
CCD-OWC	7493	2073	249.6	238.4	-11.2	247.0	-2.6
Shallow Piezometer			234.3	233.8	-0.5	234.3	0.0
La Cienega Well	10,727	16,149	227.4	225.8	-1.6 ⁷	NM	--
El Rancho Well	2777	4517	214.0	214.1	0.1 ⁸	NM	--
Rancho Viejo Obs. Well	11,112	12,146	203.3	202.7	-0.6 ⁹	NM	--
SFCC Well	1228	5907	238.1 ¹⁰	233.7 ¹¹	-4.4 ¹²	NM	--

¹ Below ground level, measured August 2006 unless otherwise noted

² Below ground level, measured 2/26/2007 unless otherwise noted

³ Negative number indicates groundwater buildup

⁴ Measured 9/19/2007

⁵ Measured 5/2/2006 before pumping well was airlift tested and developed

⁶ Piezometer clogged

⁷ Recovery from summer pumping

⁸ Barometric pressure effect

⁹ Affected by nearby windmill well

¹⁰ Measured 9/5/2006, after start of test

¹¹ Measured 2/20/2007

¹² Recovery from summer pumping

NM = Not measured

RANCHO VIEJO

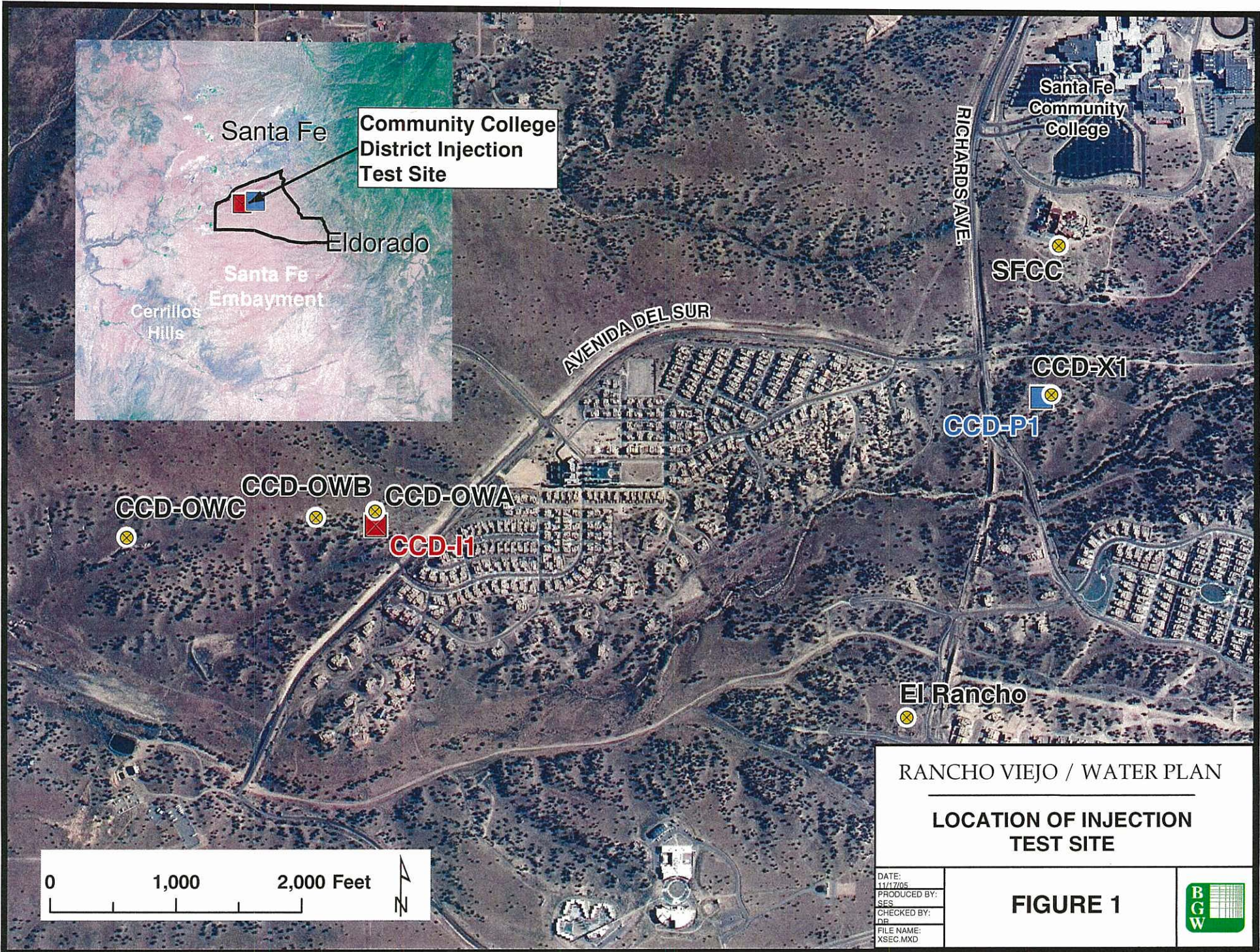
WATER PLAN

TABLE 3. RESULTS OF GRF ANALYSES FOR INJECTION/PUMPING AND RECOVERY PERIODS

Well	Six-month Pumping/Injection			Six-month Recovery		
	Transmissivity (ft ² /d)	Storativity	Flow Dimension	Transmissivity (ft ² /d)	Storativity	Flow Dimension
CCD-I1	210	0.00035	1.3	220	0.00025	1.3
CCD-OWA (intermed.)	340	0.0004	1.1	270	0.00025	1.2
CCD-OWB	1050	0.003	1.2	900	0.007	1.2
CCD-OWC	1050	0.002	1.3	860	0.005	1.3
CCD-P1	175	0.00065	1.7	290	0.0015	1.4
CCD-X1	150	0.0008	1.8	300	0.0015	1.4

Analyzed by methods adapted from Walker and Roberts (2003).

FIGURES



Legend

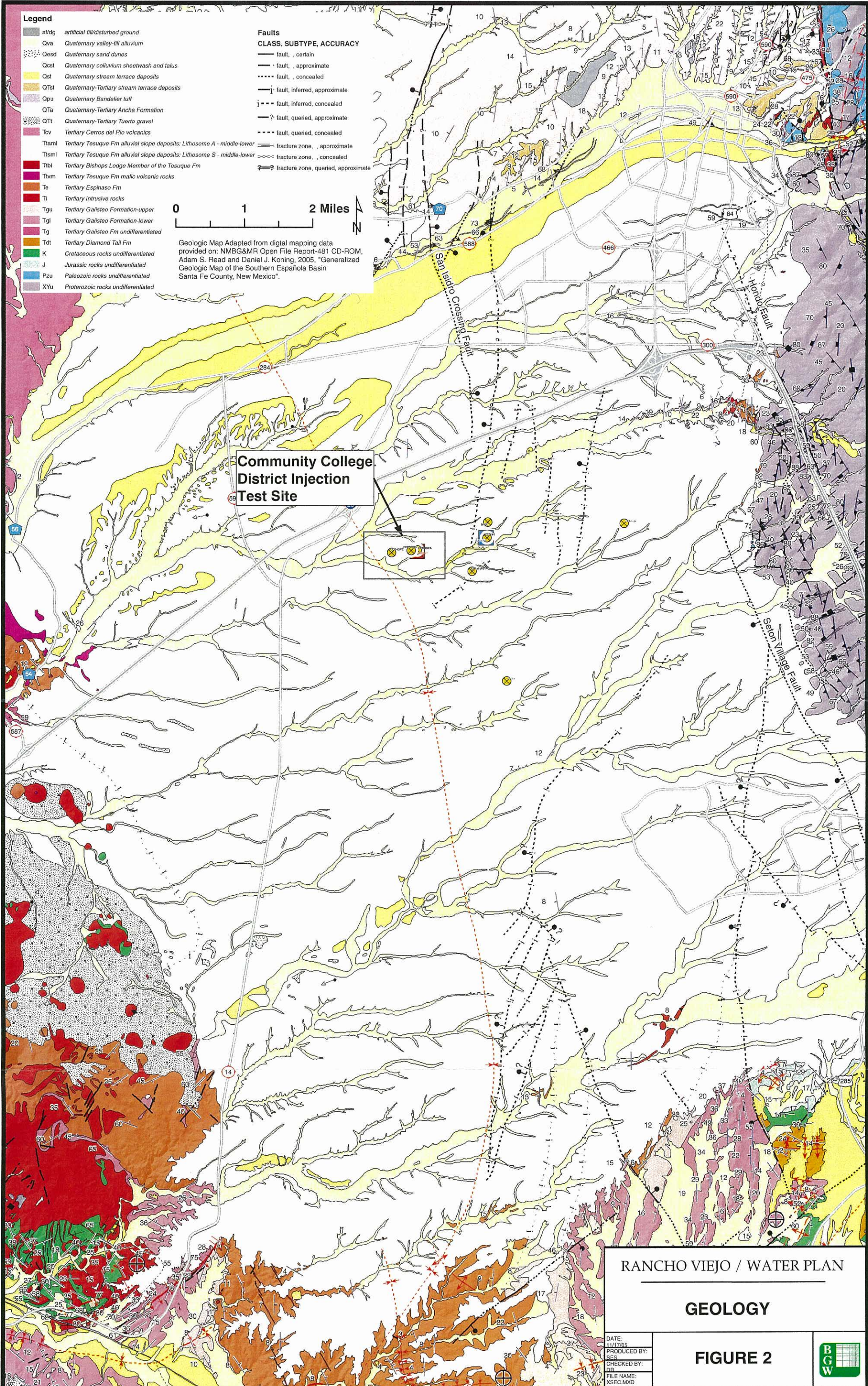
- af/dg artificial fill/disturbed ground
- Qva Quaternary valley-fill alluvium
- Qcsd Quaternary sand dunes
- Qcst Quaternary colluvium sheetwash and talus
- Qst Quaternary stream terrace deposits
- QTst Quaternary-Tertiary stream terrace deposits
- Cpu Quaternary Banderol tuff
- QTa Quaternary-Tertiary Ancha Formation
- QTt Quaternary-Tertiary Tuerto gravel
- Tcv Tertiary Cerros del Pio volcanics
- Tiaml Tertiary Tesuque Fm alluvial slope deposits: Lithosome A - middle-lower
- Tismil Tertiary Tesuque Fm alluvial slope deposits: Lithosome S - middle-lower
- Tibi Tertiary Bishop's Lodge Member of the Tesuque Fm
- Tivm Tertiary Tesuque Fm mafic volcanic rocks
- Te Tertiary Espinazo Fm
- Ti Tertiary intrusive rocks
- Tgu Tertiary Galisteo Formation-upper
- Tgl Tertiary Galisteo Formation-lower
- Tg Tertiary Galisteo Fm undifferentiated
- Tdt Tertiary Diamond Tail Fm
- K Cretaceous rocks undifferentiated
- J Jurassic rocks undifferentiated
- Pzu Paleozoic rocks undifferentiated
- XYu Proterozoic rocks undifferentiated

Faults

- CLASS, SUBTYPE, ACCURACY**
- fault, , certain
 - - - fault, , approximate
 - · · · fault, , concealed
 - | - fault, inferred, approximate
 - | - - fault, inferred, concealed
 - ? - fault, queried, approximate
 - ? - - fault, queried, concealed
 - - - - fracture zone, , approximate
 - - - - fracture zone, , concealed
 - - - - ? fracture zone, queried, approximate

0 1 2 Miles

Geologic Map Adapted from digital mapping data provided on: NMBG&MR Open File Report-481 CD-ROM, Adam S. Read and Daniel J. Koning, 2005, "Generalized Geologic Map of the Southern Española Basin Santa Fe County, New Mexico".



Community College District Injection Test Site

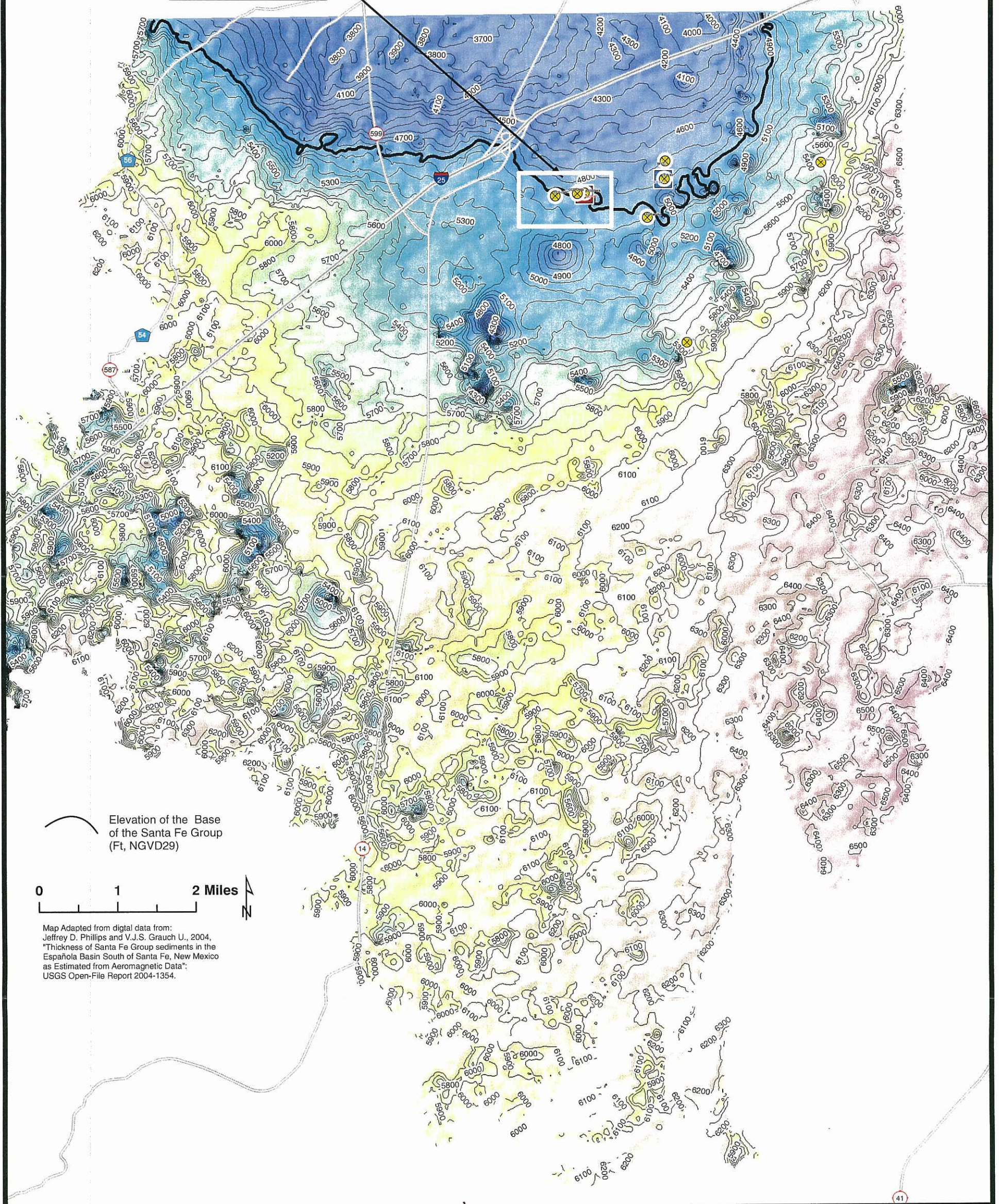
RANCHO VIEJO / WATER PLAN
GEOLOGY

FIGURE 2

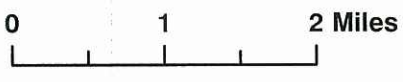
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**Community College
District Injection
Test Site**



Elevation of the Base of the Santa Fe Group (Ft, NGVD29)



Map Adapted from digital data from:
Jeffrey D. Phillips and V.J.S. Grauch U., 2004,
"Thickness of Santa Fe Group sediments in the
Española Basin South of Santa Fe, New Mexico
as Estimated from Aeromagnetic Data";
USGS Open-File Report 2004-1354.

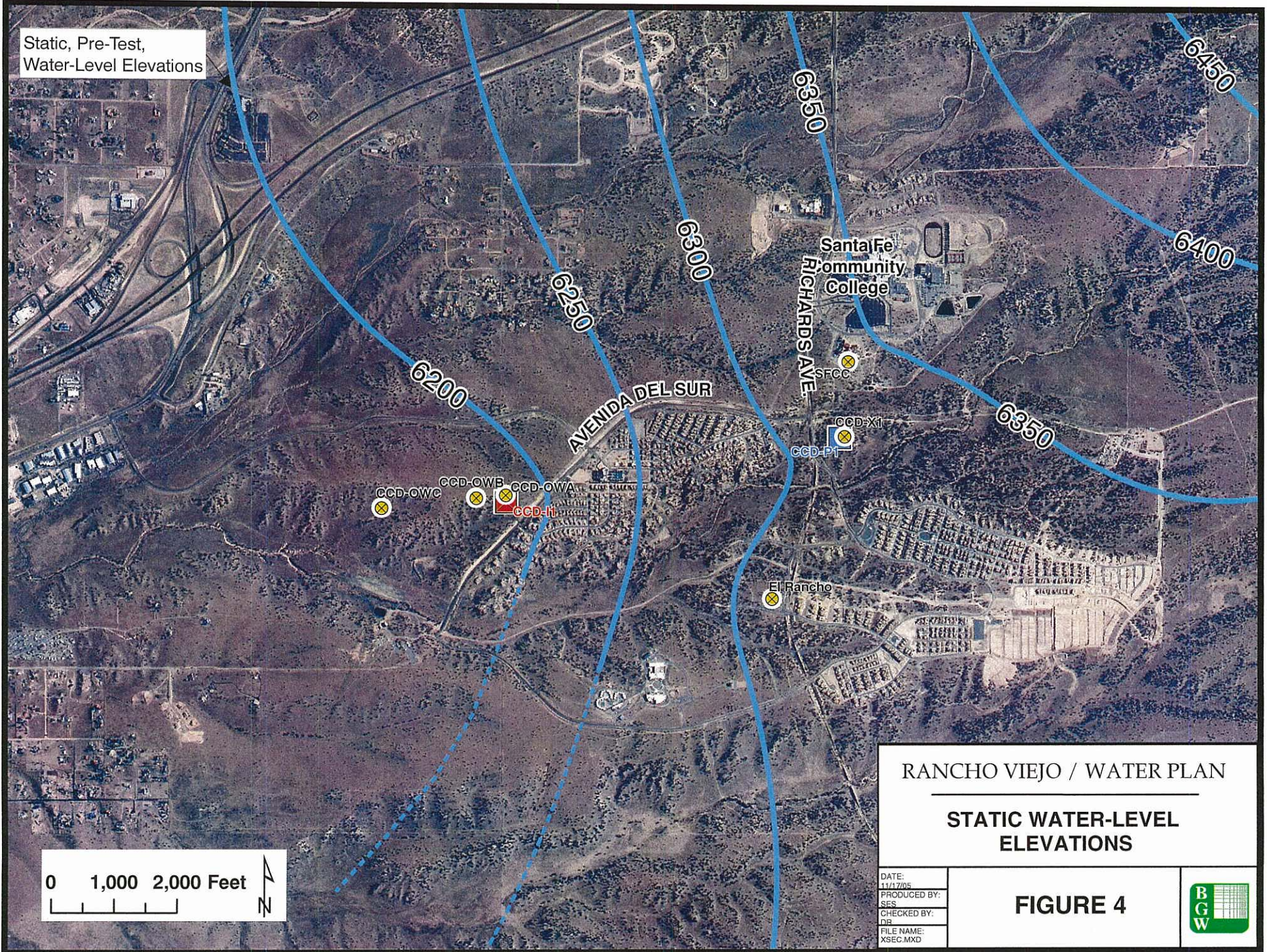
RANCHO VIEJO / WATER PLAN
ELEVATION OF BASE OF
TESUQUE FROM
AEROMAGNETIC DATA

DATE:
10/31/07
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SES
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CC
FILE NAME:
amag2.MXD

FIGURE 3



Static, Pre-Test,
Water-Level Elevations

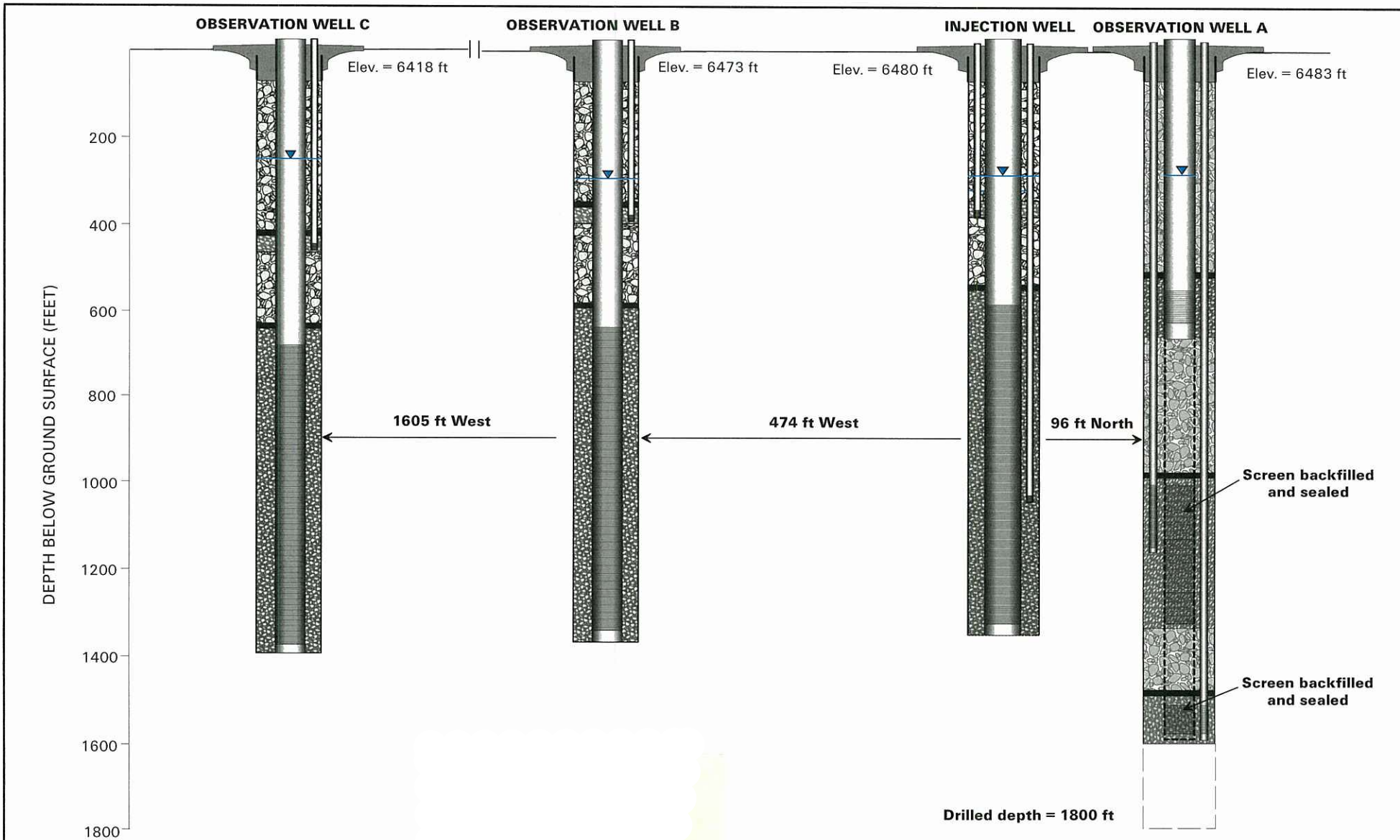


RANCHO VIEJO / WATER PLAN
STATIC WATER-LEVEL
ELEVATIONS

FIGURE 4

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11/17/05
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**RANCHO VIEJO / WATER PLAN
SCHEMATIC CROSS SECTION
OF INJECTION AND
OBSERVATION WELLS**

Date:
10/29/07
Produced By:
CWC
Checked By:
WPB
Filename:
rj wellfield as built.dwg

FIGURE 5



See BGW (2001) and BGW (2002) for CCD-P1 and CCD-X1 schematics

FIGURE 6
COMMUNITY COLLEGE DISTRICT PUMPING WELL SITE PRE-TEST HYDROGRAPHS
2002 - 2006

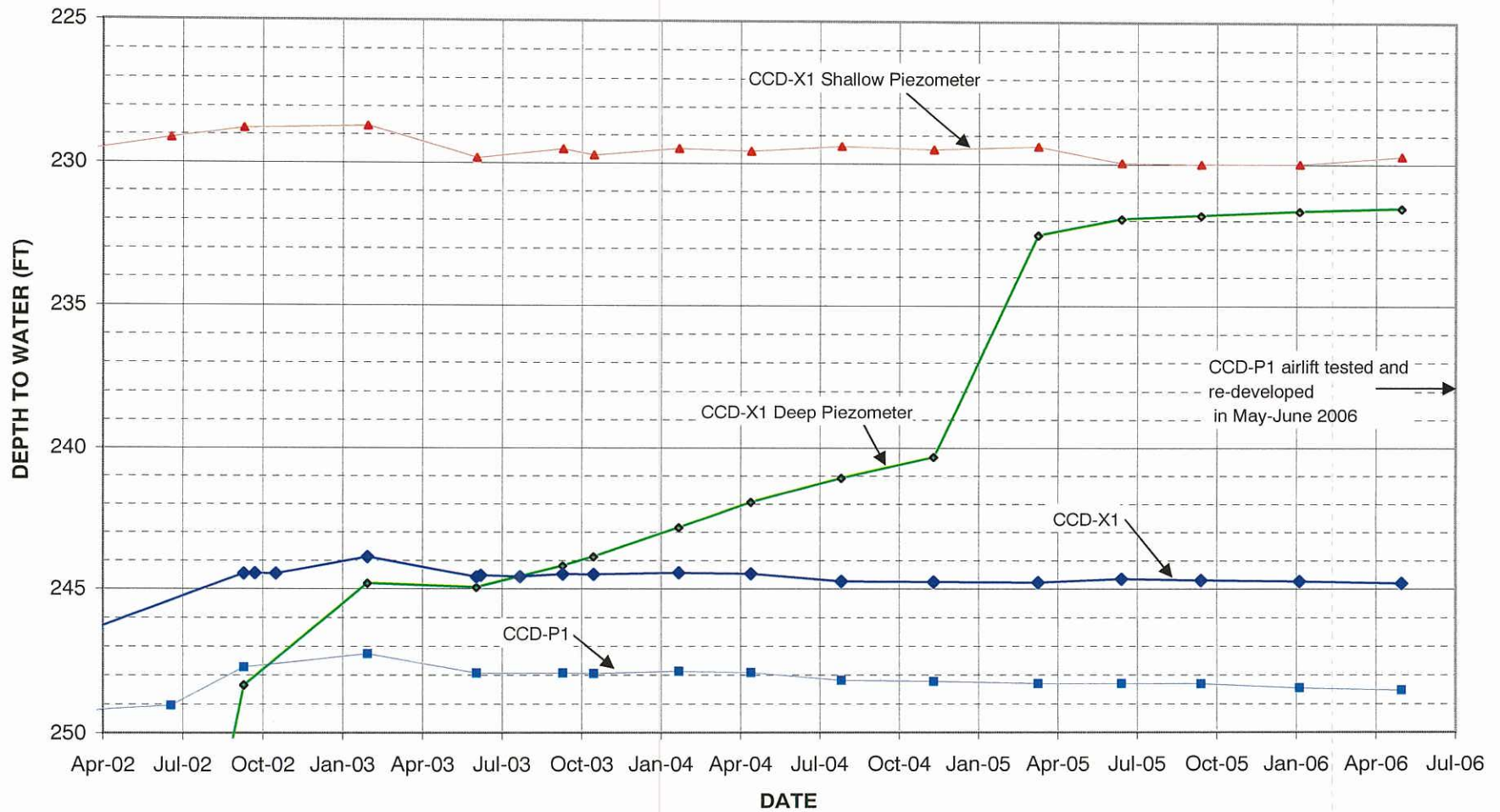


FIGURE 7
BOREHOLE GEOPHYSICS AND CORRELATIONS

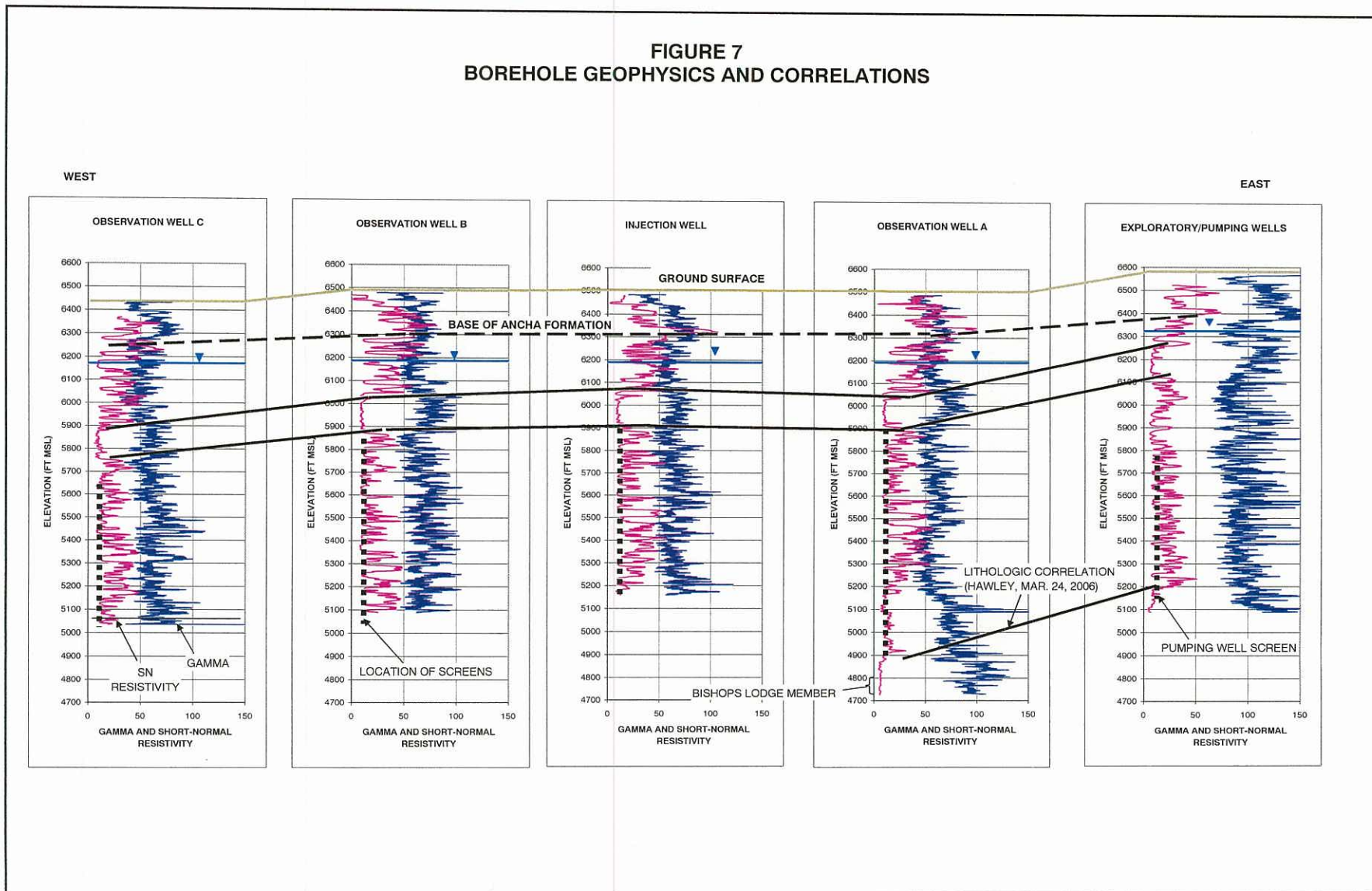


FIGURE 8
PUMPING WELL TEST SETUP

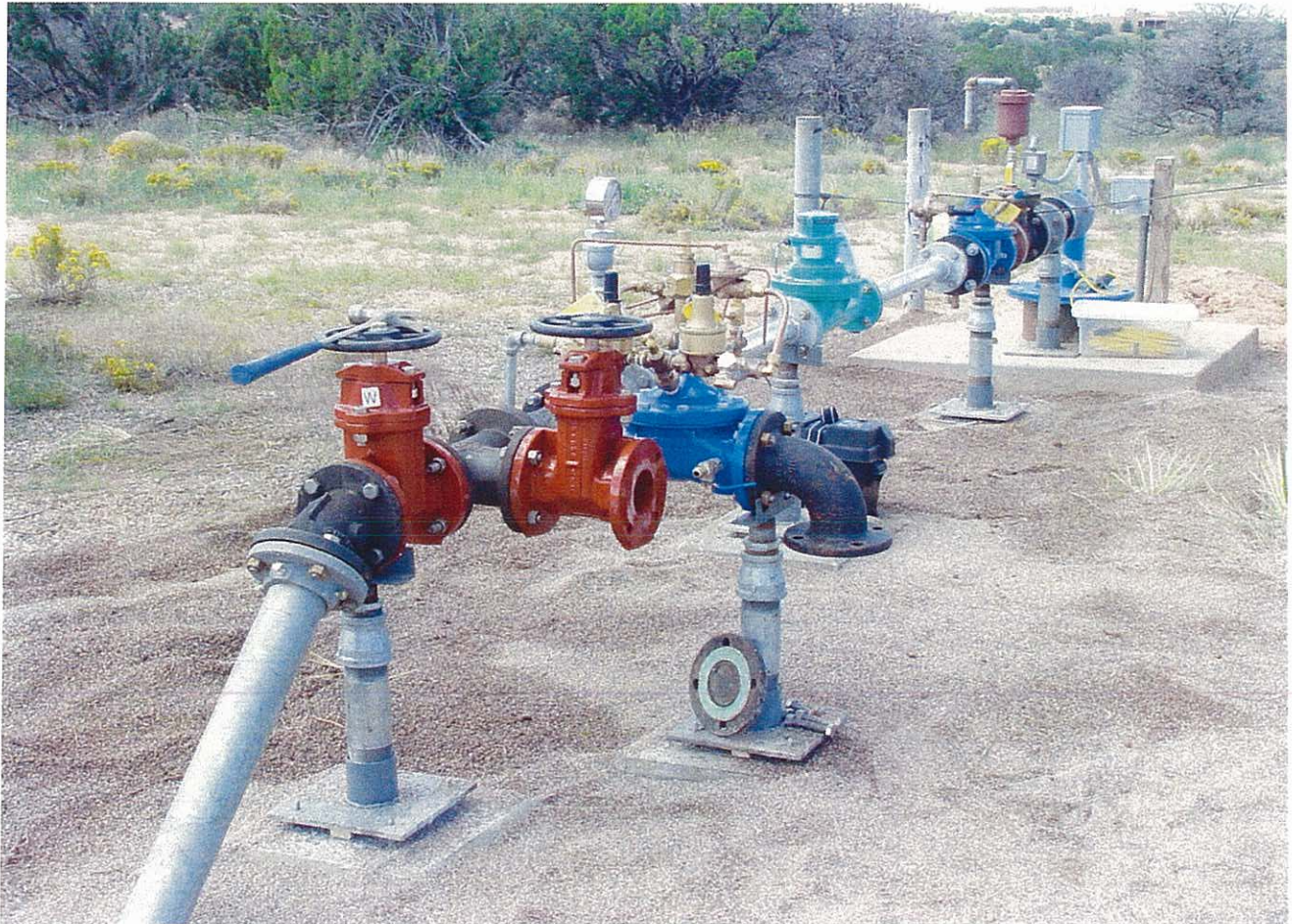
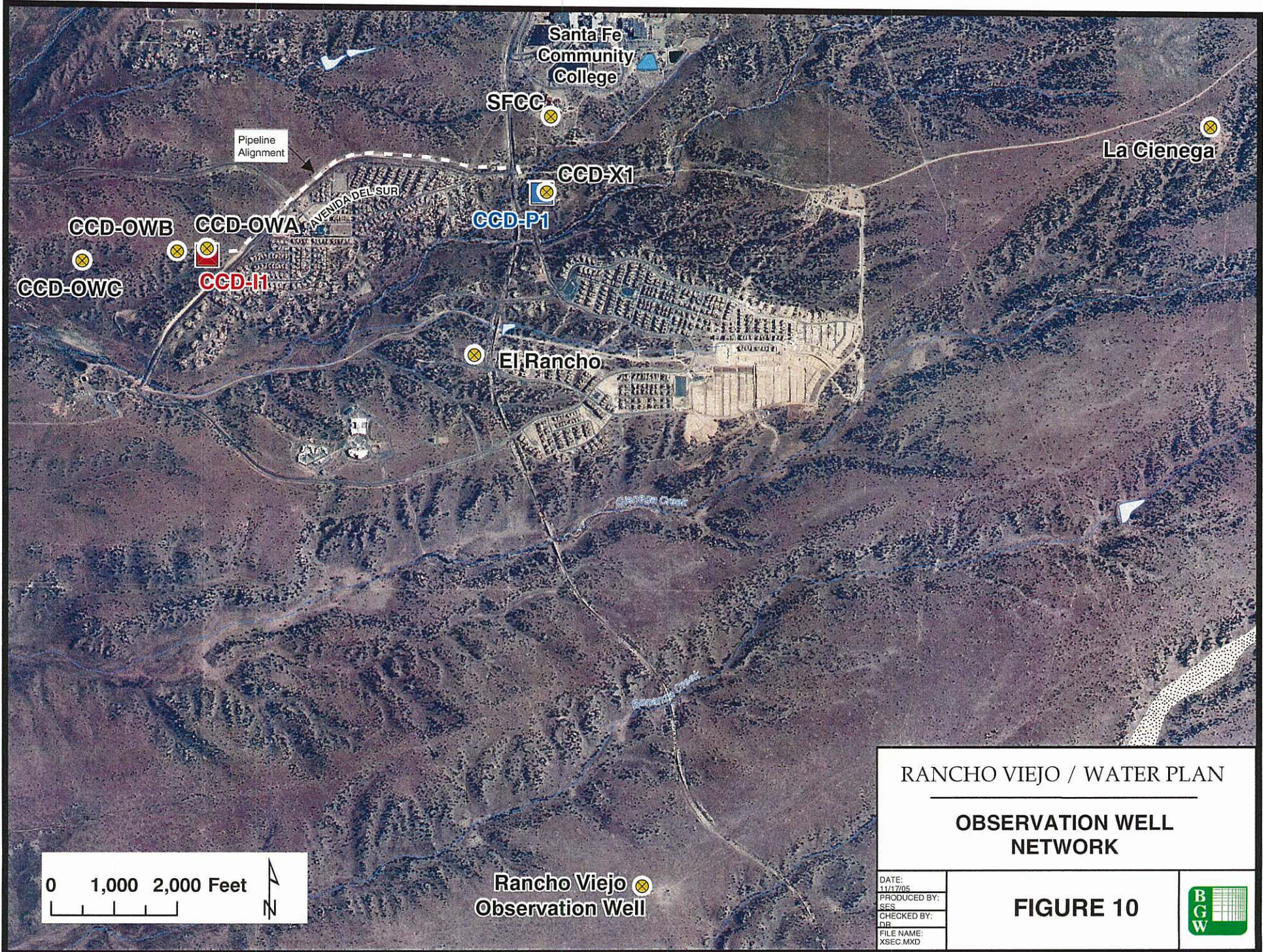


FIGURE 9
INJECTION WELL TEST SETUP





WATER PLAN

FIGURE 11
PUMPING AND INJECTION WELL WATER LEVELS AND FLOW RATES

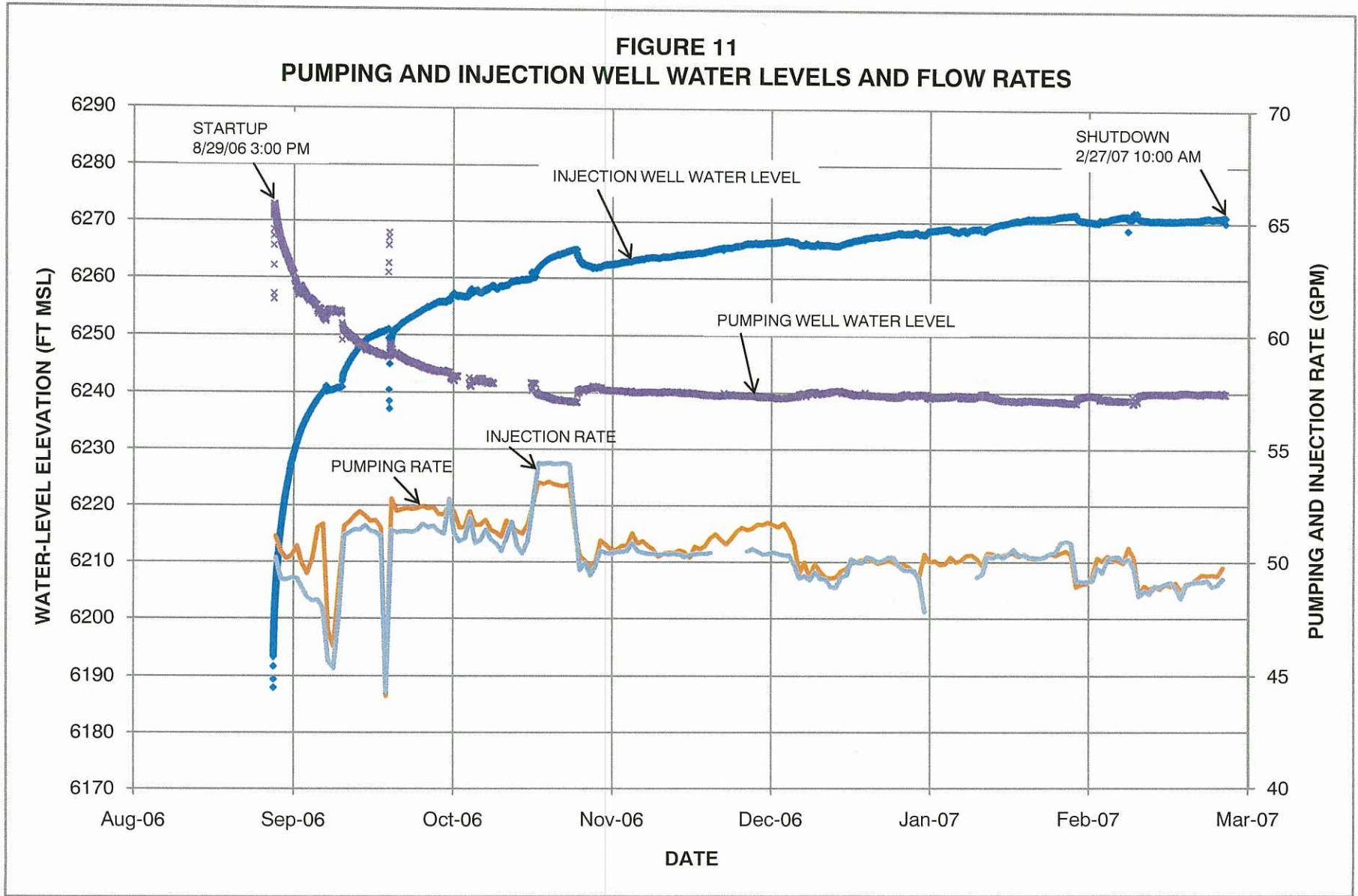


FIGURE 12
PUMPING AND EXPLORATORY WELL DRAWDOWN AND RECOVERY

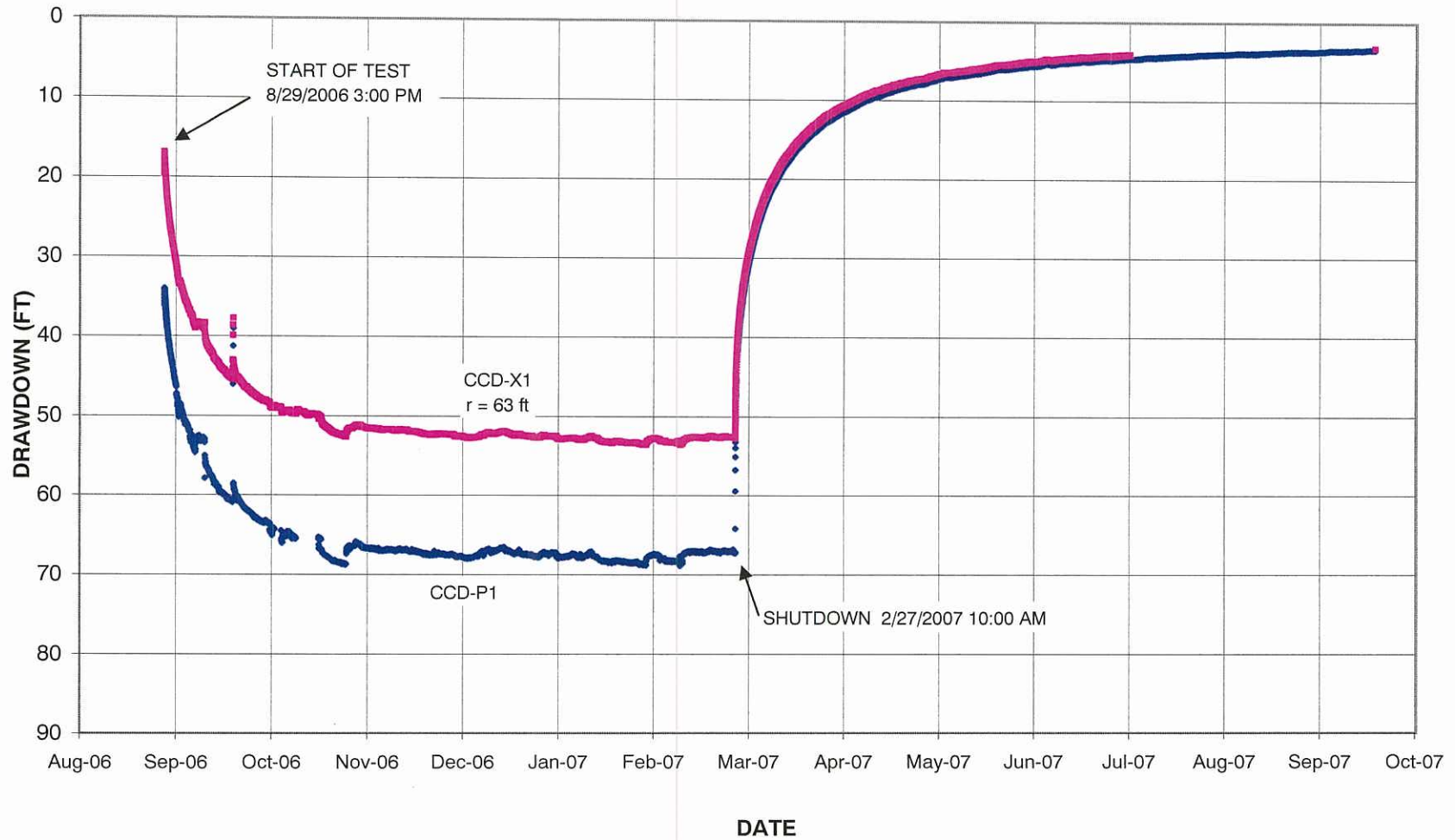
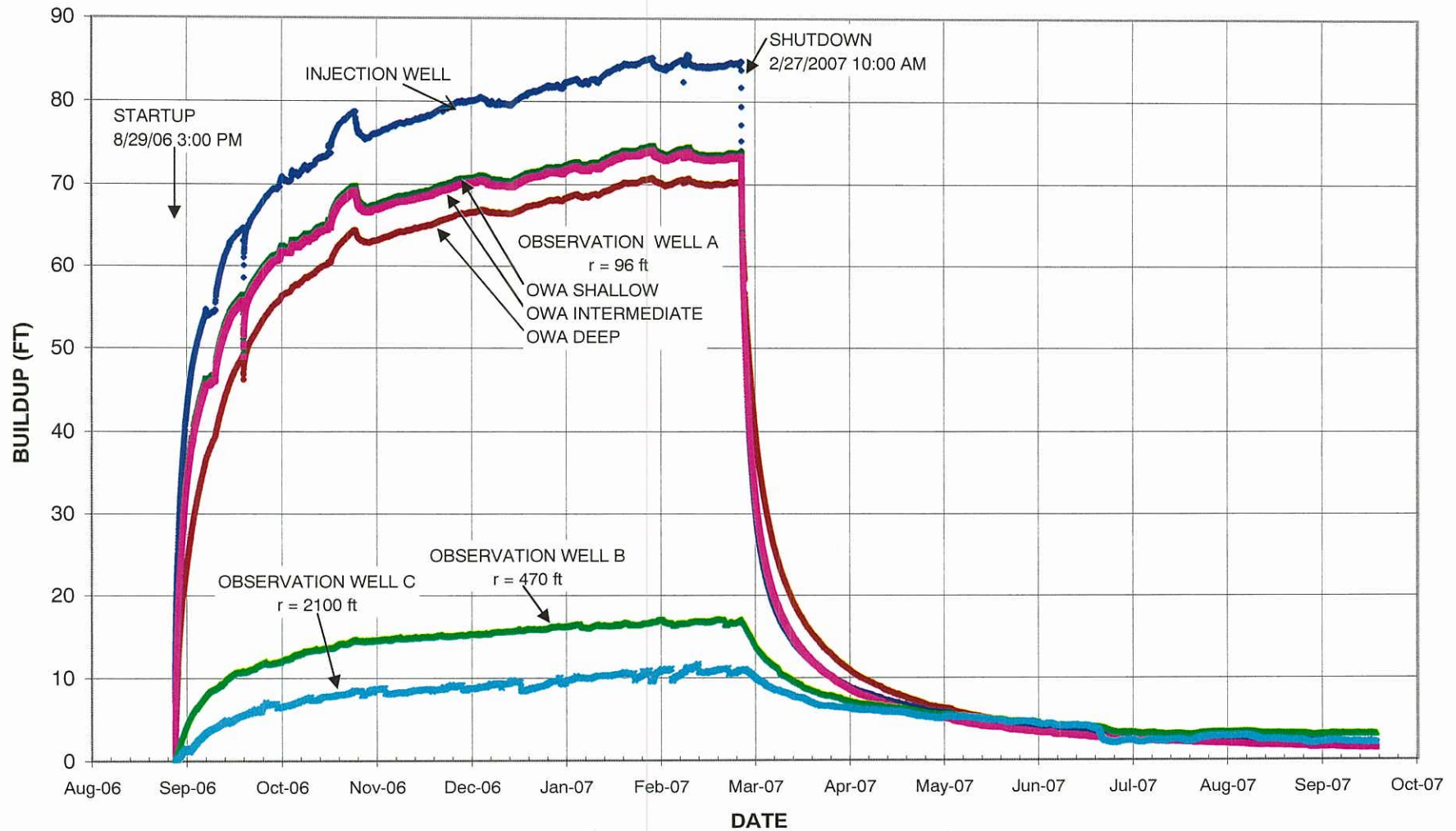
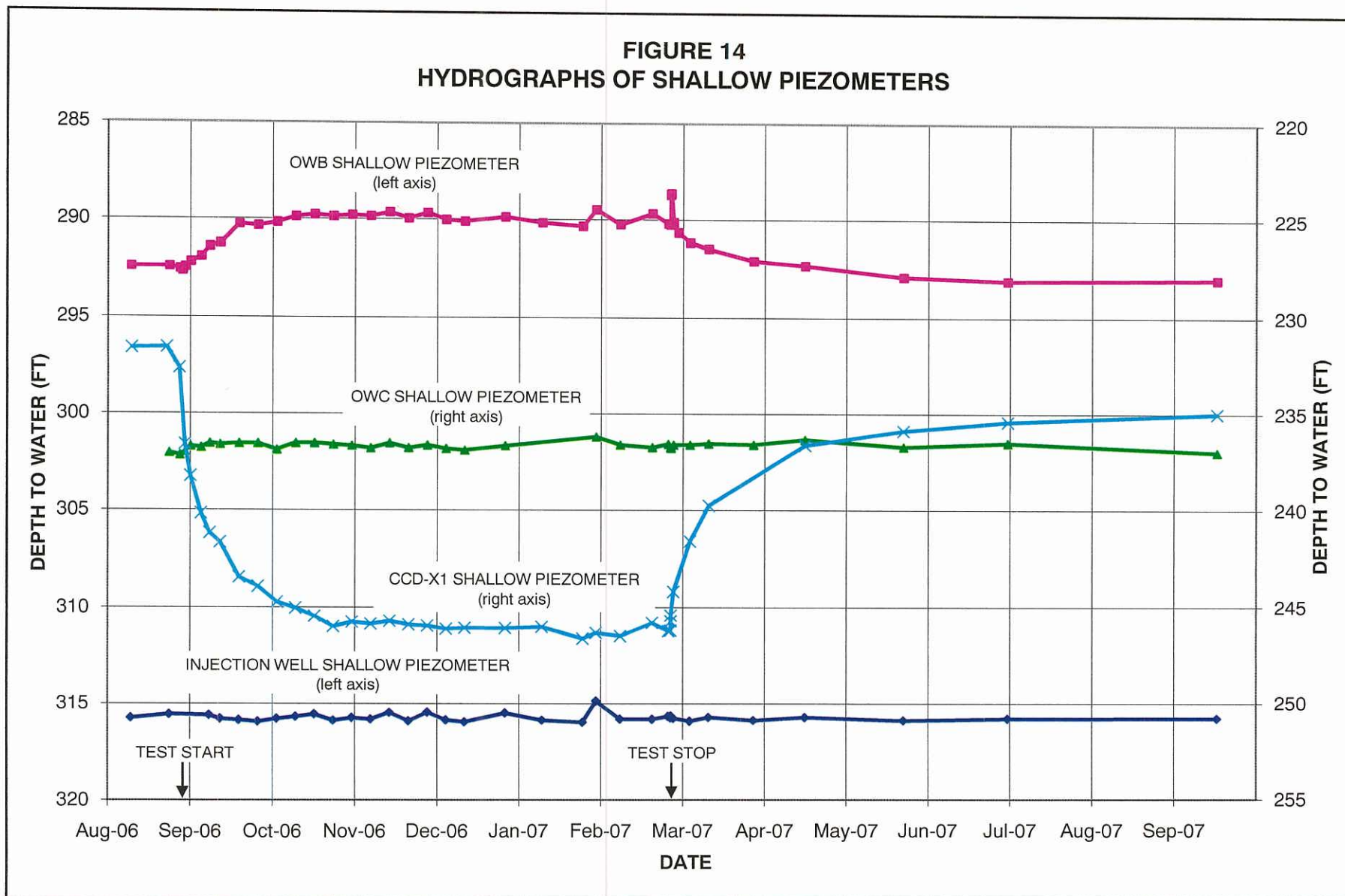


FIGURE 13
INJECTION AND OBSERVATION WELL WATER-LEVEL BUILDUP AND RECOVERY

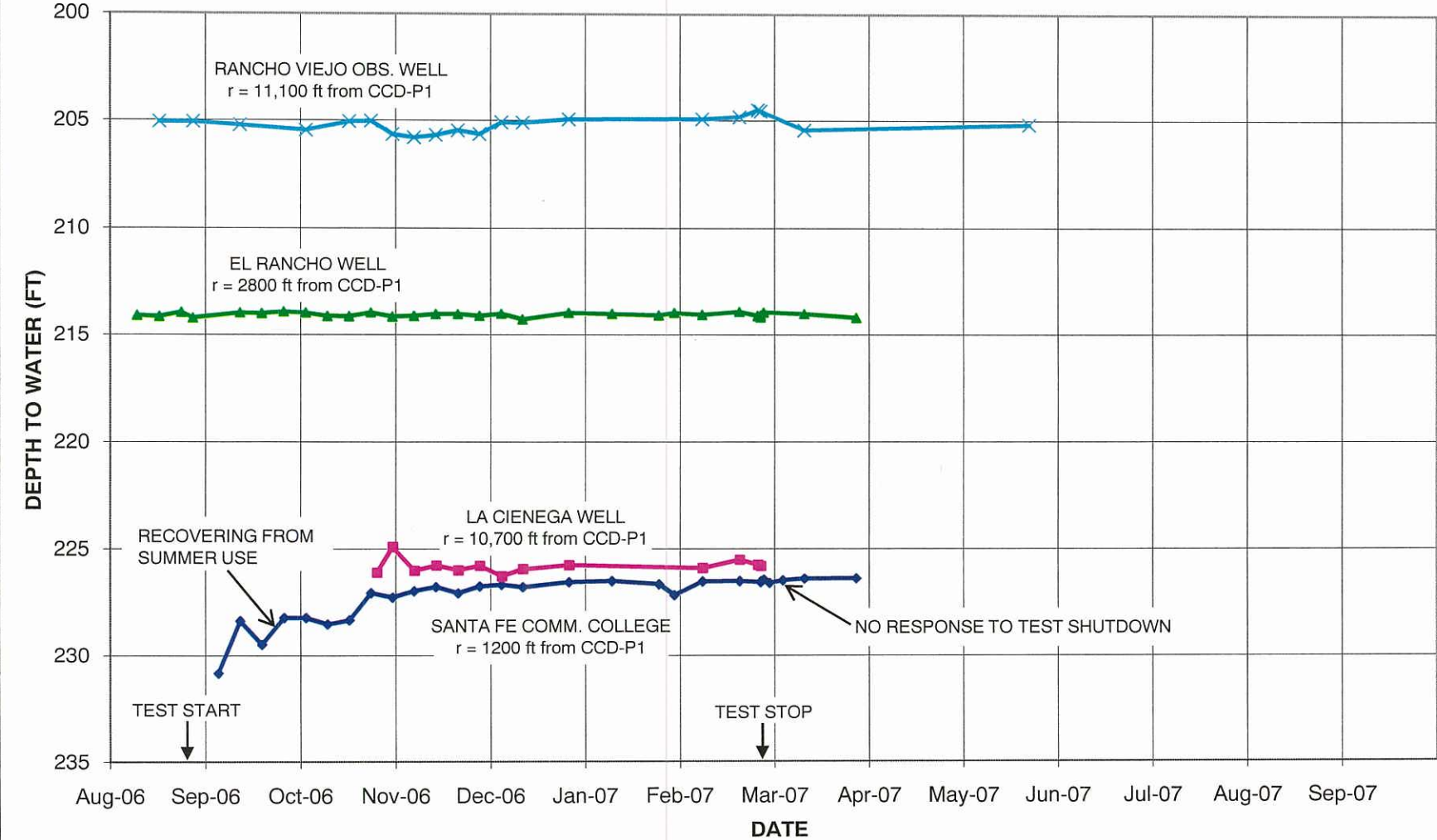


**FIGURE 14
HYDROGRAPHS OF SHALLOW PIEZOMETERS**



WATER PLAN

FIGURE 15
HYDROGRAPHS OF OUTLYING OBSERVATION WELLS



WATER PLAN

FIGURE 16
WATER-LEVEL BUILDUP VS. DISTANCE FROM INJECTION WELL

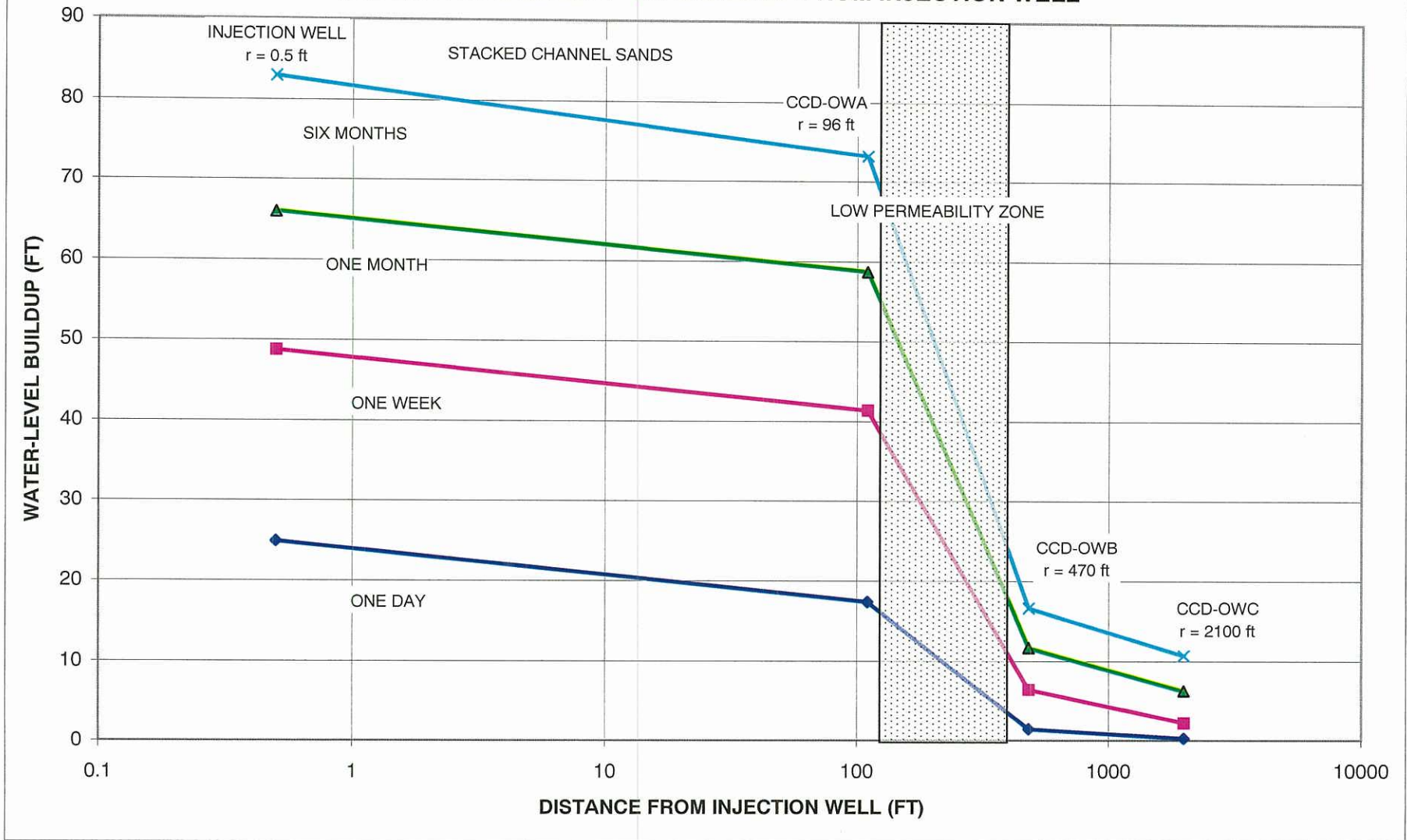


FIGURE 17
PUMPING AND INJECTION WELL WATER LEVELS AND TEMPERATURE

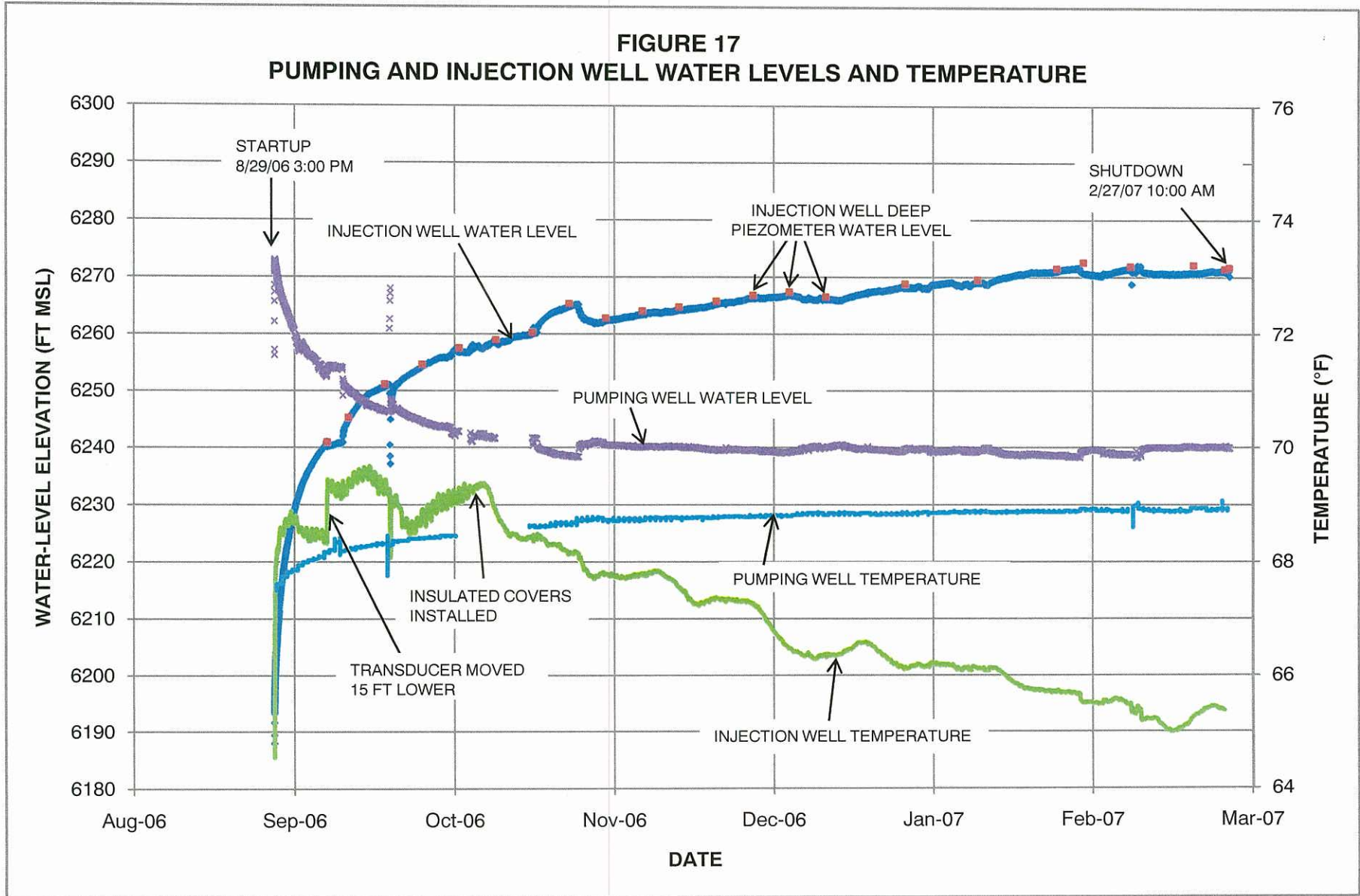


FIGURE 18
DIFFERENCE OF WATER-LEVEL BUILDUP IN INJECTION WELL, SHALLOW PIEZOMETER, AND
WELL CCD-OWA AND INJECTION WATER TEMPERATURE

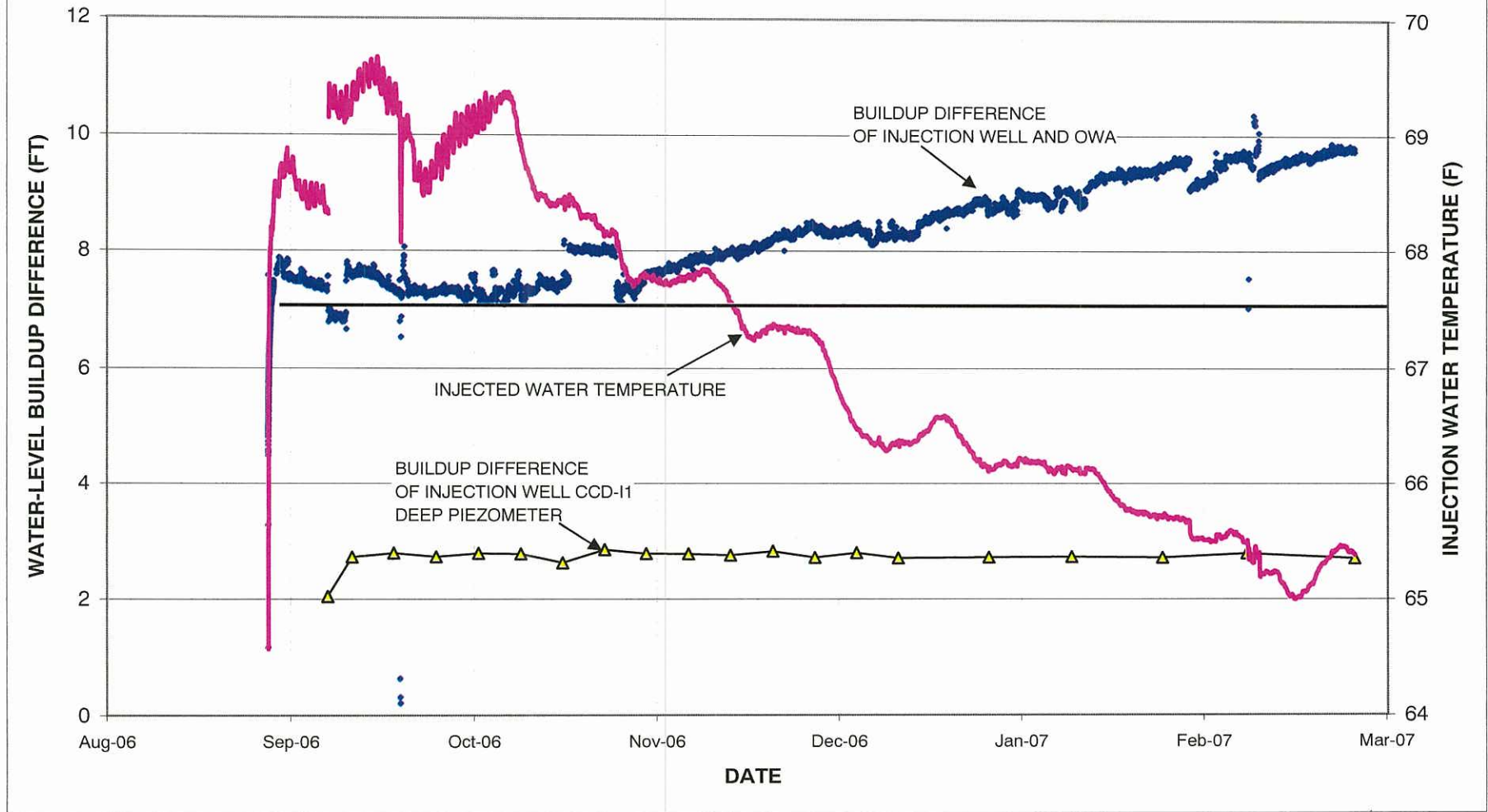


FIGURE 19
DRAWDOWN DIFFERENCE IN PUMPING AND EXPLORATORY WELLS

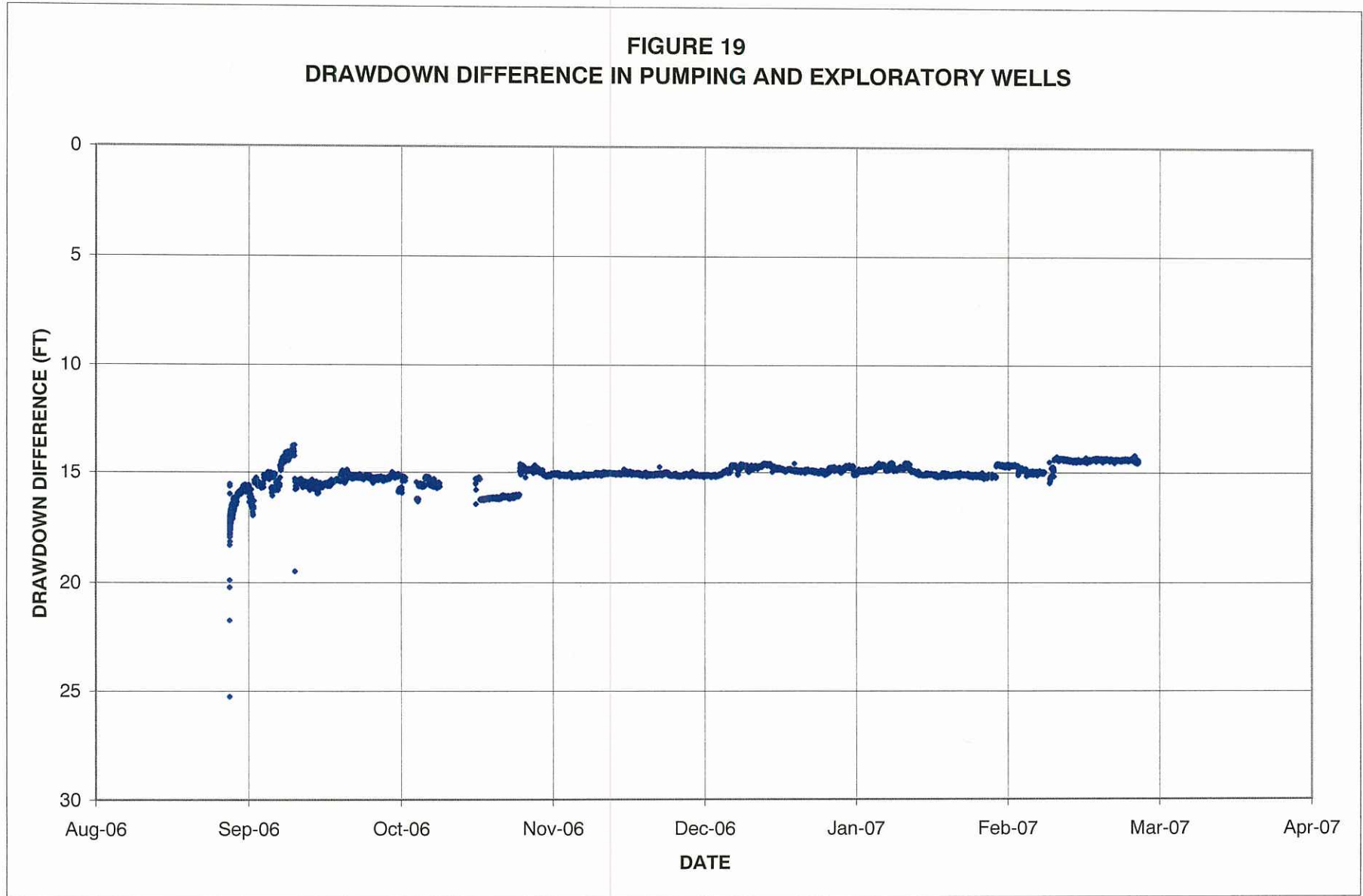
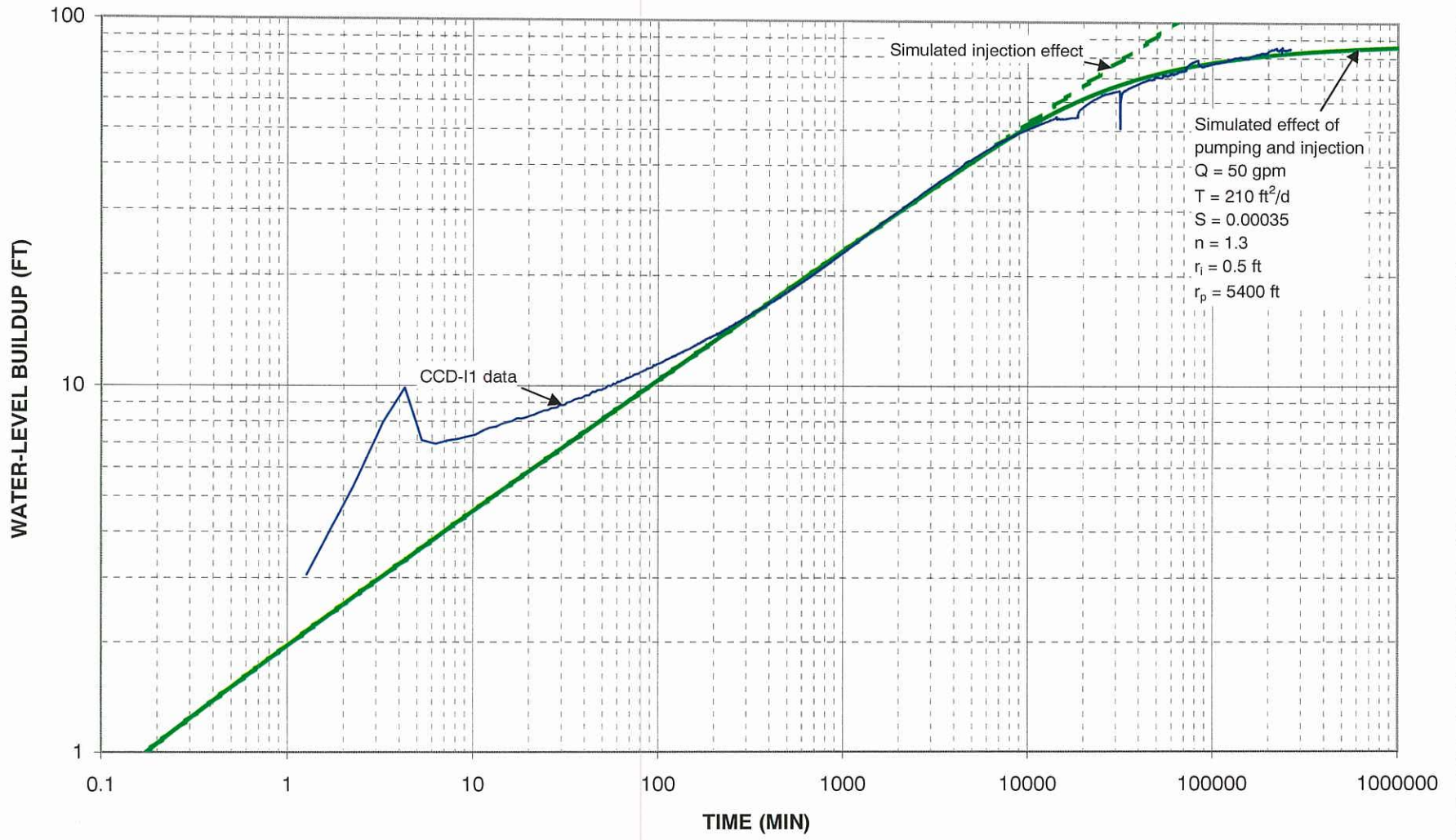
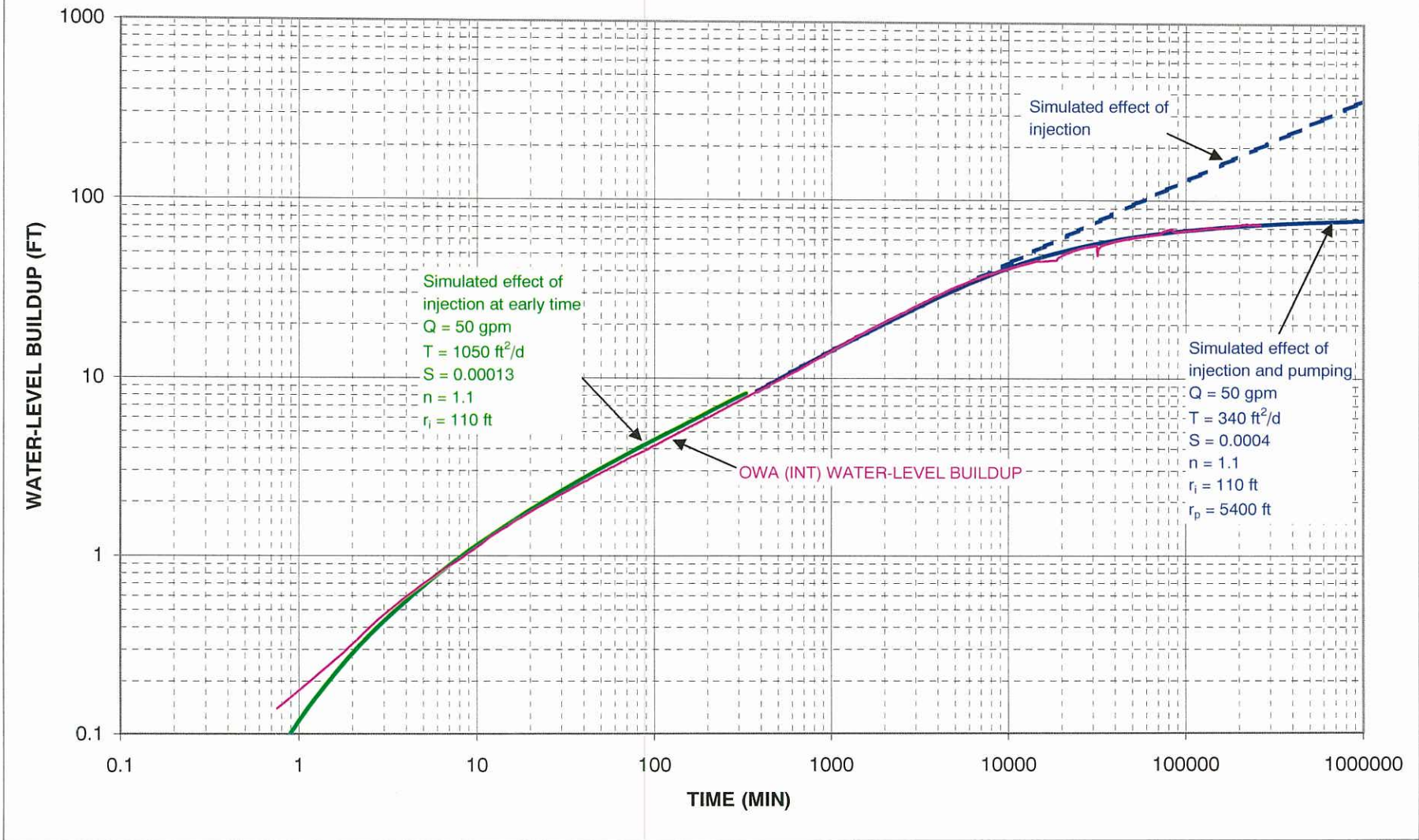


FIGURE 20
INJECTION WELL WATER-LEVEL BUILDUP AND GRF CURVE MATCH



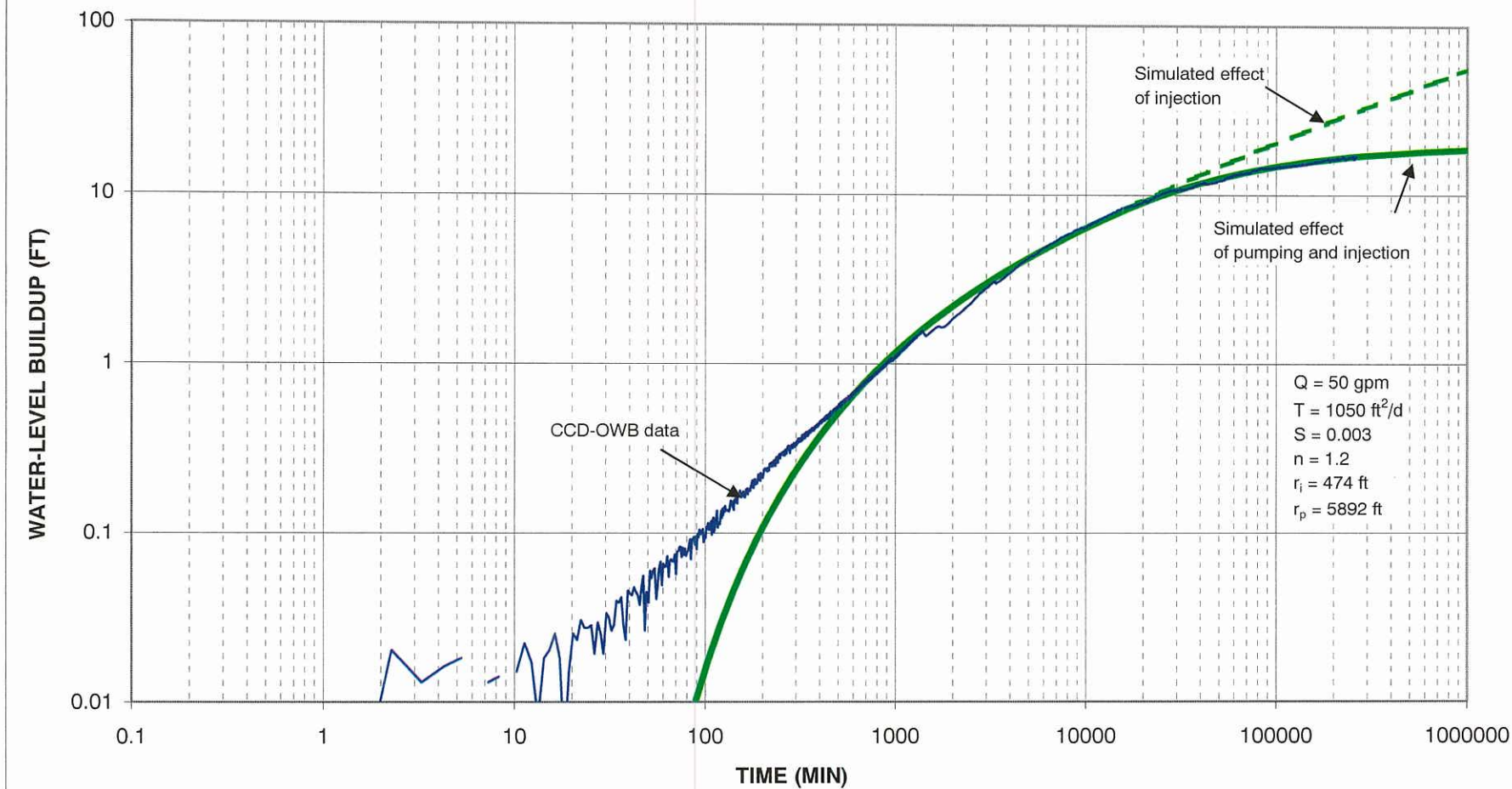
WATER PLAN

FIGURE 21
OBSERVATION WELL A WATER-LEVEL BUILDUP AND GRF CURVE MATCH



WATER PLAN

FIGURE 22
OBSERVATION WELL B WATER-LEVEL BUILDUP AND GRF CURVE MATCH



WATER PLAN

FIGURE 23
OBSERVATION WELL C WATER-LEVEL BUILDUP AND GRF CURVE MATCH

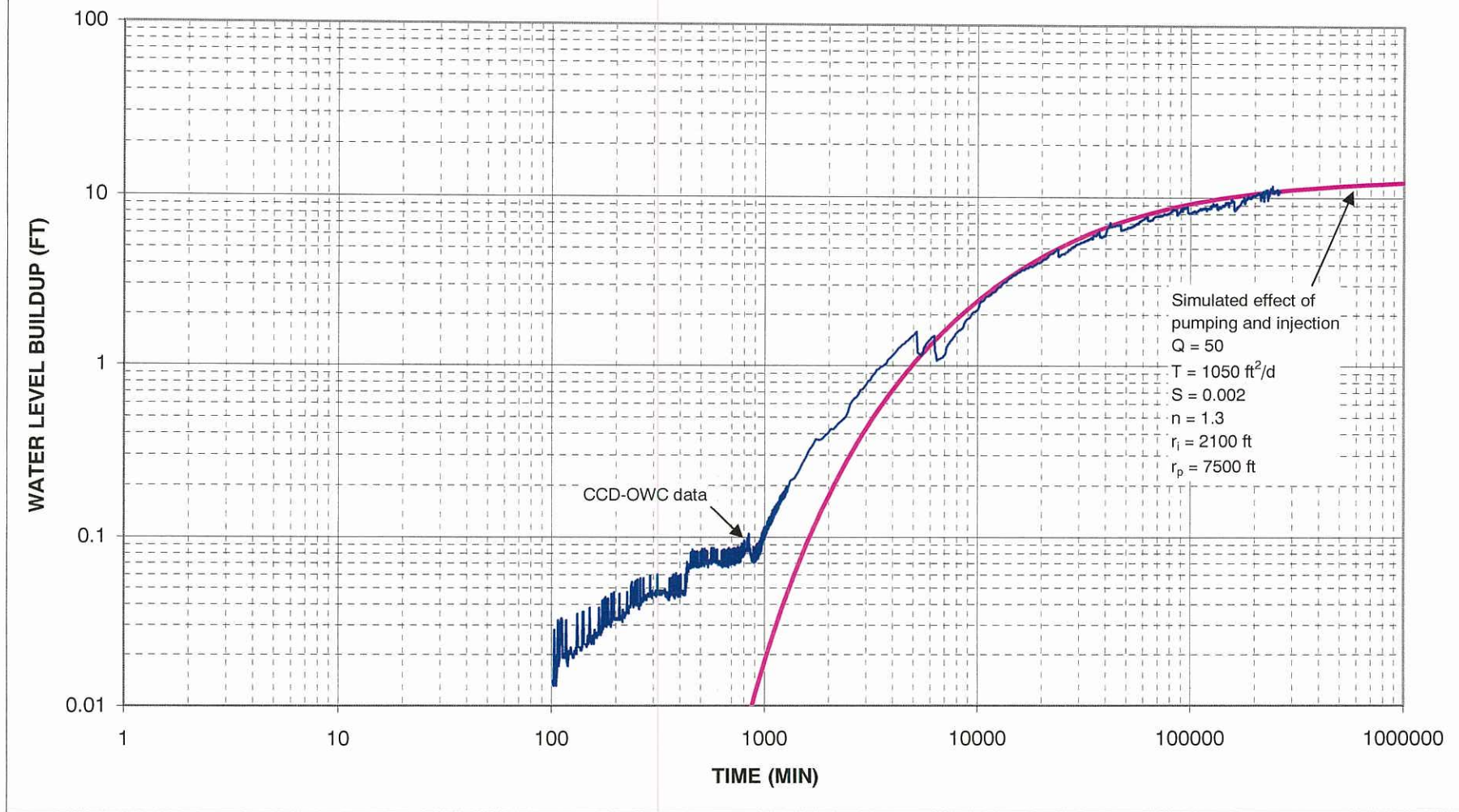


FIGURE 24
CCD-P1 DRAWDOWN AND GRF CURVE MATCH

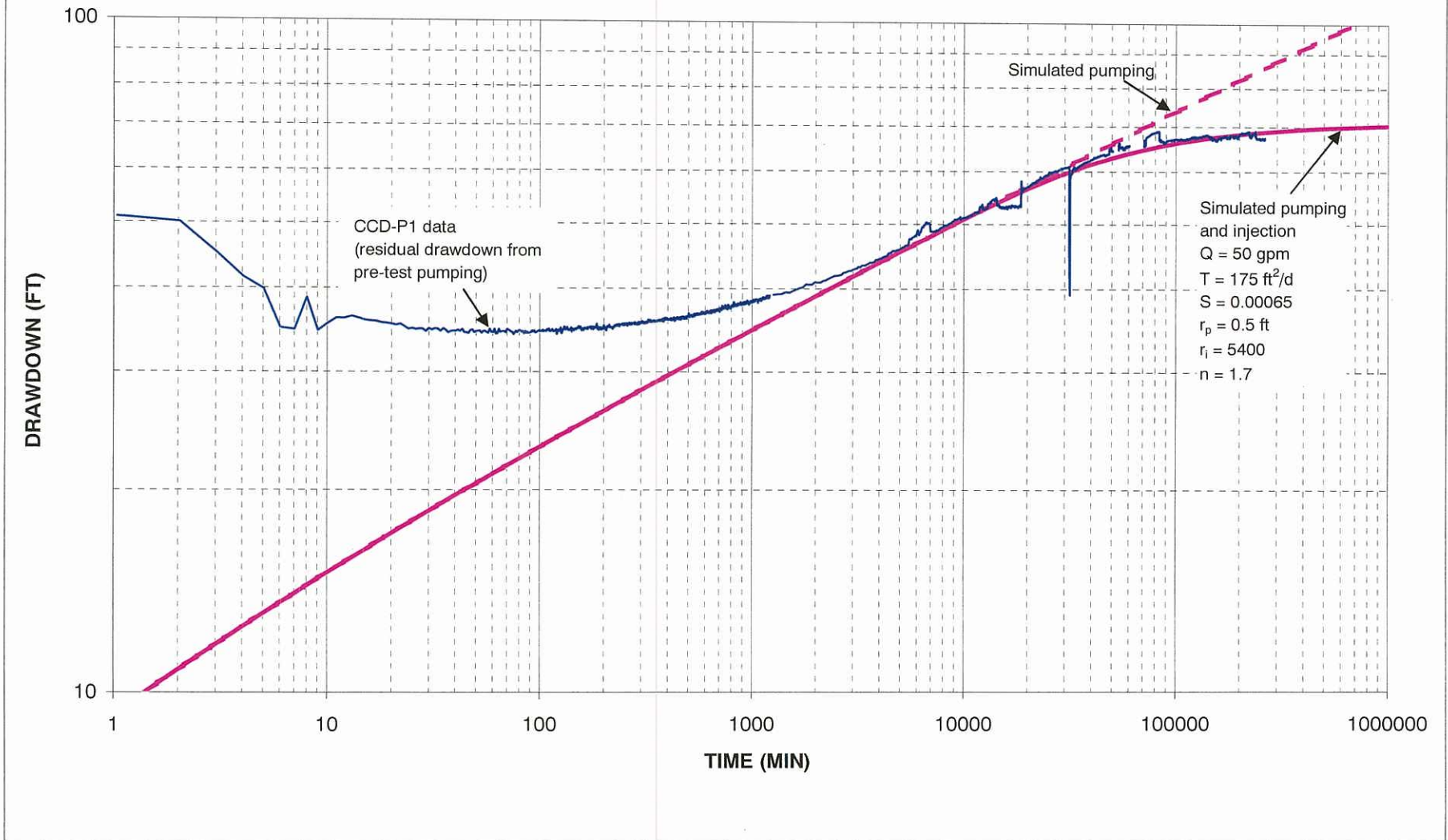


FIGURE 25
CCD-X1 DRAWDOWN AND GRF CURVE MATCH

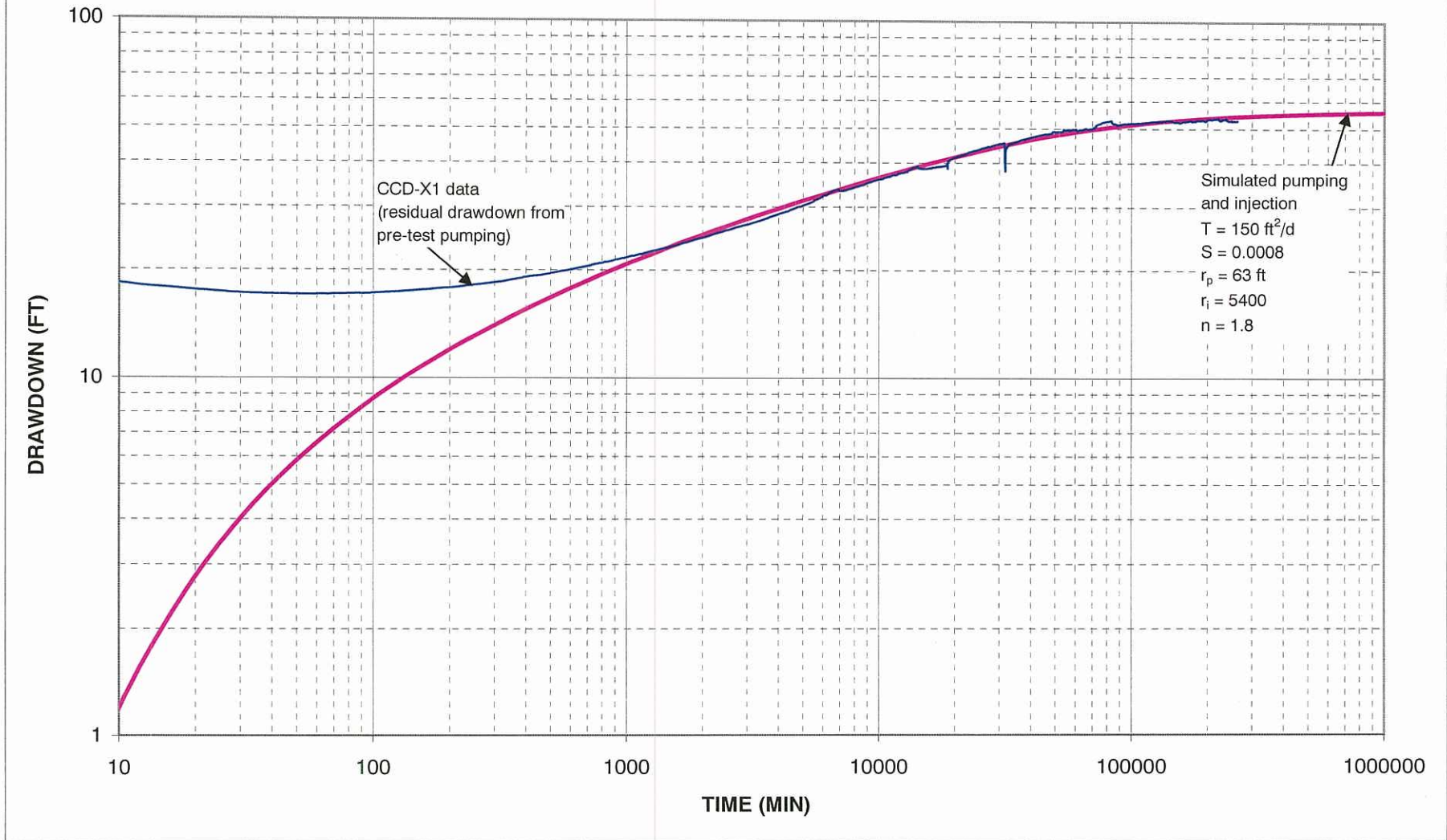


FIGURE 26
INJECTION WELL RECOVERY AND GRF CURVE MATCH

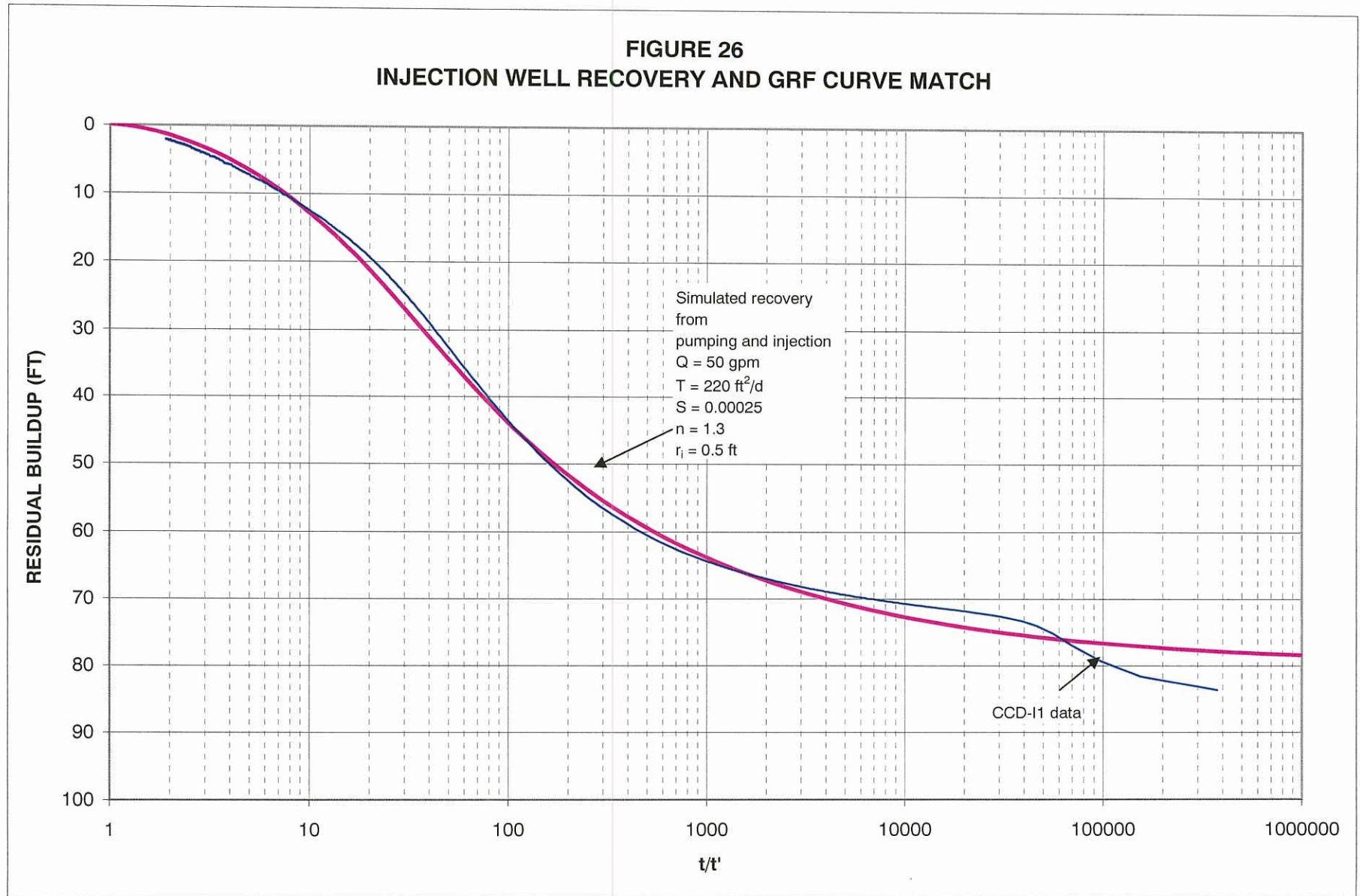


FIGURE 27
OBSERVATION WELL A RECOVERY AND GRF CURVE MATCH

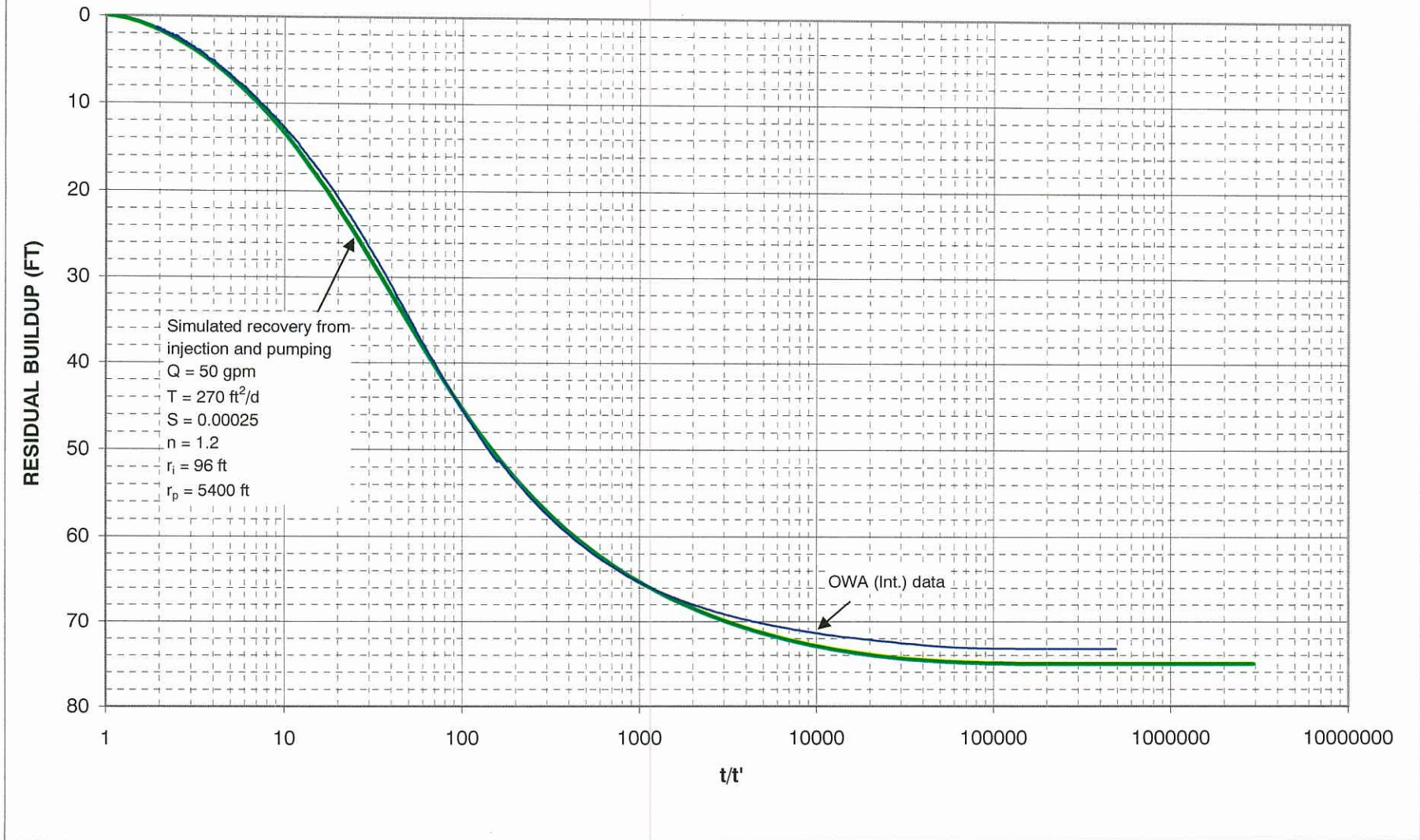


FIGURE 28
OBSERVATION WELL B RECOVERY AND GRF CURVE MATCH

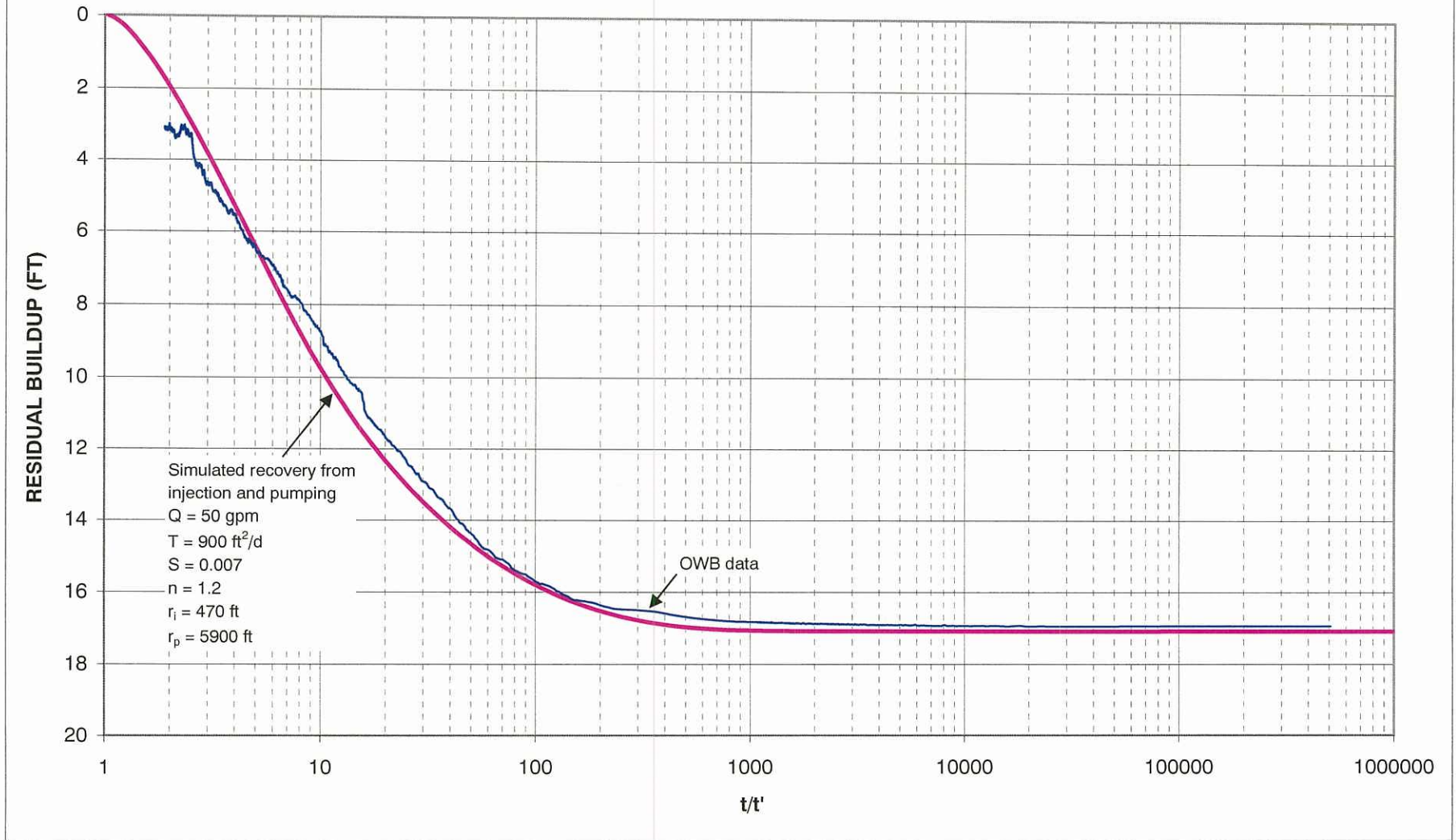


FIGURE 29
OBSERVATION WELL C RECOVERY AND GRF CURVE MATCH

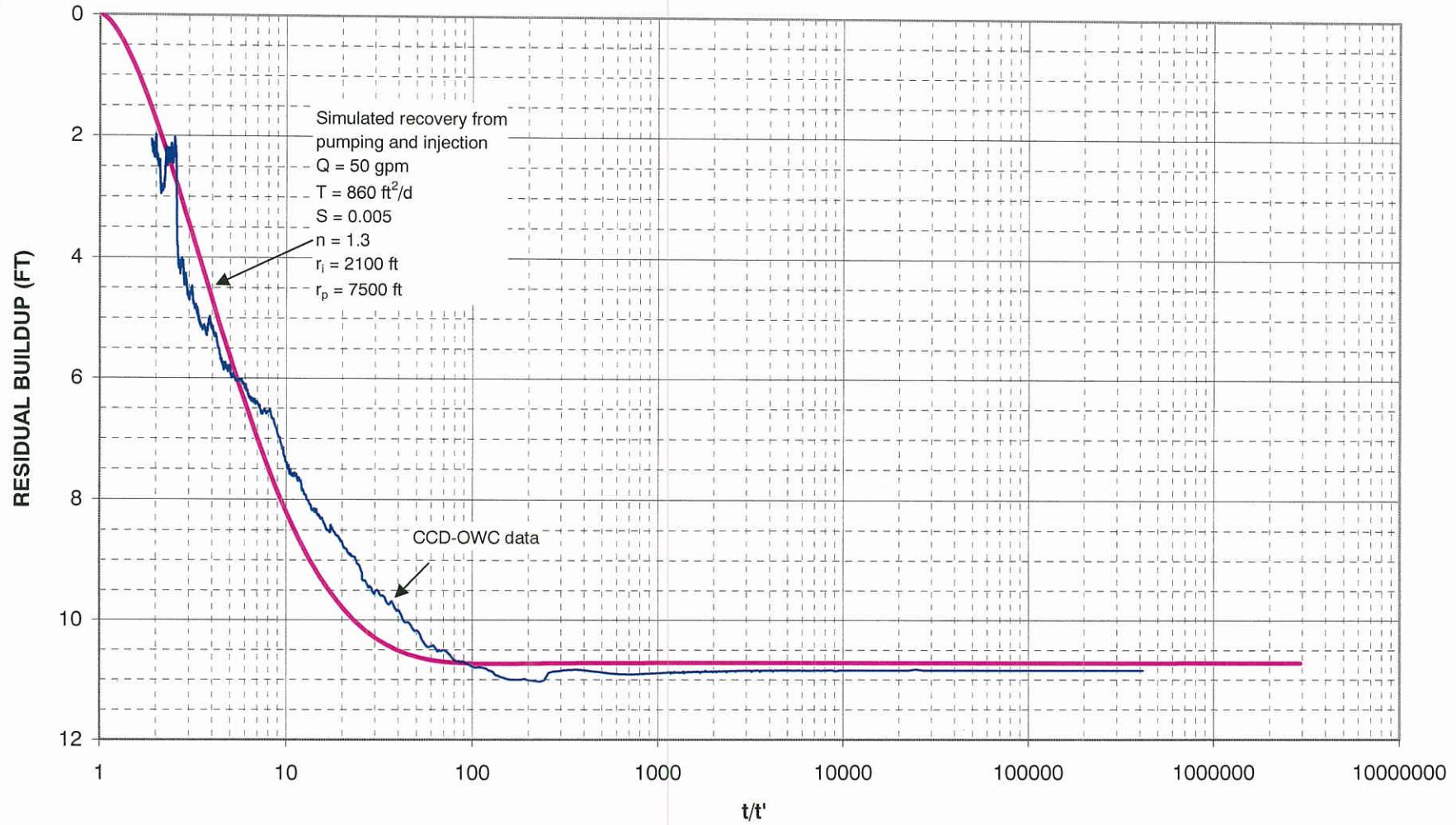


FIGURE 30
CCD-P1 RECOVERY AND GRF CURVE MATCH

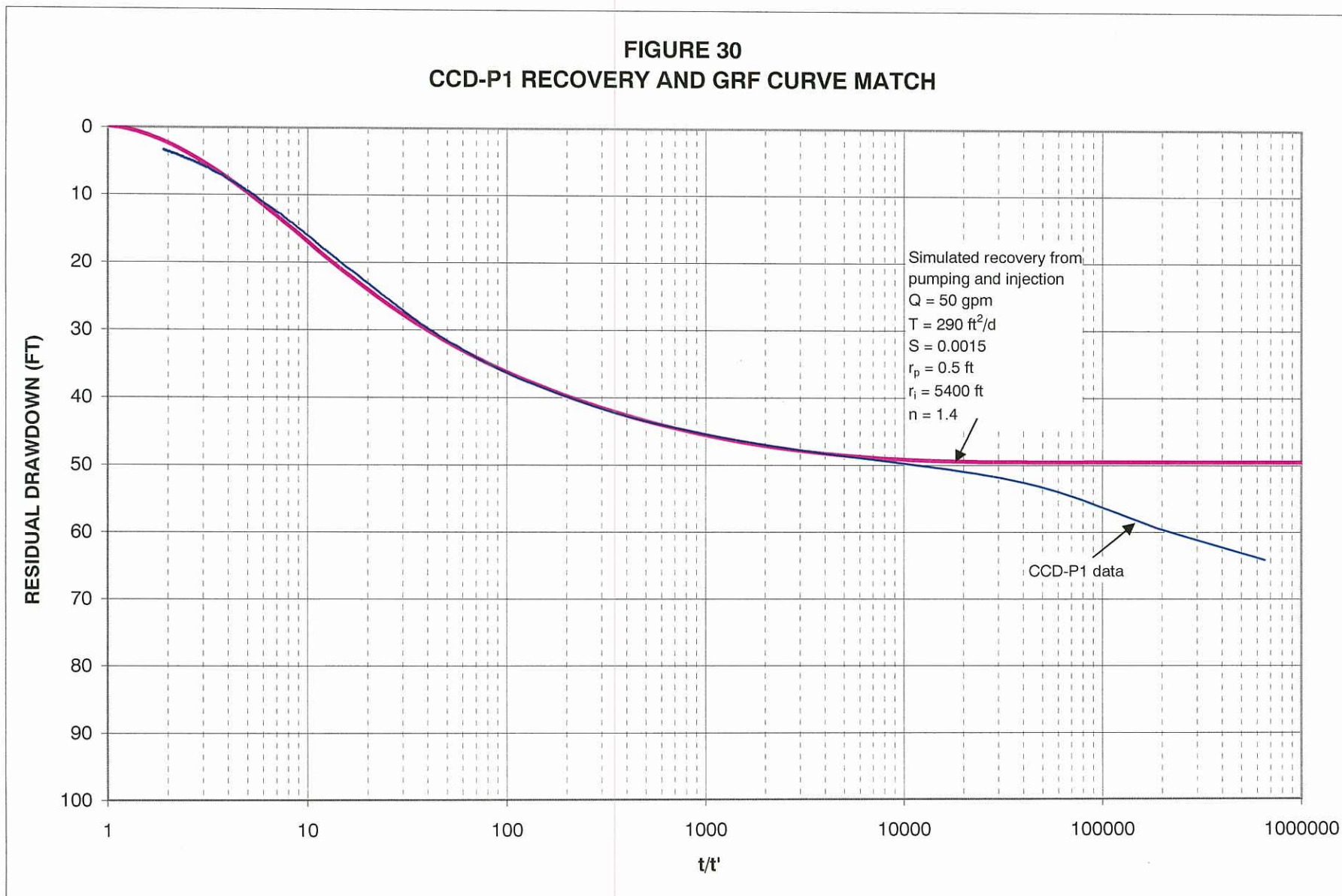
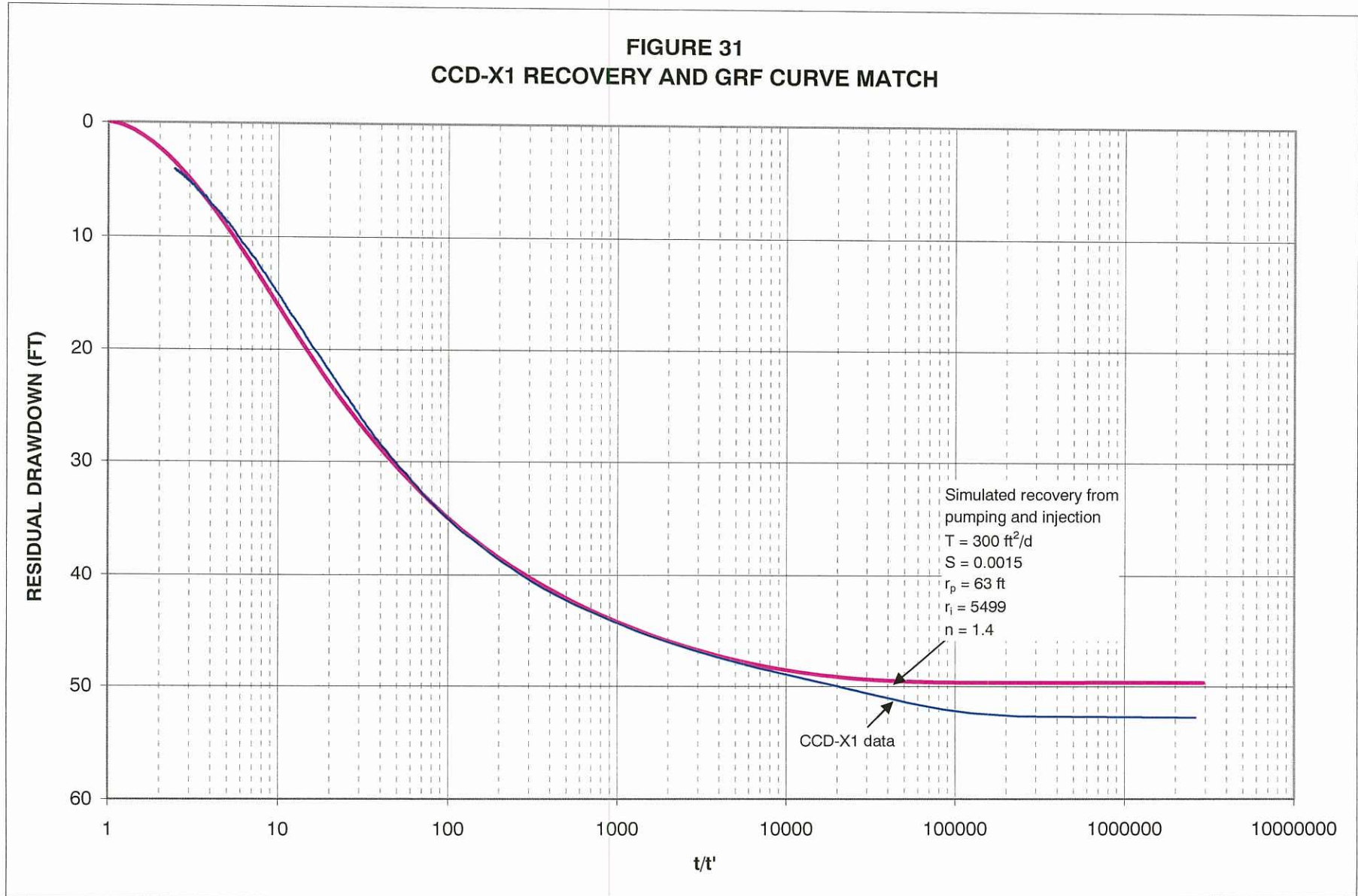
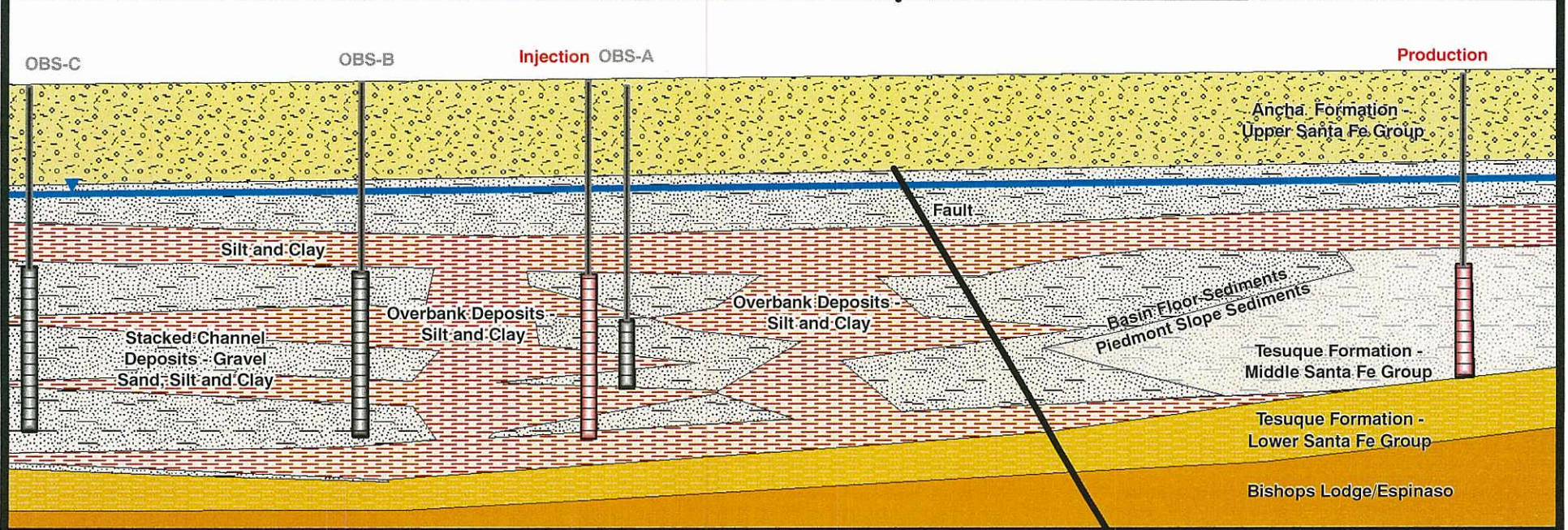
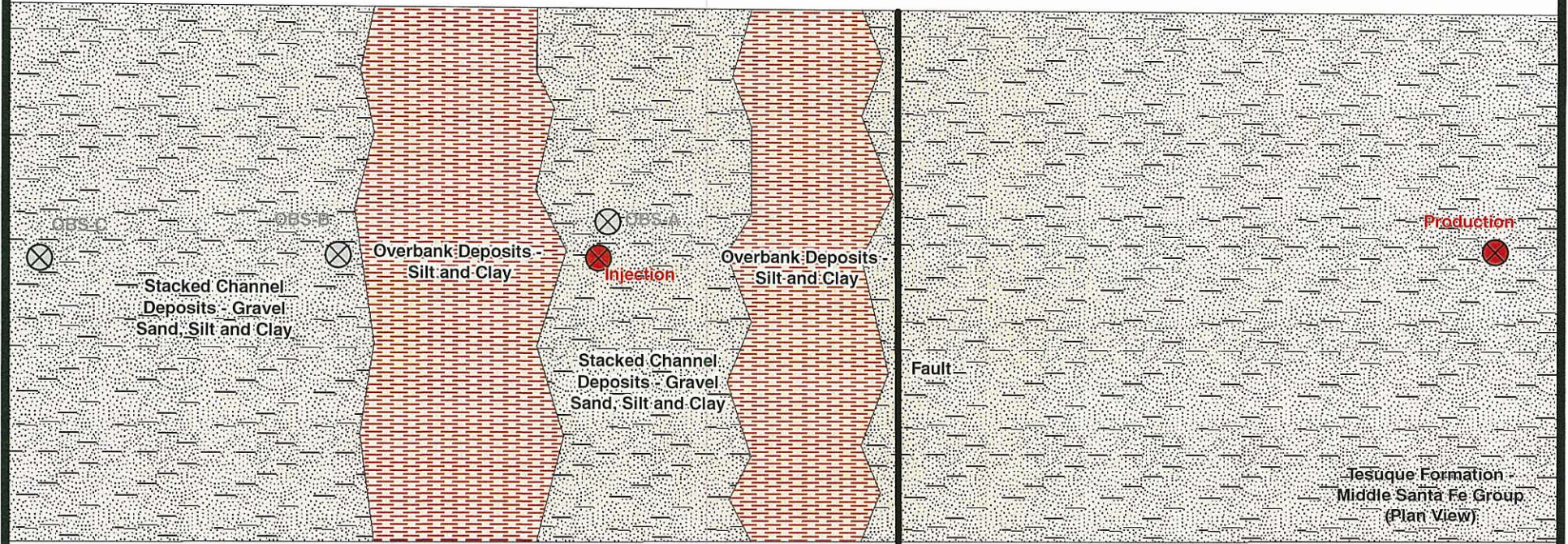


FIGURE 31
CCD-X1 RECOVERY AND GRF CURVE MATCH



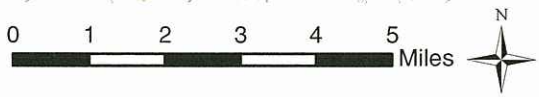
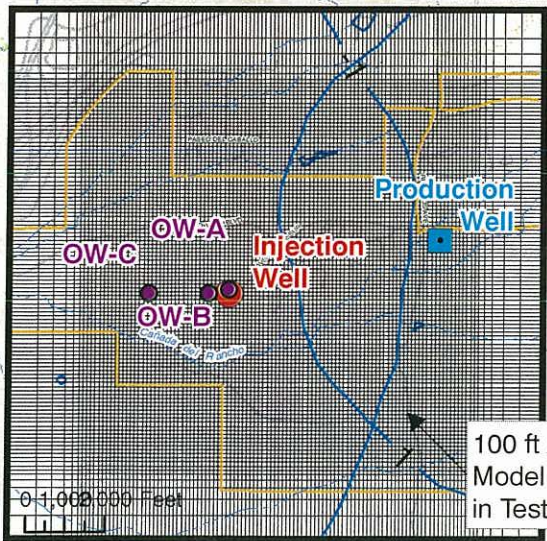
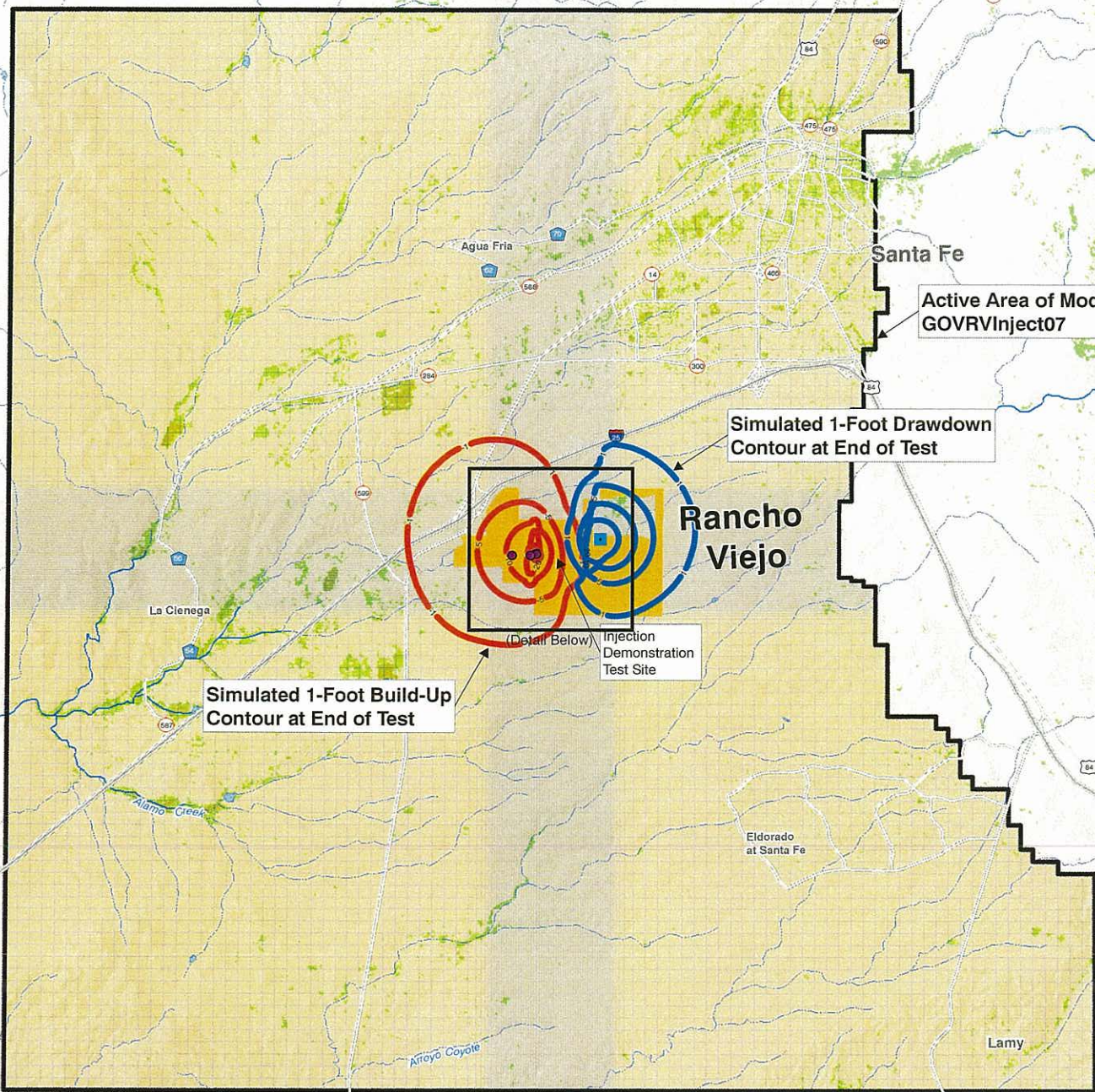
RANCHO VIEJO WATER PLAN

FIGURE 32 GEOLOGIC CONCEPTUAL MODEL



186 COLUMNS

186 ROWS

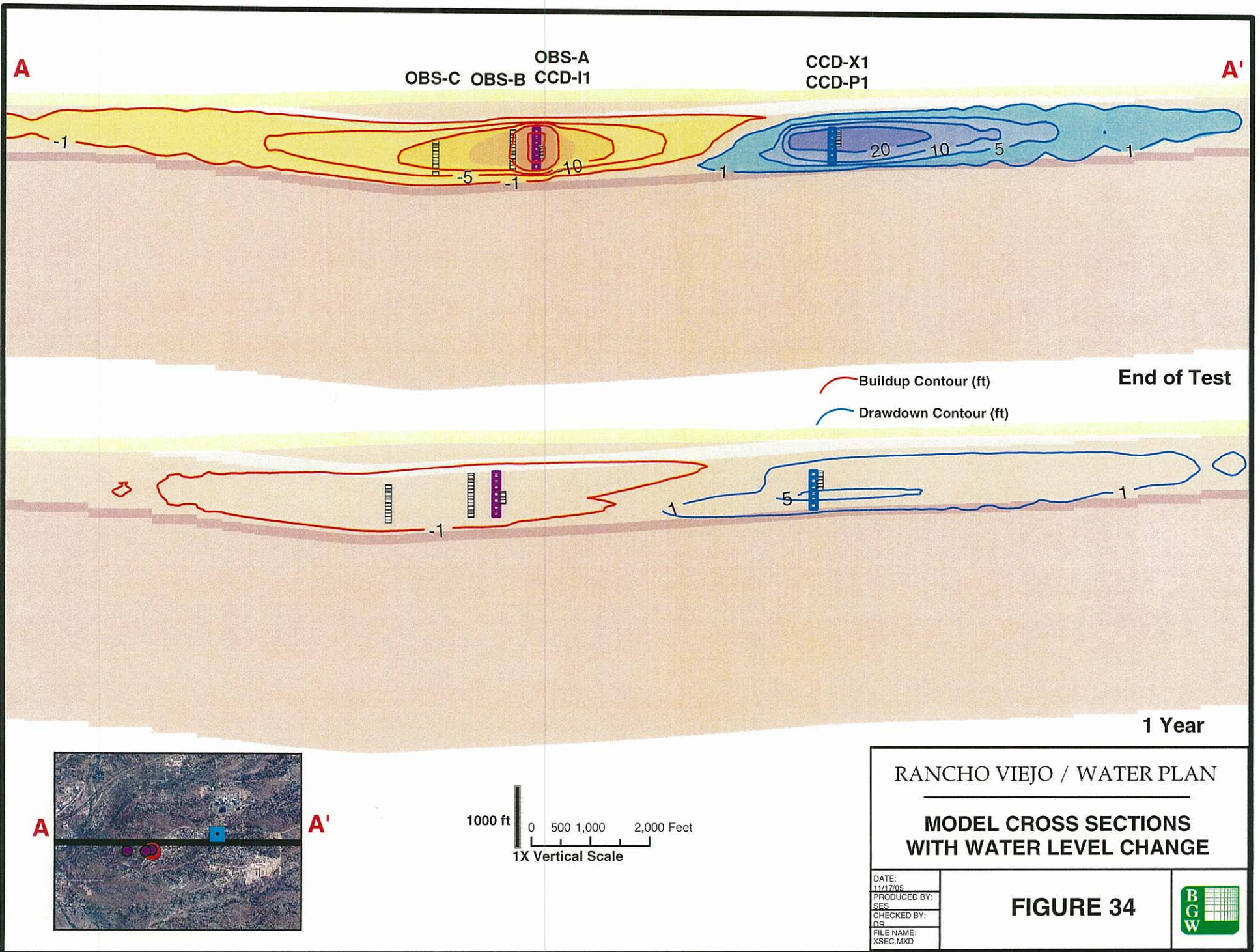


RANCHO VIEJO / WATER PLAN
GROUNDWATER MODEL GRID AND SIMULATED WATER-LEVEL CHANGE

DATE: 07/12/2005
 PRODUCED BY: SES
 CHECKED BY: CC
 FILE NAME: JSAJ_MDL_GRID.MXD

FIGURE 33





WATER PLAN

FIGURE 35
OBSERVED AND SIMULATED BUILD-UP AT CCD-OWA

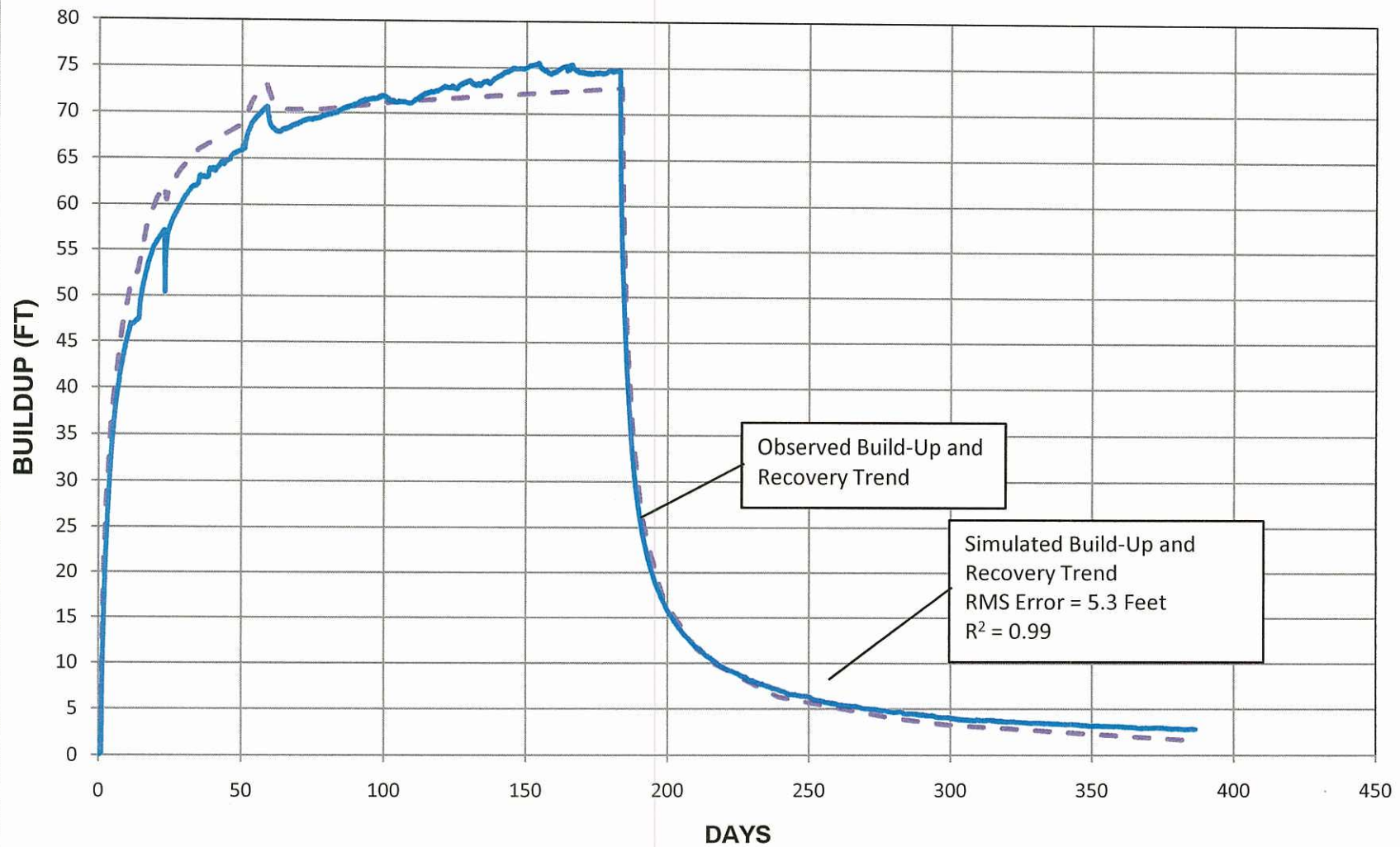
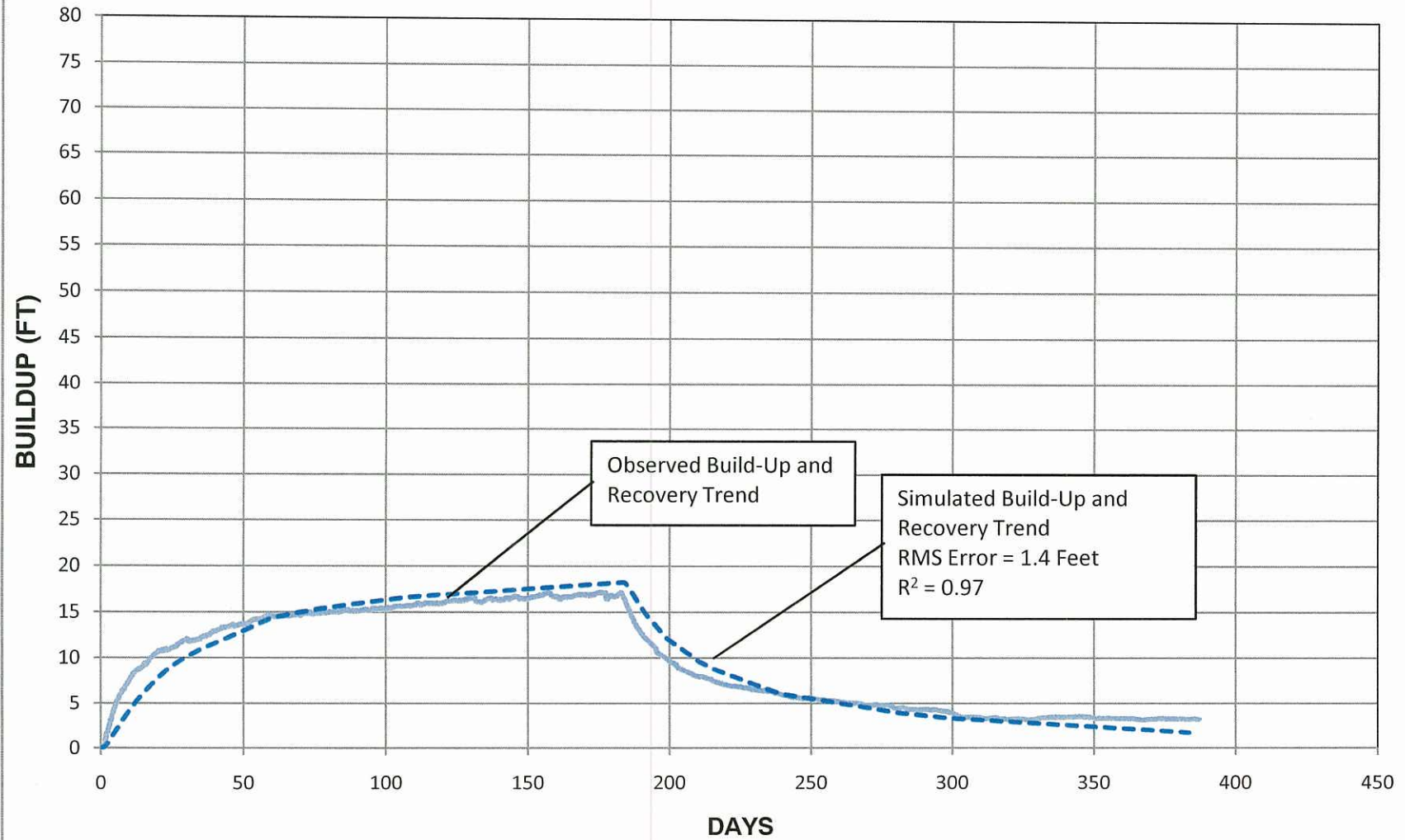
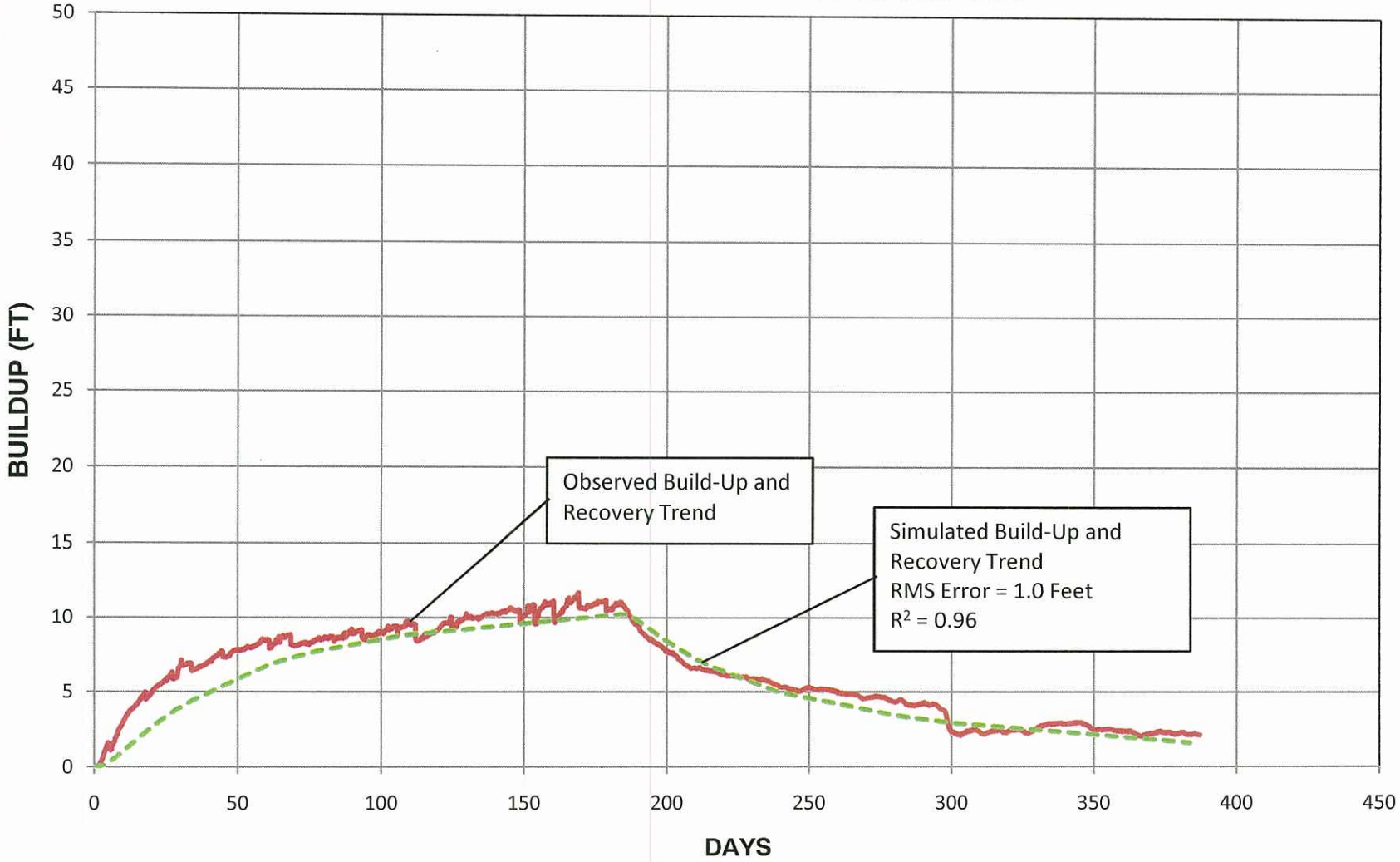


FIGURE 36
OBSERVED AND SIMULATED BUILD-UP AT CCD-OWB



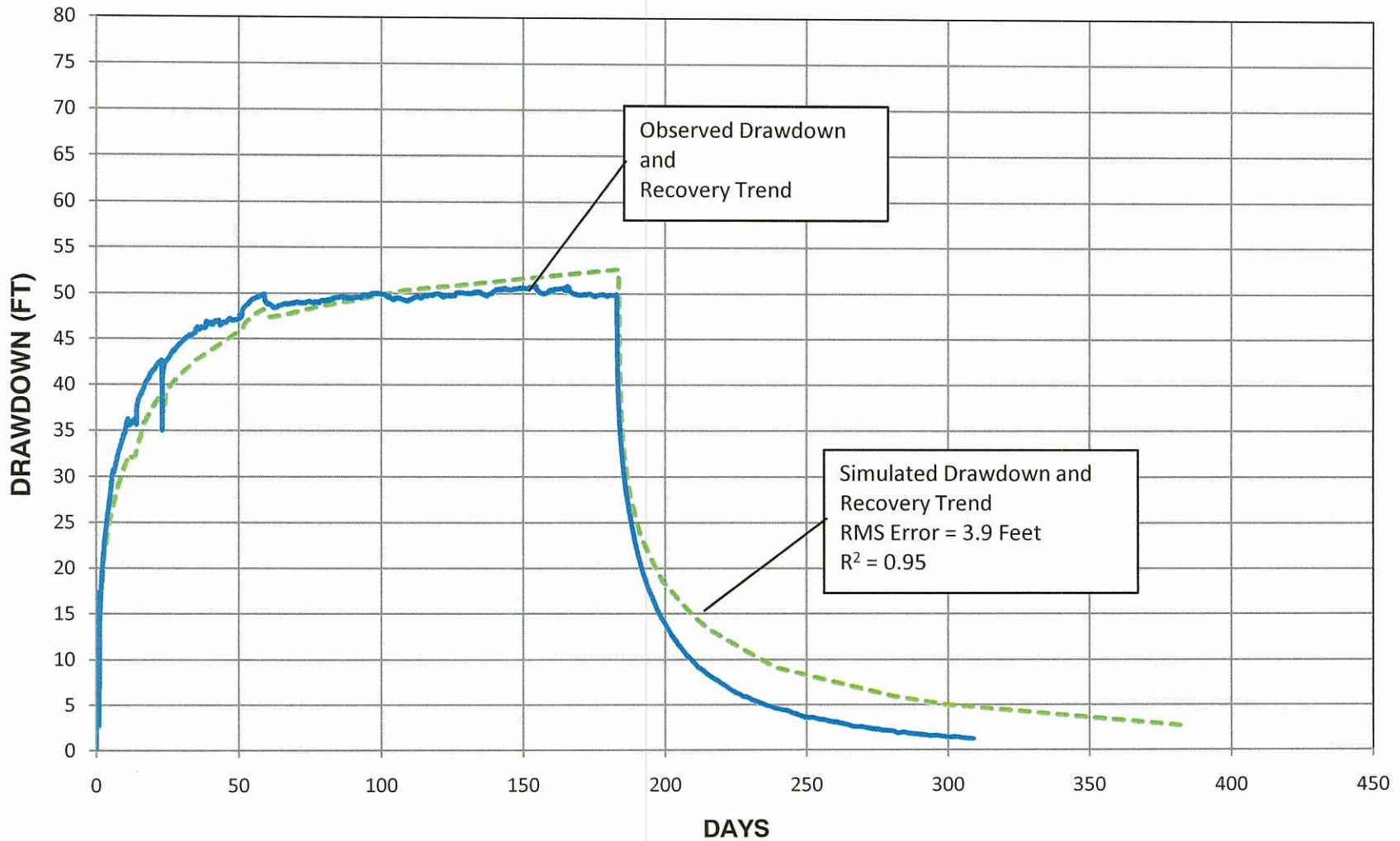
WATER PLAN

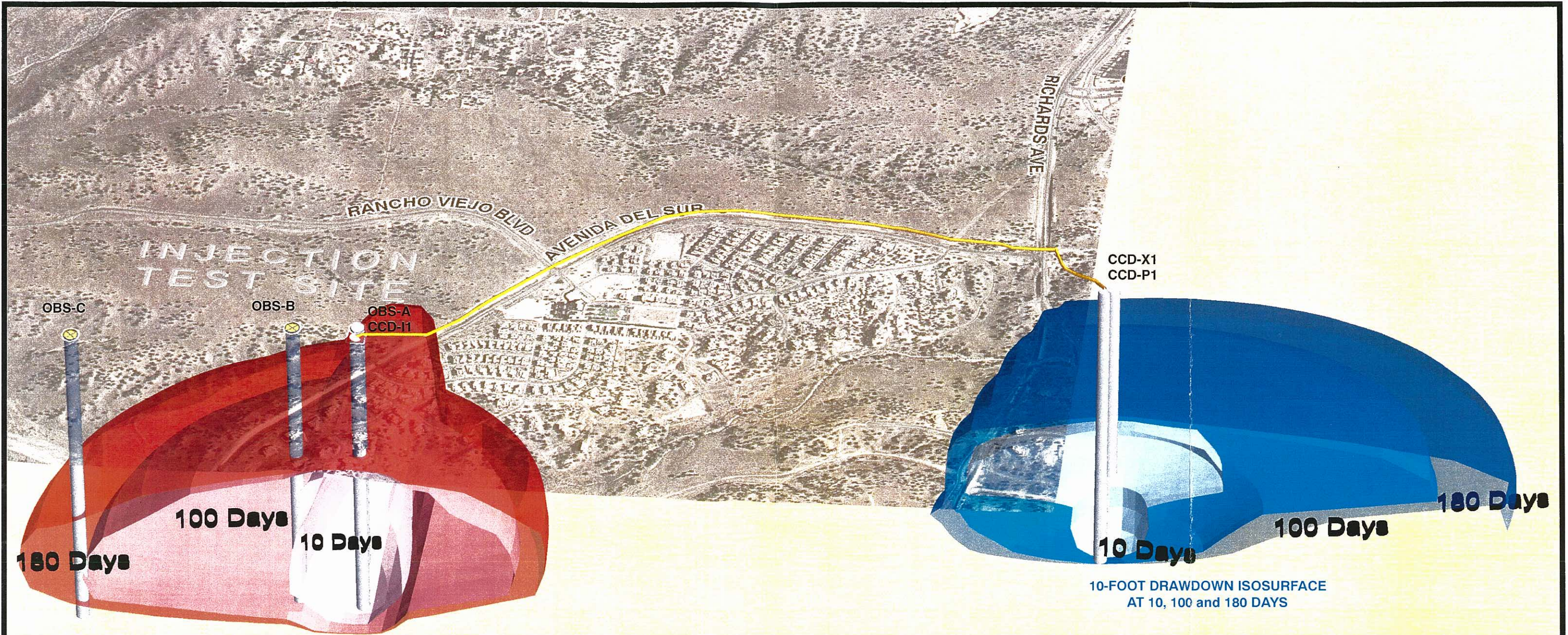
FIGURE 37
OBSERVED AND SIMULATED BUILD-UP AT CCD-OWC



WATER PLAN

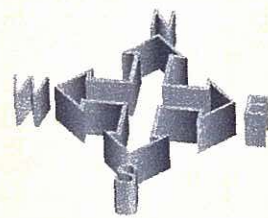
FIGURE 38
OBSERVED AND SIMULATED DRAWDOWN AT CCD-X1





10-FOOT BUILD-UP ISOSURFACE
AT 10, 100 and 180 DAYS

10-FOOT DRAWDOWN ISOSURFACE
AT 10, 100 and 180 DAYS



500 FT

500 FT

RANCHO VIEJO / WATER PLAN
ISOSURFACES OF MODELED
INJECTION AND PUMPING
RESPONSE

DATE:
11/17/05
PRODUCED BY:
SES
CHECKED BY:
DB
FILE NAME:
XSEC.MXD

FIGURE 39



APPENDIX A

AGENCY APPROVALS



STATE OF NEW MEXICO

OFFICE OF THE STATE ENGINEER

Santa Fe

John A. D'Antonio Jr., P.E.
State Engineer

BATAAN MEMORIAL BUILDING, ROOM 102
SANTA FE, NEW MEXICO 87504-5102
(505) 827-8120
FAX: (505) 827-8882

November 17, 2005

Rancho Viejo de Santa Fe, Inc.
Isaac Pino, P.E., General Manager
P.O. Box 4458
Santa Fe, NM 87502

Re: *Conditional Authorization to Proceed with Temporary Diversion from Well No. RG-38073—Expl. 5*

Dear Mr. Pino:

In our desire to support innovative water related research, which may benefit the public, the Office of the State Engineer ("OSE") is authorizing temporary use of well No. RG-38073—Expl. 5, for diversion of up to forty (40) acre-feet of water, contingent upon the formal withdrawal by Rancho Viejo de Santa Fe, Inc. ("Rancho Viejo") of Application RG-2310, RG-12312, and RG-12313 (Consolidated) into RG-38073—Expl. 5, and further subject to the following specific requirements:

1. Prior to any diversion of water, Rancho Viejo shall obtain appropriate permits as mandated by the New Mexico Environment Department for injection of water into an aquifer.
2. Prior to any diversion of water, Rancho Viejo shall obtain written verification or documentation from Santa Fe County of full compliance with any pertinent County regulations or ordinances governing the diversion of water in the Community College District.
3. Prior to any diversion of water, Rancho Viejo shall provide to the OSE written documentation of compliance with above items numbered 1 and 2.
4. Well No. RG-38073—Expl. 5 shall be equipped with a totalizing meter, installed at the wellhead before any distribution line branch.
5. Prior to any diversion of water, the OSE shall be notified in writing of the make, model, serial number, units, multiplier, and number of free moving dials of the above described totalizing meter.
6. Rancho Viejo shall obtain an exploratory permit from the OSE for the project's injection well and permits for the drilling of all monitor wells, observing all applicable well construction rules and regulations.
7. The injection well shall be equipped with a totalizing meter, which shall be installed at a location and in a manner acceptable to the OSE.

8. Prior to any injection of water, the OSE shall be notified in writing of the make, model, serial number, units, multiplier, and number of free moving dials of the totalizing meter required under item number 7.
9. Prior to any diversion of water under this authorization, well No. RG-38078—Expl. 5, the injection well, and all project observation wells proximal to the diversion and injection wells shall be completed and equipped with continuous recording water level piezometers, installed and operated in a manner acceptable to the OSE.
10. The monitoring well network shall be designed to be capable of measuring all pumping and injection effects in such a manner as to determine any impacts on existing water rights.
11. Prior to any diversion of water, Rancho Viejo shall notify the OSE by Certified Mail of the date of first diversion of water under this authorization.
12. This authorization shall expire on December 31, 2006 or six (6) months from the date of first diversion, as documented above in item number 10, whichever occurs first.
13. Records of the amount of water diverted from well No. RG-38073—Expl. 5, and the amount of water injected into the aquifer shall be submitted to the Santa Fe Office of the State Engineer on or before the 10th day of each month for the preceding calendar month.
14. All water diverted from well No. RG-38073—Expl. 5 shall be injected back into the same hydro-geologic strata from which it was diverted (as documented by means of well samples, geophysical well log and cross sectional data).
15. No water shall be put to beneficial use or consumed under this authorization. If the quantity of water injected is less than the quantity of water diverted, Rancho Viejo shall offset any operational loss or other loss of water in a manner acceptable to the OSE.
16. Copies of all technical data and interpretations developed during this study shall be promptly provided to the OSE.

Please be aware that, although Rancho Viejo is highly encouraged to work with OSE Hydrology Bureau staff in designing its project and conducting the study, by granting this authorization the OSE neither endorses or validates the study or the results obtained there from.

I will anticipate receipt of the required Environment Department and County authorizations, the data for the totalizing meters, as well as the notification of the first day of diversion.

Please contact me if further discussion of this matter is needed. I can be reached at 827-4187.

Sincerely,


John T. Romero, P.E.

Director, Water Resource Allocation Program

cc: John R. D'Antonio, Jr., P.E., New Mexico State Engineer
Jim Sizemore, P.E., Water Right Director
Charles T. DuMars, J.D.
Richard Martinez, DFA-Capital Projects
Richard Rose, P.E., NM Environmental Dept.
Gerald T.E. Gonzalez, Santa Fe County Manager



BILL RICHARDSON
GOVERNOR

State of New Mexico
ENVIRONMENT DEPARTMENT

Ground Water Quality Bureau

Harold Runnels Building

1190 St. Francis Drive, P.O. Box 26110

Santa Fe, New Mexico 87502-6110

Telephone (505) 827-2918

Fax (505) 827-2965



RON CURRY
SECRETARY

DERRITH WAICHMAN-MOORE
DEPUTY SECRETARY

COPY

JAN 09 2006

CERTIFIED MAIL - RETURN RECEIPT REQUESTED

January 4, 2006

Isaac Pino P.E.,
Vice President & General Manager
Rancho Viejo del Santa Fe, Inc.
55 Cañada del Rancho
Santa Fe, NM 87508

**RE: Response to Notice of Intent to Discharge for the Pilot Injection Well,
Rancho Viejo Aquifer Recharge Project**

Dear Mr. Pino:

The New Mexico Environment Department (NMED) received a Notice of Intent to discharge for the Rancho Viejo Aquifer Recharge Project Pilot Injection Well on November 30, 2005. The notice satisfies the requirements of Section 20.6.2.1201.B of the New Mexico Water Quality Control Commission (WQCC) Regulations (20.6.2 NMAC). The proposed discharge is located approximately 2 miles south of the City of Santa Fe in Section 29, T16N, R9E, Santa Fe County

Based on the information provided in your Notice of Intent, NMED has determined that a Discharge Permit is not required as long as the discharge is as described. The discharge is exempt from the Discharge Permit requirement pursuant to Section 20.6.2.3105.D NMAC because the information provided indicates that the discharge is the result of the transport of water diverted and that the water diverted has not had added to it after the point of diversion any effluent received from a sewerage system and the secretary has not determined that a hazard to public health may result.

The exempt discharge is briefly described as follows:

Up to 50 gallons per minute of Tesuque Formation ground water will be pumped from the Community College District Production Well (CCDP1), piped about 1 mile and returned to the Tesuque Formation through an injection well constructed for the purpose. The total project duration is limited to a six-month period. Injected water is anticipated to have a similar chemical

Isaac Pino, No DP Required for Rancho Viejo Pilot Well

1/4/06

p. 2

composition to the water of the receiving aquifer. No water contaminants are added to the diverted water and no increase to the weight of water contaminants is anticipated. Measures are taken to prevent chemical changes from occurring during withdrawal, transport and re-injection. Water will be withdrawn and re-injected at correlative stratigraphic intervals. The project will provide a hydrologic assessment of the feasibility of a full-scale aquifer recharge system.

Although a Discharge Permit is not being required for this discharge at this time, you are not relieved of liability should your operation result in actual pollution of surface or ground waters. Further, this decision by NMED does not relieve you of your responsibility to comply with any other applicable federal, state, and/or local laws and regulations, such as zoning requirements, plumbing codes and nuisance ordinances.

If at some time in the future you intend to change the amount, character or location of your discharge, or if observation or monitoring shows that the discharge is not as described in your Notice of Intent or that unforeseen impacts to ground water quality are resulting from your activities, you must file a revised Notice of Intent with the Ground Water Quality Bureau. To this end, NMED requests that information resulting from the project be provided to NMED in a timely manner to verify that ground water impacts are not occurring from the pilot project activities.

If you have any questions, please contact either Robert George, Domestic Waste Team Leader of the Ground Water Pollution Prevention Section at (505) 476-3648 or George Schuman, Program Manager of the Ground Water Pollution Prevention Section, at 505-827-2900.

Sincerely,

George Schuman for W. Olson

William C. Olson, Chief
Ground Water Quality Bureau

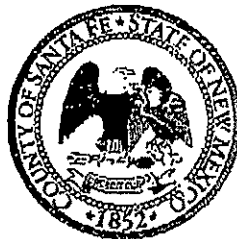
WO:RJG/rg

cc: Andy Edmonson, NMED Construction Programs Bureau
John T. Romero, Office of the State Engineer
Cecilia Williams, District Manager, NMED District II
NMED Santa Fe Field Office
NOI File
County File

Harry B. Montoya
Commissioner, District 1

Virginia Vigil
Commissioner, District 2

Michael D. Anaya
Commissioner, District 3



Paul Campos
Commissioner, District 4

Jack Sullivan
Commissioner, District 5

Gerald E. González
County Manager

March 1, 2006

Issac Pino, P.E.
General Manager
Rancho Viejo de Santa Fe, Inc
P.O. Box 4458
Santa Fe, NM 87502

Re: Temporary Diversion from well No. RG-38073

Dear Mr. Pino:

You have requested that Santa Fe County address those matters identified in the letter of November 17, 2005 of the State Engineer. You sought the authorization of the Office of the State Engineer to divert an amount of water not to exceed 40 acre-feet Well No. RG-38073. In the response to your request, the Office of the State Engineer, in its letter dated November 17, 2005 specified that "Prior to any diversion of water, Rancho Viejo shall obtain verification or documentation from Santa Fe County of full compliance with any pertinent County regulations or ordinances governing the diversion of water in the Community College District."

Santa Fe County expects that Rancho Viejo will comply with all regulations and ordinances governing the diversion of water in the Community College District. However, since the well is unrelated to a specific development, there does not appear to be any specific requirements that apply to the proposed project.

Sincerely,

Dolores I. Vigil
Land Use Administrator

Copy: County Manager
County Attorney
Utilities Resources Director



REC'D AUG 29 2006

STATE OF NEW MEXICO
OFFICE OF THE STATE ENGINEER
Santa Fe

John R. D'Antonio Jr., P.E.
State Engineer

August 28, 2006

BATAAN MEMORIAL BUILDING, ROOM 102
SANTA FE, NEW MEXICO 87504-5102
(505) 827-6120
FAX: (505) 827-6682

Rancho Viejo de Santa Fe, Inc.
Isaac Pino, P.E., General Manager
P.O. Box 4458
Santa Fe, NM 87502

Re: Authorization to Change Completion Date for Injection of Water Diverted
from Well No. RG-38073—Expl. 5

Dear Mr. Pino:

In our continued desire to support innovative water related research, the Office of the State Engineer (OSE) is authorizing the Change in the completion date for the injection of water diverted from well No. RG-38073—Expl. 5. The expiration date for this authorization shall now be February 28, 2007. The original requirements in our Conditional Authorization issued on November 17, 2005 must still be met.

Please contact me if further discussion of this matter is needed. I can be reached at 827-4187.

Sincerely,

John T. Romero, P.E.

Director, Water Resource Allocation Program

cc: John R. D'Antonio, Jr., P.E., New Mexico State Engineer
Jim Sizemore, P.E., Water Right Director
Charles T. DuMars, LRPA
Richard Martinez, DFA-Capital Projects
Andy Edmondson, NM Environmental Dept.
Gerald T.E. Gonzalez, Santa Fe County Manager

Jtr

APPENDIX B

HAWLEY GEOLOGY REPORT CCD-OWA

BOREHOLE-SAMPLE AND GEOPHYSICAL LOGS FROM COLLEGE DISTRICT EXPLORATORY WELL CDX1, SANTA FE COUNTY, NM—INCLUDING SUMMARY OF HYDROGEOLOGIC INTERPRETATIONS

John W. Hawley, Ph.D., HAWLEY GEOMATTERS hgeomatters@qwest.net

The following log of drill cuttings from the 1,802-ft Pilot Hole for Rancho Viejo Observation-Well OB-A, in the Española Basin southwest of Santa Fe; and preliminary interpretations of basin-fill hydrogeology in the well-site area were made during and shortly after drilling operations in February and March, 2006. Except for a thin Quaternary erosion-surface veneer in the uppermost part of the borehole (~5-10ft), all deposits penetrated by the test well are correlated with the Oligocene to Lower Pleistocene Santa Fe Group (SFG)—Tesuque and Ancha Formations as defined by Brewster Baldwin (*in Spiegel and Baldwin 1993, p. 38-64*). *Note that the ‘upper’ Santa Fe-Ancha Formation has recently been ‘redefined’ by Koning and others (2002); but at test-well sites in the Rancho Viejo study area, the Ancha Fm conforms to both original and current lithostratigraphic concepts. Johnson and others (2004) have also extended Tesuque Fm-Lithosome mapping-unit concepts of Cavazza (1986) and Koning (2004) into the southern Española Basin (Appendix, p. 49-51).*

The bulk of SFG sediments in the study area (including the College District Exploratory [CDX1] Well site) are here interpreted as sandy, distal piedmont-slope lithofacies derived from the adjacent Santa Fe Range (southern Sangre de Cristos); and interbedded fine- to coarse-grained basin-floor sediments. These deposits are here classified according to two major systems of stratigraphic nomenclature: 1) Upper Neogene Santa Fe Group lithostratigraphic units: upper Santa Fe-Ancha Fm, and middle to lower Santa Fe-Tesuque Formation—“main body” and Bishop Lodge Mbr; and 2) informal lithofacies-assemblage (**LFA**) and hydrostratigraphic (**HSU**) subdivisions of the Santa Fe Group (**Fig. 1, Tables A-D**; Hawley and Kernodle, 2000). Major Tesuque Fm lithosomes S, and E?) are also tentatively identified. A lithologic description of drill cuttings (**Table A**, p. 4-24) is followed by summaries of major lithofacies, stratigraphic, and hydrogeologic interpretations (**Tables B and C**, p. 25-34, 35-45). **Table D** (p. 46) is a chart that summarizes the distribution of major hydrostratigraphic units, lithofacies assemblages, and Tesuque Fm lithosomes. **Selected References** are listed on p. 47 and 48.

Sample logging was done in cooperation with Casey Cook and Peter Balleau of Balleau Groundwater. Rodgers Brothers Drilling Company drilled the test well using the reverse-rotary method. Borehole geophysical logging (incl: natural Gamma, SP, short-normal and dual-induction resistivity, neutron, and caliper) was done by Welenco following drilling completion (2/13/06). Drill cuttings were collected at 10-ft intervals from the land surface to 1,800 ft. Sample logging involved use of standard field-identification procedures developed by the USDA-Natural Resource Conservation Service (NRCS) and other Federal agencies for their geological engineering and soil mapping programs (NRCS, 1996, National Soil Survey Handbook, 430-VI-NSSH).

Prior drilling experience in the area indicates that the basin fill is unconsolidated to moderately consolidated. Therefore, systems of classification developed in soil mechanics and soil surveys (i.e. Unified-ASTM) will be used in this investigation along with standard geological field descriptions. Bulk lithologic properties (incl. texture, color, grain-size grading, mineralogy, and secondary carbonate content) are estimated visually, manually, and with dilute HCl. "Visual" procedures include use of a hand-lens and binocular microscope where needed. Supplemental interpretations of vertical distribution of major textural classes (e.g. fine-grained vs. sand to fine gravel zones) are based on borehole geophysics and other drilling records. However, detailed analyses involving combined use of binocular and petrographic microscopy have not been done; so identification of fine-grained igneous and sedimentary rocks is definitely at a provisional level.

It is also important to note that drill cuttings from rotary-drilling methods represent only an approximation of the in-place lithologic character of the units penetrated by the drill bit. This is due to the mixing of cuttings and some loss of fine-grained material (clay, silt and fine sand) as the drilling fluid circulates through the borehole and mud pit. Comparison of borehole samples and geophysical logs, however, indicates that the reverse-rotary method used in this particular drilling operation produced a suite of samples that are representative of general subsurface conditions at the site. Because geophysical logging shows that there is some lag in drill-cutting return (usually <20ft), reported lithologic-unit depth ranges are adjusted to an estimated "true depth" in Tables 2 and 3. Descriptions of sampled intervals include all or part of the following information on drill-cutting properties:

1. Dominant textural class(es)¹
2. Dominant moist color[s]²
3. Grain-size distribution by major textural class³
4. Grading of sand grains and fine (pebble) gravel clasts⁴
5. Grain and clast angularity/roundness (angular, subangular, subrounded, rounded)
6. Dominant grain and clast composition
7. Carbonates: calcareous/noncalcareous—effervescence in dilute HCl; and secondary carbonate morphologies⁵
8. Other classifications: **Unified-ASTM**, *USDA-NRCS*

Footnotes:

¹ For standard geological notation (see³)

² Munsell Color (2000)

³ Major textural classes

- a. Mud/fines: silt-clay mixtures (<0.062mm [w/clay <0.004mm]). Note that the sand/silt break varies from 0.05mm (USDA) to 0.074mm (ASTM)
- b. Sand (0.062 to 2mm): very fine (vf sd)-0.062 to 0.125mm, fine (f sd)-0.125 to 0.25mm, medium (m sd)-0.25 to 0.5mm, coarse (c sd)-0.5 to 1mm, very coarse (vc sd)-1 to 2mm. Note that sand the sand/fine gravel break varies from 2mm (USDA) to 4.75mm (ASTM)
- c. Gravel [Pebbles](2 to 64mm): very fine (vf gvl)-2 to 4mm, fine (f gvl)-4 to 8mm, medium (m gvl)-8 to 16, coarse (c gvl)-16 to 32mm, very coarse (vc gvl)-32-64mm. Note: Cobbles [cobble gravel]-64 to 256mm, and boulders [boulder gravel]->256mm

- ⁴ Well graded (poorly sorted)=large range of size classes, poorly graded (well sorted)=small range of size classes. Note that “moderately” may be used to indicate intermediate levels of grading (sorting)
- ⁵ e=effervescent – bubbles readily observed, es=strongly effervescent – bubbles form a low foam, ev=violently effervescent – thick foam “jumps up”

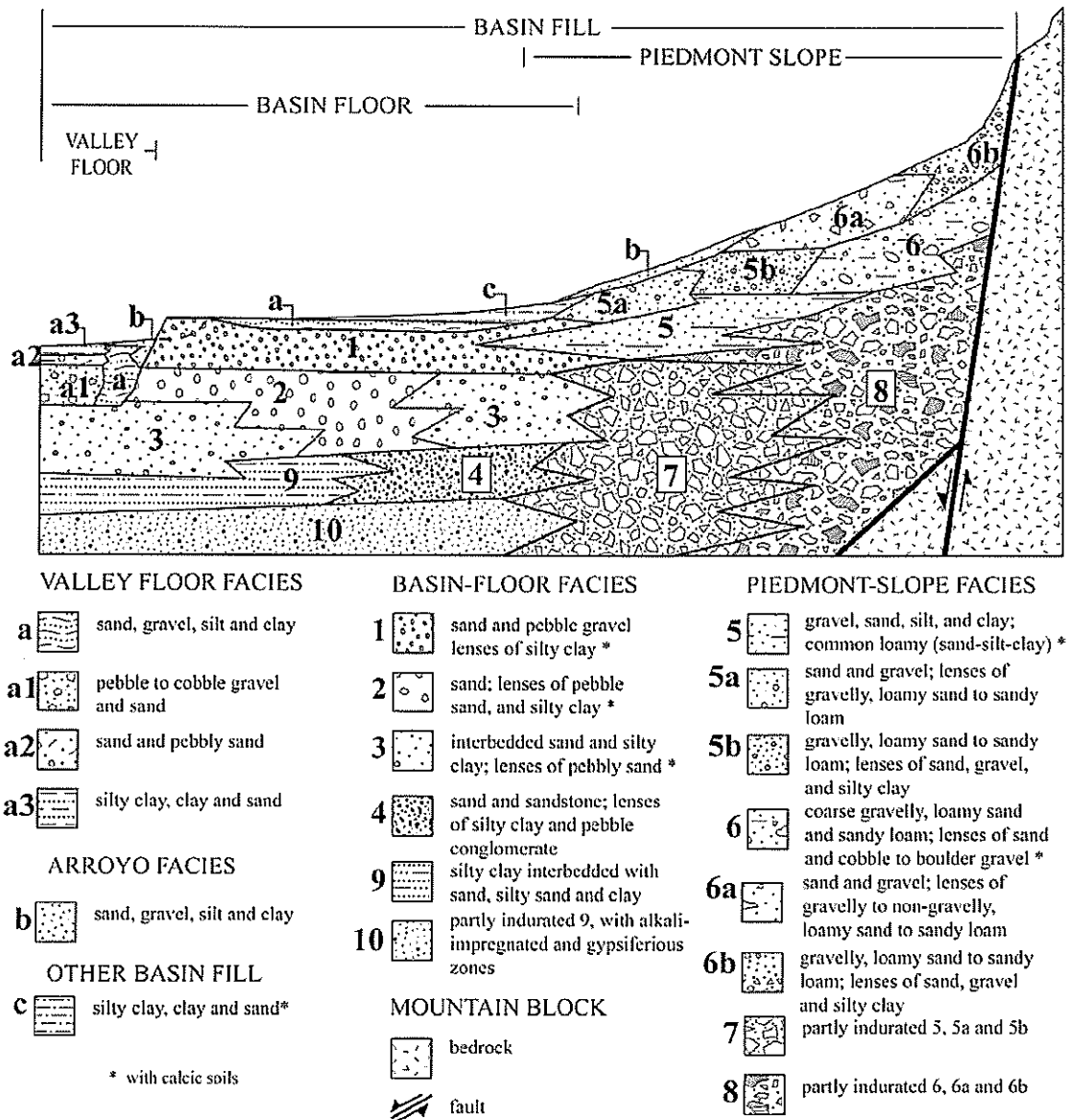


Figure 1. Schematic distribution pattern of major lithofacies assemblages (Tables 1 to 3) in Santa Fe Group basin fill and post-Santa Fe valley fills of the Rio Grande rift region. From Hawley and Kernodle (2000)

**TABLE A. DETAILED LITHOLOGIC LOG OF PILOT HOLE FOR
OBSERVATION WELL OB-A (RANCHO VIEJO) BASED
ON VISUAL ANALYSES OF DRILL CUTTINGS**

Well Name: OB-A
Location: T16N, R9E, Section 29.111
Lat/Long: 35°35'43" N, 106°01'05" W
State Plane Coordinates (est.): X=1709332 (569100) Y=1672077 (1671600)
Elevation: 6,475ft asl
Total Depth: 1,802 ft
Completed: 2/12/2006
Geophysical Logging (to 1,760 ft): 2/13/2006

Description and Classification of Drill Cuttings

Depth (ft)	Description, Classification, and Remarks
0-10	Pebbly sand, slightly silty and poorly sorted. Dark reddish gray to reddish brown (5YR4/2-3). Sand (vf-vc), with 10% vf-m pebble gravel and 10% silt. Well graded, angular to subangular sand grains and gravel clasts. Arkosic mineralogy (quartz, K-feldspar, granite/pegmatite lithics; w/ one weathered micaceous gneiss pbl (derived from local Pre-Cambrian terrane). Calcareous (e-es). SW , <i>Sand</i> .
Note: Top (?) of Upper Santa Fe-Ancha Fm (Pliocene-Early Pleistocene) within 5-10 ft of land surface. Cuttings to 40ft from auger borehole for surface casing.	
10-20	Silty sand, poorly sorted. Reddish brown (5YR4/4). 70-75% sand (vf-vc), 25-30% silt, and <2% pebbles (pbls)(vf-m). Well graded, angular to subrounded sand grains and gravel clasts. Arkosic grain/clast mineralogy (as above), w/common K-mica flakes, one m pbl-granite, and f pbl-brown chert. Calcareous (e-es). SM , <i>Sandy loam</i> .
20-30	Sandy pebble gravel, poorly sorted. Reddish brown (5YR4/3). 60% pbls (vf-vc), 35% sand (vf-vc), and 5% silt. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/ mica flakes and 64mm subrounded granite pbl. Noncalcareous. GW , <i>Sandy fine gravel</i> .
30-40	Silty sand, poorly sorted. Reddish brown (5YR4/4). 70-75% sand (vf-vc), 20-25% silt, and 5% pbls (vf-c). Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/few m-c pbls of gray to black siliceous ss and conglomeratic ss. Noncalcareous. SM , <i>loamy sand</i> .

Description and Classification of Drill Cuttings

Depth (ft)	Description, Classification, and Remarks
40-50	Very fine pebbly sand, poorly sorted. Reddish brown (5YR5/3). 85-90 % sand (vf-vc), with 10-15% pbls (vf-f). Well graded, angular to subrounded grains and clasts. Arkosic- micaceous mineralogy (as above). Noncalcareous. SW , <i>Sand</i> . <u>Remarks: Start reverse-rotary drilling with water drilling fluid.</u>
50-60	Silty sand, poorly sorted. Reddish brown (5YR4-5/3). 75-80% sand (vf-vc), 20-25% silt, and trace vf-f pbls. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/common mica flakes. Noncalcareous. SM , <i>Loamy sand</i> .
60-70	Very fine pebbly sand, poorly sorted. Reddish brown (5YR5/3). Sand (vf-vc), with vf-f pbls (10-15%). Well graded, angular to subrounded grains and clasts. Arkosic- micaceous mineralogy (as above). Noncalcareous. SW , <i>Sand</i> .
70-80	Silty sand—dominant, w/ interbedded(?) very fine sandy silt. Sand: dark brown (7.5YR3/2); silt: brown (7.5YR5/3). 85-90% sand (vf-vc), 10-15% silt, and few vf-f pbls. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Calcareous (e-es). SW-SM , <i>Sand-loamy sand</i> . <u>Remarks: Possible buried soil in upper part of interval.</u>
80-90	Pebbly sand, slightly silty and poorly sorted. Reddish brown (5YR4-5/3). 80% sand (vf-vc), 10% silt, and 10% vf-m pbls. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/common mica flakes. Calcareous (e). SW , <i>Sand</i> .
90-100	Silty to sandy clay. Reddish gray (5YR5/2). 60% silt-clay (fine-fraction, fines, mud), 35% sand (vf-vc), and 5% pbls (vf-m). Well graded, angular to subrounded grains and clasts. Arkosic mineralogy (as above). Calcareous (ev). SC , <i>Sandy loam-sandy clay loam</i> .
100-110	Pebbly sand, poorly sorted, w/ minor interbedded(?) silty to sandy clay (as above, 90-100). Reddish brown (5YR4-5/3). 80-85% sand (vf-vc), 10% pbls (vf-m), and 5-10% fines. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Calcareous (es-ev), with trace (mostly pink, 2.5-5YR7/3) soft carbonate segregations (<i>can</i>). SW , <i>Sand</i> and minor SC , <i>Sandy clay loam</i> .
110-120	Slightly silty sand, poorly sorted. Reddish brown (5YR5/3), with some reddish gray (5YR5/2) silty zones. 80-85% sand (vf-vc), 10-15% fines, and 5-10% pbls (vf-f). Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Very calcareous (ev), with trace pink <i>can</i> as above. SW , <i>Sand</i> .

Description and Classification of Drill Cuttings

Depth (ft)	Description, Classification, and Remarks
120-130	Sandy pebble gravel, poorly to moderately sorted. Reddish brown (5YR5/3-4). 60% pbls (vf-m) and 40% sand (f-vc). Moderately to well graded, angular to subrounded grains and clasts; clast max: 15mm. Arkosic grain/clast mineralogy (as above). Noncalcareous. GW , <i>Sandy fine gravel</i> .
130-140	Pebbly sand, slightly silty and poorly sorted. Reddish brown (5YR5/3-4). 60% sand (vf-vc), 30% pbls (vf-m), and 10% fines. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Calcareous fine fraction w/ trace <i>can</i> . SW-GW , <i>Sand to very fine gravelly sand</i> .
140-150	Pebbly sand, slightly silty and poorly sorted. Reddish brown (5YR5/3-4). 70% sand (vf-vc), 25-30% pbls (vf-f), and <5% fines. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Calcareous fine fraction. SW-GW , <i>Sand to very fine gravelly sand</i> .
150-160	Pebble gravel and sand, poorly sorted. Reddish brown (5YR5/4). 50% pbls (vf-m) and 50% sand (f-vc). Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above) w/ trace diorite. Noncalcareous. GW-SW , <i>Sandy fine gravel and very fine gravelly sand</i> .
160-170	Pebble gravel and sand, as above (150-170).
170-180	Pebbly sand, poorly sorted. Reddish brown (5YR5/4). 65% sand (vf-vc) and 35% pbls (vf-m). Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Noncalcareous. SW-GW , <i>Sand to very fine gravelly sand</i> .
180-190	Sandy pebble gravel, poorly sorted. Reddish brown (5YR5/3-4). 60% pbls (vf-m) and 40% sand (vf-vc). Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/ trace dark quartzite. Noncalcareous. GW , <i>Sandy fine gravel</i> .
190-200	Pebbly sand, poorly sorted. Reddish brown (5YR5/3-4). 60% sand (vf-vc) and 40% pbls (vf-m). Well graded, angular to subrounded grains and clasts; clast max: 13mm. Arkosic grain/clast mineralogy (as above), w/ some quartzite and diorite. Noncalcareous. SW-GW , <i>Sand to very fine gravelly sand</i> .
200-210	Pebbly sand, poorly sorted. Reddish brown (5YR5/3). 65% sand (vf-vc) and 35% pbls (vf-m). Well graded, angular to subrounded grains and clasts; clast max: 16mm. Arkosic grain/clast mineralogy (as above). Noncalcareous. SW-GW , <i>Sand to very fine gravelly sand</i> .

Description and Classification of Drill Cuttings

Depth (ft)	Description, Classification, and Remarks
210-220	Pebble gravel and sand, poorly sorted. Reddish brown (5YR5/4). 50% pbls (vf-m) and 50% sand (f-vc). Well graded, angular to subrounded grains and clasts; clast max: 10mm. Arkosic grain/clast mineralogy (as above), w/ quartzite and diorite. Noncalcareous. GW-SW , <i>Sandy fine gravel and very fine gravelly sand</i> .
220-230	Coarse pebble gravel, poorly to moderately sorted. Reddish brown (5YR5/3). 75% pbls (vf-vc) and 40% sand (f-vc). Moderately to well graded, angular to subrounded grains and clasts; clast max: 45mm. Arkosic grain/clast mineralogy (as above), with gneiss, diorite, and quartzite. Noncalcareous. GW , <i>Fine gravel</i> .
<p>Note: Contact of Upper Santa Fe-Ancha Fm on Middle Santa Fe-Tesuque Fm at ~215ft is inferred from “drillograph” records, borehole geophysics, and major texture-mineralogy shift in drill cuttings. Driller noted very coarse gravel (“boulders”) at about 205ft and a shift to much faster bit penetration at 213ft.</p>	
230-240	Silty clay to clay. Reddish brown (2.5YR4/4). 80 fines, >18% sand (vf-c), <2% pbls (vf). Arkosic grain/clast mineralogy (as above). Very calcareous (es-ev). CL , <i>Clay to clay loam</i> .
240-250	Silty clay to clay. Reddish brown (2.5YR4/3-4). 80% fines and 20% sand (vf-c), and trace vf pbls. Arkosic grain/clast mineralogy (as above). Very calcareous (es-ev), w/ few pink (5YR7/3) <i>can.</i> CL , <i>Clay to clay loam</i> .
250-260	Silty clay to clay, as above (230-250), with trace vf-f pbls. Clasts include quartz, K-feldspar, granite, and quartzite.
260-270	Pebble gravel and sand, poorly sorted. Brown (7.5YR5/3) to reddish brown (5YR5/4). 50% pbls (vf-m) and 50% sand (f-vc). Well graded, w/ angular to rounded grains and angular to subrounded clasts; clast max: 15mm. Arkosic grain/clast mineralogy (quartz, K-feldspar, K-mica, and granite/gneiss lithics) w/ few Pz ss, siltstone (slts), and gray chert. Noncalcareous. GW-SW , <i>Sandy very fine gravel and very fine gravelly sand</i> . <u>Remarks: Interpreted as Lithosome S of the Tesuque Fm (Johnson et al., 2004; Koning and Hallett, 2001 [2006 update]).</u>
270-280	Silty clay to clay—dominant, with interbedded(?) pebble gravel and sand as above (260-270). Fines: Reddish brown (2.5YR4/4); 80% silty clay and 20% sand (vf-c), <2% pbls (vf). Arkosic grain/clast mineralogy (as above). Noncalcareous to very calcareous (es). CL and GW-SW , <i>Clay to clay loam and very fine gravel to fine gravelly sand</i> .

Description and Classification of Drill Cuttings

Depth (ft)	Description, Classification, and Remarks
280-290	Sandy to silty clay. Reddish brown (5YR5/3). 70 fines, >28% sand (vf-c), <2% pbls (vf-m); clast max: 10mm. Arkosic grain/clast mineralogy (as above), including weathered gneiss; w/ trace light-gray chert. Noncalcareous to very calcareous (es). SC-CL , <i>Sandy clay loam to clay</i> .
290-300	Silty clay to clay. Reddish brown (2.5YR4/4). 80 % fines, 20% sand (vf-c), and trace vf pbls. Arkosic grain/clast mineralogy (as above). Very calcareous (es-ev), w/ few pink can. CL , <i>Clay Loam to clay</i> .
300-310	Coarse pebbly sand, slightly silty and poorly sorted. Reddish brown to light reddish brown (5YR5-6/3). 50% sand (vf-vc), 40% pbls (vf-c), and 10% fines. Well graded, grain/clast angularity/rounding as above (260-270); clast max: 30mm. Arkosic grain/clast mineralogy (as above); w/ trace quartzite. Calcareous fine fraction w/ trace can. SW-GW , <i>Fine gravelly sand</i> .
310-320	Pebbly sand as above (300-310, 260-270) dominant, with some interbedded(?) silty to sandy clay. Fines: reddish brown (2.5YR4/4). 50% fines, 35% sand (vf-vc), and 5% pbls (vf-m); clast max: 15mm. Arkosic mineralogy (as above), w/ trace black chert (Pz). Calcareous (e-ev). SW-GW , <i>Fine gravelly sand</i> ; w/ SC , <i>Sandy clay loam</i> .
320-330	Fine pebbly sand, poorly sorted. Reddish brown (5YR5/3). 80-85% sand (vf-vc), 15% pbls (vf-f), and <5% fines. Well graded, grain/clast angularity/rounding as above (260-270); clast max: 30mm. Arkosic grain/clast mineralogy (as above); w/ trace black and gray chert (Pz). Non- to slightly calcareous (e). SW , <i>Very fine gravelly sand</i> .
330-340	Fine sandy to silty clay. Reddish brown (5YR5/4&2.5YR4/4). 75% fines, 25% sand (vf-c), and trace vf pbls. Arkosic grain/clast mineralogy (as above). Slightly to very calcareous (e-ev). SC-CL , <i>Clay loam to clay</i> .
340-350	Interbedded(?) fine pebbly sand and silty clay to clay as above (320-340).
350-360	Interbedded(?) fine pebbly sand and silty clay to clay as above (320-340), w/ fine-grained zones dominant (~67%).
360-370	Sandy to silty clay, with few thin sandy zones (like 320-330). Reddish brown (5YR5/4&2.5YR4/4). 60% fines, 40% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above). Very calcareous (es-ev), w/ few light yellowish brown (10YR6/3) high-carbonate zones. SC , <i>Sandy loam to sandy clay loam</i> .
370-380	Interbedded(?) fine pebbly sand and silty clay to clay as above (320-350).

Description and Classification of Drill Cuttings

Depth (ft)	Description, Classification, and Remarks
380-390	Sandy to silty clay. Reddish brown (5YR5/3). 60% fines, 40% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above). Calcareous (ev). SC , <i>Sandy loam to sandy clay loam</i> .
390-400	Fine to medium pebbly sand, poorly sorted. Reddish brown (5YR5/3). 75% sand (vf-vc), 20% pbls (vf-f), and <5% fines. Well graded, grain/clast angularity/rounding as above (260-270); clast max: 30mm. Arkosic grain/clast mineralogy (as above); w/ highly weathered gneiss fragment, and trace coarse ss and black chert (Pz). Non- to slightly calcareous (e). SW , <i>Fine gravelly sand</i> .
400-410	Silty clay. Reddish brown (2.5YR4/4-5). 80% fines and 20% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above). Very calcareous (ev), w/ pink (5YR7/3) <i>can</i> . CL , <i>Clay to clay loam</i> .
410-420	Clay to silty clay. Weak red to reddish brown (10R4/3-2.5YR4/4). 90% fines and 10% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/ trace Pz? slts and light reddish brown to pink (2.5YR6-7/3) limestone (Is) fragments. Very calcareous (ev), w/ pink <i>can</i> . CL , <i>Clay</i> . <u>Remarks: Some "Is" fragments here and below could be indurated carbonate segregations (<i>cam</i>).</u>
420-430	Silty clay, as above (400-410).
430-440	Sand, poorly to moderately sorted, with interbedded(?) silty clay, as above (400-430). Sand: reddish brown (5YR5/3) and fines: 5YR4/4). 85-90% sand (vf-vc), <5% pbls (vf-m), and 10% fines. Well to moderately graded, grain/clast angularity/rounding as above (260+); clast max: 13mm. Arkosic grain/clast mineralogy (as above); w/ trace quartzite. Non- to very calcareous (ev). SW , <i>Sand</i> ; with CL , <i>Clay loam to clay</i> .
440-450	Clay to silty clay. Reddish brown (2.5-5YR5/4), with trace weak red (10R4/3). 90% fines and 10% sand (vf-c), w/ trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/ trace slts (Pz?). Non- to slightly calcareous (e). CL , <i>Clay</i> .
450-460	Clay to silty clay, as above (440-450), with slightly more (5-10%) very fine sandy silt.
460-470	Fine sandy to silty clay. Reddish brown (2.5-5YR5/4), with trace weak red (10R4/3). 70% fines, 30% sand (vf-f), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/weathered calcareous ss (Pz?). Very calcareous (es-ev), w/ pink <i>can</i> . SC-CL , <i>Clay loam to clay</i> .
470-480	Fine sandy to silty clay. Light reddish brown (2.5-5YR6/3). Texture, mineralogy, and secondary carbonates as above (460-470).

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
480-490	Clay to silty clay. Variegated: Pale red to reddish brown (10R-2.5YR4-5/4), and light reddish brown (2.5YR6/4). 85-90% fines, 10-15% sand (vf-f), and trace vf-f pbls. Arkosic grain mineralogy (as above), w/ trace ls (Pz?). Very calcareous (es-ev), w/ pink <i>can</i> and zones of black Mn-oxide (MnO) dendrites. CL , <i>Clay</i> . <u>Remarks: See 410-420; lighter values indicate slight increase in silt and vf sand.</u>
490-500	Clay to silty clay. Reddish brown (2.5-5YR5/4), with trace weak red (10R4/3). 90% fines and 10% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/ trace slts (Pz?). Non- to slightly calcareous (e). CL , <i>Clay</i> .
500-510	Clay to silty clay, as above (490-500).
510-520	Fine sandy to silty clay. Reddish brown (2.5-5YR5/4). 70% fines, 30% sand (vf-f), and trace vf pbls. Arkosic grain mineralogy (as above), w/ weathered calcareous ss (Pz?). Very calcareous (ev), w/ pink <i>can</i> . SC-CL , <i>Clay loam to clay</i> .
520-530	Clay to silty clay, as above (480-490); variegated.
530-540	Clay to silty clay, as above (480-490, 520-530). Variegated: Pale red to reddish brown (10R-2.5YR5/4), and reddish brown (5YR5/3). 80-90% fines, 10-20% sand (vf-f), and trace vf pbls. Arkosic grain mineralogy (as above). Very calcareous (ev), w/ pink <i>can</i> . CL , <i>Clay loam to clay</i> .
540-550	Clay to silty clay. Reddish brown (2.5YR4/4), with trace weak red (10R4/3). 90% fines and 10% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/ trace ss (Pz?). Very calcareous (ev). CL , <i>Clay</i> .
550-560	Silty clay to clay—dominant, with interbedded(?) silty vf-m sand. Reddish brown (2.5YR4-5/4 & 5YR5/3). 80-90% fines, 10-20% sand (vf-f), and trace vf pbls. Arkosic grain mineralogy (as above). Very calcareous (ev), w/ pink <i>can</i> . CL and SW , <i>Clay and fine sand</i> .
560-570	Clay to silty clay, as above (540-550), with trace vf-m pbls. Arkosic grain/clast mineralogy (as above), w/ trace ls (Pz?). Very calcareous (ev), w/ pink <i>can</i> . CL , <i>Clay</i> .
570-580	Clay to silty clay, as above (540-550, 560-570); with few thin beds(?) of soft silty ss and fine sand. Sand and ss: Light reddish brown (2.5YR6/3), Very calcareous (ev), w/ pink <i>can</i> . CL w/minor SM , <i>Clay w/minor loamy sand</i> .
580-590	Clay to silty clay, with some sand/ss beds, as above (570-580). Trace (~1%) vf –f pebbles of weathered calcareous ss.
590-600	Fine sandy to silty clay. Reddish brown (5YR5/3). 70% fines, 30% sand (vf-f), and trace (<1%) vf pbls. Arkosic grain mineralogy (as above), w/ trace chert (Pz?). Calcareous (e-es), w/ pink <i>can</i> . SC-CL , <i>Clay loam to clay</i> .

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
600-610	Sandy clay. Reddish brown (5YR5/4). 45% fines, 55% sand (vf-vc), and <1% pbls (vf-m). Well graded, w/ angular to rounded sand grains and angular to subrounded pebble clasts. Arkosic grain/clast mineralogy, w/ trace quartzite. Very calcareous (ev), w/ pink can. SM-SC , <i>Sandy clay loam</i> . <u>Remarks: Uppermost sample selected for sieve analysis, with representative sample-splits taken at about 50-ft intervals btw 600 and 1,610ft.</u>
610-620	Muddy sand, poorly sorted—dominant; with interbedded(?) sandy-silty clay. Reddish brown (2.5-5YR4/4, 5YR5/3). 65% sand (vf-vc), <35% fines, and <1% pbls (vf-m). Well graded sands; grain/clast angularity/rounding as above (600-610). Arkosic grain/clast mineralogy, w/ trace chert?(Pz) and quartzite. Very calcareous (ev), w/ pink can. SM , <i>Sandy loam</i> . <u>Remarks: Some K-feldspar pebbles highly weathered and cleave readily.</u>
620-630	Fine sandy to silty clay. Reddish brown (5YR4/4-5/3). 70% fines, <30% sand (vf-f), and 1-2% pbls (vf-m); clast max: 15mm. Arkosic grain mineralogy (as above), w/ quartzite, weathered gneiss, and white (10YR8/1) chert (Pz?). Very calcareous (ev), w/ pink can. SC-CL , <i>Clay loam to clay</i> .
630-640	Silty sand, poorly sorted—dominant; with interbedded(?) sandy-silty clay, as above (610-620).
640-650	Clay to silty clay. Reddish brown (2.5YR4/3). 90% fines and 10% sand (vf-c), and trace vf pbls. Arkosic grain/clast mineralogy. Very calcareous (ev). CL , <i>Clay</i> .
650-660	Muddy sand to sandy clay. Reddish brown (2.5YR4/4 & 5YR5/3). 40% fines, 55-60% sand (vf-vc), and <5% pbls (vf-f). Well graded sands, grain/clast angularity/rounding as above (600-610). Arkosic grain/clast mineralogy, w/ trace chert and weathered calcareous ss (Pz). Very calcareous (ev), w/ pink can. SM-SC , <i>Sandy loam to sandy clay loam</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
660-670	Silty to sandy clay, as above (650-660); no chert noted in coarsest-size fraction.
670-680	Muddy sand, poorly sorted—dominant; with interbedded(?) sandy-silty clay. Reddish brown (2.5-5YR4/4, 5YR5/3). 65% sand (vf-vc), <35% fines, and <1% pbls (vf-m); clast max: 12mm. Well graded sands; grain/clast angularity/rounding as above (600-670). Arkosic grain/clast mineralogy, w/ trace chert?(Pz) and quartzite. Very calcareous (ev), w/ pink can. SM , <i>Sandy loam</i> .
680-690	Clay to silty clay. Reddish brown (2.5YR4/3). 90% fines, 10% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy. Very calcareous (ev). CL , <i>Clay</i> . <u>Remarks: Like 640-650.</u>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
690-700	Muddy sand to sandy clay. Reddish brown (2.5YR4/4 & 5YR5/3). 55-60% sand (vf-vc), 40% fines, and <5% pbls (vf-f). Well graded sands, grain/clast angularity/rounding as above (600-610). Arkosic grain/clast mineralogy, w/ trace chert and weathered calcareous ss (Pz). Very calcareous (ev), w/ pink <i>can.</i> SM-SC , <i>Sandy clay loam.</i>
700-710	Muddy sand, with interbedded(?) sandy and silty clay. Reddish brown (2.5YR4/4 & 5YR5/3). 55-60% sand (vf-vc), 40% fines, and <5% pbls (vf-f) in sieved sample. Well graded sands, grain/clast angularity/rounding as above (650-660). Arkosic grain/clast mineralogy, w/ trace chert (Pz) and quartzite. Very calcareous (ev), w/ pink <i>can.</i> SM-SC , <i>Sandy loam to sandy clay loam</i> ; and SC-CL , <i>Sandy clay to clay.</i> <u>Remarks: Coarser fraction of sampled interval selected for sieve analysis.</u>
710-720	Sandy clay, with interbedded(?) silty clay, as above (700-710); w/ trace ls (Pz?).
720-730	Clay to silty clay. Reddish brown (2.5YR4/3). 85% fines, 15% sand (vf-c), and trace vf pbls. Arkosic grain/clast mineralogy. Very calcareous (ev). CL , <i>Clay.</i> <u>Remarks: Like 640-650, 680-690.</u>
730-740	Silty sand, as below (740-740). 75-80% sand (vf-vc), 20% fines, and <3% pbls (vf-f). Arkosic mineralogy, w/ trace ss (Pz?).
740-750	Muddy sand, moderately sorted. Sand: reddish brown (5YR5/3); fines: reddish brown (2.5YR4/3-5/4). 79% sand (vf-vc), 15% fines, and 6% pbls (vf-f). Moderately graded sands, grain/clast angularity/rounding as above (700-710). Arkosic grain/clast mineralogy, w/ trace chert (Pz) and quartzite. Very calcareous (ev), w/ pink <i>can.</i> <u>Remarks: Sieve analysis of representative sample-split.</u>
750-760	Clay to silty clay. Reddish brown (2.5YR4/3). 90% fines, 10% sand (vf-c), and trace vf pbls. Arkosic grain/clast mineralogy. Very calcareous (ev), w/ pink <i>can.</i> CL , <i>Clay.</i> <u>Remarks: Like 640-650, 680-690, 720-730.</u>
760-770	Clay to silty clay, as above (750-760), with no pbls.
770-780	Clay to silty clay. Reddish brown (2.5YR4/3). 85% fines, 15% sand (vf-c), and trace vf-f pbls. Arkosic grain/clast mineralogy; w/ trace ls (Pz?). Very calcareous (ev). CL , <i>Clay.</i> <u>Remarks: Like 640-650, 680-690, 720-730, 750-770.</u>
780-790	Fine sandy to silty clay. Reddish brown (5YR4/4-5/3). 70% fines, <30% sand (vf-f), and trace vf pbls. Arkosic grain mineralogy (as above) ; w/ trace ls (Pz?). Very calcareous (ev), w/ pink <i>can.</i> SC-CL , <i>Clay loam to clay.</i>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
790-800	Muddy sand, poorly sorted. Reddish brown (2.5-5YR5/3). <75% sand (vf-vc), 25% fines, and 1% pbls (vf-f). Well graded sands, grain/clast angularity/rounding as above (740-750). Arkosic grain/clast mineralogy, w/ trace dark quartzite. Very calcareous (ev), w/ pink <i>can</i> .
800-810	Muddy sand, moderately sorted; with interbedded(?) silty clay. Sand: reddish brown (5YR5/3), fines (2.5YR4/4-5YR5/3). 60% sand (vf-vc), 35% fines, and 5% pbls (vf-f) in sieved sample. Moderately graded sands, w/ grain/clast angularity/rounding as above (740-750). Arkosic grain/clast mineralogy, w/ trace ls, ss, chert, and quartzite. Very calcareous (ev), w/ pink <i>can</i> . SM-SC , <i>Sandy clay loam to loam</i> . <u>Remarks: Coarser fraction of sampled-interval selected for sieve analysis.</u>
810-820	Clay to silty clay. Reddish brown (2.5YR4/3). 85% fines and 15% sand (vf-c). Arkosic grain mineralogy. Very calcareous (ev). CL , <i>Clay</i> . <u>Remarks: Like 640-650, 680-690, 720-730, 750-780.</u>
820-830	Clay to silty clay, as above (810-820); interbedded with silty sand, as above (800-810).
830-840	Silty clay (dominant) with some interbedded(?) silty sand, as above (800-830), and 1-2% vf-f pebbles. Fines: Reddish brown (2.5YR4/4); sand: reddish brown (5YR5/3). Very calcareous (es-ev), w/ pink <i>can</i> .
840-850	Silty to fine sandy clay, with few silty sand beds. Variegated: Reddish brown (5YR4/4-5/3) and light brown to pink (7.5YR6-7/3). 66% fines, 32% sand (vf-vc), and 2% pbls (vf-f). Arkosic grain mineralogy (as above); w/ trace ls (Pz?). Very calcareous (ev), w/ pink <i>can</i> . SC-CL , <i>Clay loam to clay</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
850-860	Fine sandy to silty clay. Reddish brown (5YR5/3). 75% fines, 25% sand (vf-f), and trace(?) vf pbls. Arkosic grain mineralogy (as above). Very calcareous (ev), w/ pink <i>can</i> . SC-CL , <i>Clay loam to clay</i> .
860-870	Fine to very coarse sand (~60%); with interbedded silty to sandy clay, as above (850-860). Reddish brown: Sand (5YR5/3); fines (2.5YR4-5/4). 5% pebbles (vf-m). Well graded sands, w/ grain/clast angularity/rounding as above (800-810). Arkosic grain/clast mineralogy, w/ trace weathered gneiss and ls (Pz?). Very calcareous (ev), w/ pink <i>can</i> . SW , <i>Sand</i> and SC-SL , <i>Sandy clay-loam</i> .

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
870-880	Silty clay—dominant; with some interbedded(?) silty (vf) sand, as above (800-840), and no(?) pebbles. Fines: Reddish brown (2.5YR4-5/4); sand: reddish brown (5YR5/3). Very calcareous (ev), w/ few pink <i>can.</i> CL w/ SM , <i>clay w/Sandy clay loam to loam.</i>
880-890	Fine sandy to silty clay. Reddish brown (2.5-5YR5/4). 75% fines, 25% sand (vf-f), and no(?) pebbles. Arkosic grain mineralogy (as above). Very calcareous (ev), w/ pink <i>can.</i> SC-CL , <i>Clay loam to clay.</i>
890-900	Clay to silty clay. Reddish brown (2.5-5YR5/4). 80% fines and 20% sand (vf-m). Arkosic grain mineralogy. Very calcareous (ev). CL-ML , <i>Clay to clay loam.</i>
900-910	Silty clay, as above (880-900—dominant; with some interbedded(?) silty sand, as above (730-750), and no(?) pebbles. Fines: Reddish brown (2.5YR4-5/4); sand: reddish brown (5YR5/3). Very calcareous (ev), w/ few pink <i>can.</i>
910-920	Fine to medium pebbly sand, well to moderately sorted. Pinkish gray (7.5YR6/2). 73% sand (f-vc), 24% pbls (vf-m), and 3% fines. Moderately to well graded, with angular to subrounded grains and clasts; clast max: 13mm. Arkosic grain/clast mineralogy (as above); w/ trace slts and coarse ss (Pz). Sand: Non calcareous; fines very calcareous (ev). SW , <i>Fine gravelly sand.</i> <u>Remarks: Sieve analysis of representative sample-split. Upper beds of medium to coarse grained part of Lithosome S (910-1320)?</u>
<p>Note: In samples below 910 ft, well-rounded sand grains only present in trace amounts or absent, and indicate possible shift to zone of intertonguing of distal piedmont and marginal basin-floor facies (e.g. LFA's 5 & 2-3-9; Tesuque Lithosomes A and S).</p>	
920-930	Clay to silty clay. Reddish brown (2.5YR4/4). 85% fines, 15% sand (vf-m), and trace vf-f pbls. Arkosic grain/clast mineralogy. Very calcareous (es-ev). CL , <i>Clay.</i>
930-940	Silty clay, as above (920-930), interbedded with fine to coarse sand. Fines: Reddish brown (2.5YR4-5/4) and light reddish brown (2.5-5YR6/3); sand: reddish brown (5YR5/3). Trace vf-f pbls; arkosic, w/ ls (Pz?). Very calcareous (ev), w/ few pink <i>can.</i> CL , <i>Clay and SW</i> , <i>sand.</i>
940-950	Sandy to silty clay; with minor interbedded sand, as above (930-940). Fines: Reddish brown (2.5YR4-5/4). 65% fines, 35% sand (vf-m), Very calcareous (ev), w/ few pink <i>can.</i> CL-SC , <i>clay loam to sandy clay.</i>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
950-960	Fine sandy to silty clay. Reddish brown (2.5-5YR5/4). 70% fines, 30% sand (vf-f), and trace vf pebbles. Arkosic grain mineralogy (as above). Very calcareous (ev). SC-CL , <i>Clay loam to sandy clay</i> .
960-970	Fine pebbly, medium to very coarse sand, well sorted. Reddish brown (5YR5/3); w/ minor fines: Reddish brown (2.5YR4-5/3). 82% Sand (f-vc), 15% pbls (vf-f), and 3% fines. Poorly graded, grain/clast angularity/rounding as above (from 910 ft). Arkosic grain/clast mineralogy (as above); w/ trace slts, fine to coarse ss (Fe-MnO cement), and black chert (Pz). Sand: Non calcareous; fines very calcareous (ev). SP , <i>Fine gravelly sand</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
970-980	Fine to medium pebbly sand, well to moderately sorted. Reddish brown (5YR5/3); w/ minor fines: Reddish brown (2.5YR4-5/3).. >75% sand (f-vc), 20% pbls (vf-c), and <5% fines. Moderately to well graded, grain/clast angularity/rounding as above (from 260ft); clast max: 25mm. Arkosic grain/clast mineralogy (as above); w/ trace marlstone and brown chert (Pz). Sand: Non calcareous; fines very calcareous (ev). SP-SW , <i>Fine gravelly sand</i> .
980-990	Fine to medium pebbly sand, as above (960-980); without coarse pebbles and Pz chert. SP-SW , <i>Fine gravelly sand</i> .
990-1000	Clay to silty clay—dominant; with minor interbedded(?) fine sand. Reddish brown (2.5YR4/3-5YR5/3). 85% fines, 15% sand (vf-f), and trace vf-f pbls. Arkosic grain/clast mineralogy. Very calcareous (ev), w/ pink can. CL , <i>Clay</i> .
1000-1010	Clay to silty clay. Reddish brown (2.5YR4/4), and weak red to reddish brown (10R-2.5YR4/3). 80-90% fines and 10-20% sand (vf-f). Arkosic grain/clast mineralogy. Very calcareous (ev), w/ pink can. CL , <i>Clay to clay loam</i> ; with minor SW , <i>sand</i> .
1010-1020	Silty clay. Reddish brown (2.5YR4/4). 70-80% fines, 20-30% sand (vf-c), and trace vf-m pbls. Arkosic grain/clast mineralogy, w/ trace ss (cemented zone fragment?). Very calcareous (ev), w/ pink can. SC-CL , <i>Sandy clay to clay loam</i> .
1020-1030	Pebbly, medium to very coarse sand, well sorted. Reddish brown (5YR5/4); fines: weak red (10R4/3). 75% Sand (m-vc), 25% pbls (vf-m), and trace fines; clast max: 10mm. Poorly graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ trace slts, ss, ls, and gray "banded" chert (Pz). Sand: Noncalcareous; fines very calcareous (ev). SP , <i>Fine gravelly sand</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1030-1040	Pebbly, medium to very coarse sand, as above (1020-1030); clast max: 15mm.
1040-1050	Pebbly, medium to very coarse sand, as above (1020-1040); with minor interbedded(?) silty clay. Fines: Weak red to reddish brown (10R-2.5YR4/4). Clast max: 20mm. Arkosic grain/clast mineralogy (as above); w/ trace sandy ls and chert (Pz). Sand: Non calcareous; fines very calcareous (ev). SP , <i>Fine gravelly sand, with minor CL, Clay loam to clay.</i>
1050-1060	Clay to silty clay. Weak red to reddish brown (10R-2.5YR4/4). 80-90% fines, 10-20% sand (vf-vc), and trace vf pbls. Arkosic grain/clast mineralogy. Very calcareous (ev), w/ pink can. CL , <i>Clay to clay loam.</i>
1060-1070	Clay to silty clay, as above (1050-1060). Reddish brown (2.5YR4/3). 90% fines, 10% sand (vf-c), and trace vf pbls. CL , <i>Clay.</i>
1070-1080	Pebbly, medium to very coarse sand, well to moderately sorted. Reddish brown (5YR5/4); fines: Weak red (10R4/3). 73% Sand (m-vc), 25% pbls (vf-m), and 2% fines; clast max: 15mm. Poorly to moderately graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ trace f-c ss and chert (Pz). Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev). SP , <i>Fine gravelly sand.</i> Remarks: Sieve analysis of representative sample-split.
1080-1090	Pebbly, fine to very coarse sand, moderately to well sorted; with some interbedded pebble gravel. Reddish brown (5YR5/4); fines: Weak red (10R4/3). 63% Sand (f-vc), 35% pbls (vf-vc), and 2% fines; clast max: 15mm. Moderately to poorly graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ fragment of very coarse, rounded pbl of "purple" metaquartzite. Sand: Noncalcareous; fines very calcareous (ev). SP , <i>Gravelly sand; with(?) GP, Sandy gravel.</i>
1090-1100	Pebbly sand, as above (1070-1080), well sorted. Reddish brown (5YR5/4). 75% Sand (m-vc), 25% pbls (vf-c). Poorly graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ fragment of coarse, rounded pbl of metaquartzite. Noncalcareous. SP , <i>Gravelly sand.</i>
1100-1110	Pebbly, medium to very coarse sand, well sorted. Reddish brown (5YR5/4); fines: Reddish brown and pinkish gray (2.5YR4/4 & 6YR6/2). 76% Sand (f-vc), 23% pbls (vf-c), and 2% fines; clast max: 20mm. Poorly graded. Angularity/roundness and grain/clast mineralogy, as above and below (910+); w/ trace gray and brown chert (Pz). Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (es-ev). SP , <i>Fine gravelly sand.</i>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1110-1120	<p>Pebbly, medium to very coarse sand, well to moderately sorted. Reddish brown (5YR5/4); fines: Weak red (10R4/3). 76% Sand (m-vc), 22% pbls (vf-m), and 2% fines; clast max: 15mm. Poorly to moderately graded. Angularity/roundness and grain/clast mineralogy, as above; w/ trace f-c ss and chert (Pz). Sand: Noncalcareous; fines calcareous (e-es). SP, <i>Fine gravelly sand</i>. <u>Remarks: Sieve analysis of representative sample-split.</u></p>
1120-1130	<p>Sandy, fine to coarse pebble gravel, well sorted. Reddish brown (5YR5/4). 50% pbls (vf-c), 50% sand (f-vc) and trace fines (as above); clast max: 20mm. Poorly graded. Angularity/roundness and grain/clast mineralogy, as above; w/ trace ss and chert (Pz), and white "marlstone." Sand: Noncalcareous; fines calcareous (e-es). GP-SP, <i>Sandy very fine gravel and very fine gravelly sand</i>.</p>
1130-1140	<p>Pebbly, fine to very coarse sand, well sorted. Reddish brown (5YR5/4); fines: Reddish brown (2.5-5YR5/4). 70% Sand (f-vc), 30% pbls (vf-c), and trace fines; clast max: 25mm. Poorly graded. Angularity/roundness and grain/clast mineralogy, as above and (910+). Sand: Noncalcareous; fines calcareous (e-es). SP, <i>Fine gravelly sand</i>.</p>
1140-1150	<p>Silty clay to clay; with minor pebbly sand, as above (1130-1140). Fines: weak red to reddish brown (10R-2.5YR4/3). 80% fines, 20% sand (vf-f), and trace vf-f pbls. Arkosic grain/clast mineralogy. Very calcareous (ev), w/ pink can. CL, <i>Clay loam to clay</i>.</p>
1150-1160	<p>Interbedded(?) pebbly sand and silty clay, as above (1130-1140 & 1140-1150). SP, <i>Fine gravelly sand</i> and CL, <i>Clay loam to clay</i>.</p>
1160-1170	<p>Pebbly coarse sand, well sorted; with interbedded(?) silty clay; as above (1130-1160). Coarse fraction: 58% sand (m-vc) and 42% pbls (vf-c) in sieved sample; clast max: 25mm. Poorly graded, w/ grain/clast angularity/rounding as above (910+). Arkosic grain/clast mineralogy, w/ trace siliceous ss, chalcedony, and gray and brown chert (Pz). Noncalcareous to very calcareous (ev), w/ pink can, and sparry-calcite cement on some pebbles. SP, <i>Fine gravelly sand</i> and CL, <i>Clay loam to clay</i>. <u>Remarks: Coarser fraction of sampled-interval selected for sieve analysis.</u></p>
1170-1180	<p>Interbedded(?) pebbly sand and silty clay, as above (1130-1140 & 1140-1150); with about 10% f pebbles. SP, <i>Very Fine gravelly sand</i> and CL, <i>Clay loam to clay</i>.</p>
1180-1190	<p>Sandy, fine to coarse pebble gravel, well sorted. Reddish brown (5YR5/4). 50% pbls (vf-c), 50% sand (m-vc). Poorly graded. Angularity/roundness and arkosic grain/clast mineralogy, as above. Noncalcareous. GP-SP, <i>Sandy very fine gravel and very fine gravelly sand</i>.</p>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1190-1200	Sandy, fine to coarse pebble gravel, as above (1180-1190), over : sandy to silty clay. Reddish brown (2.5YR4/3). 60% fines, 40% sand (vf-vc), and trace vf-f pbls. Arkosic grain/clast mineralogy; w/ fragment of vc pebble (gneiss). Sand: Noncalcareous; fines very calcareous (ev), w/ pink <i>can.</i> GP-SP , <i>Sandy very fine gravel</i> and <i>very fine gravelly sand</i> , over : SC-CL , <i>Sandy clay to Clay loam</i> .
1200-1210	Sandy to silty clay. Reddish brown (2.5YR4-5/4) and pale red (10R5/4). 60% fines, 40% sand (vf-vc), and trace vf-f pbls; clast max: 8mm. Arkosic grain/clast mineralogy, as above. Very calcareous (ev), w/ pink <i>can.</i> SC-CL , <i>Sandy clay to clay loam</i> .
1210-1220	Muddy sand; with minor interbedded(?) fine to coarse sand. Fines: Weak red (10R4/3) and reddish brown (2.5YR5/3-4); sand: reddish brown (5YR4-5/4). 60% sand (vf-vc [$<10\%$ vc]), 40% fines, and trace vf pbls. Arkosic grain/clast mineralogy. Very calcareous (ev). SM-SC , <i>Sandy loam to sandy clay loam</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
1220-1230	Interbedded(?) silty clay and sand. Fines: Reddish brown (10R-2.5YR4/3). Sand: Reddish brown (5YR5/4). Fines: 40-60% silty clay and 40-60% sand (vf-m). Sand: 85% (vf-vc), w/ 10% vf-c pbls and 5% fines; moderately to poorly graded; angularity/roundness and arkosic grain/clast mineralogy (as above); w/ fragment of coarse, rounded pbl of metaquartzite. Fines very calcareous (ev), w/ pink <i>can.</i> SW-SP , <i>Sand</i> and SM-SC , <i>Sandy loam to sandy clay loam</i> .
1230-1240	Interbedded(?) sand and silty clay, as above (1220-1230)—sand dominant
1240-1250	Fine to medium pebbly sand, well sorted. Reddish brown (5YR5/4), with minor reddish brown (10R-2.5YR4/3) fines. $>80\%$ sand (vf-vc), 15% pbls (vf-m), and $<5\%$ fines. Poorly graded w/ grain/clast angularity/rounding as above (910+). Arkosic grain/clast mineralogy. Noncalcareous. SP , <i>Very fine gravelly sand</i> .
1250-1260	Pebbly, medium to very coarse sand, moderately sorted. Sand: Reddish brown (5YR5/4); fines: reddish brown (10R4-5/3). 78% Sand (f-vc), 13% pbls (vf-m), and 10% fines. Moderately graded. Angularity/roundness and grain/clast mineralogy, as above (1,070+); w/ trace slts and chert (Pz), and quartzite. Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev). SW-SP , <i>Fine gravelly sand</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
1260-1270	Silty clay and clay. Reddish brown (2.5YR4/3-4), and weak red (10R4/4). 75-85% fines, 15-25% sand (vf-f), and trace(?) vf pbls. Arkosic grain mineralogy. Calcareous (e-es). CL , <i>Clay to clay loam</i> .

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1270-1280	Sandy to silty clay; with minor interbedded(?) sand (like 1250-1260). Fines: reddish brown (2.5YR5/4) and pale red (10R5/4). 60% fines, 40% sand (vf-vc), and trace vf-f pbls; clast max: 8mm. Arkosic grain/clast mineralogy, as above. Very calcareous (ev), w/ pink can. SC-CL , <i>Sandy clay to clay loam</i> ; w/ minor SW , <i>sand</i> .
1280-1290	Clay and silty clay. Weak red to reddish brown (10R-2.5YR4/3-4). 85% fines, 15% sand (vf-f), and trace(?) vf pbls. Very calcareous (ev), w/ pink can. CL , <i>Clay</i> .
1290-1300	Clay and silty clay, as above (1280-1290).
1300-1310	Pebbly, medium to very coarse sand, moderately to well sorted. Sand: Reddish brown (5YR5/4); fines: reddish brown (10R4-5/3). 83% Sand (vf-vc), 7% pbls (vf-m), and 10% fines. Moderately poorly graded. Angularity/roundness and grain/clast mineralogy, as above (910+); w/ trace ss and chert (Pz), and quartzite (pC). Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev). SW-SP , <i>Fine gravelly sand</i> . <u>Remarks: Sieve analysis of representative sample-split. Basal part of ~400-ft thick, coarsest-grained subunit of the Tesuque Fm "main body" (Lithosome S of Johnson et al., 2004?).</u>
1310-1320	Muddy sand, moderately to well sorted; with minor interbedded(?) silty clay. Sand: reddish brown (5YR5/4), fines (2.5YR4/4). 75% sand (vf-m), 25% fines, and trace pbls (vf). Moderately to poorly graded sands, w/ grain/clast angularity/rounding as above (910+). Arkosic grain mineralogy. Very calcareous (ev), w/ pink can. SM , <i>Sandy loam-loamy sand</i> .
1320-1330	Clay and silty clay. Reddish brown (2.5YR4/4). 85% fines, 15% sand (vf-f), and trace(?) vf pbls. Very calcareous (ev), w/ pinkish gray (7.5YR6/2) can. CL , <i>Clay</i> .
1330-1340	Silty clay. Reddish brown (5YR5/3 & 2.5-5YR4/4). 75% fines, 25% sand (vf-f), and trace(?) vf pbls. Very calcareous (ev), w/ pinkish gray can. SC-CL , <i>Clay loam to clay</i> .
1340-1350	Sandy to silty clay. Reddish brown (2.5YR5/3). 55% fines and 45% sand (vf-vc). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pink can. SC-SM , <i>Sandy clay loam to clay loam</i> .
1350-1360	Sandy to silty clay, as above (1340-1350). Reddish brown (2.5YR5/3). 55% fines and 45% sand (vf-c, w/ trace vc). Arkosic grain mineralogy, and with w/ grain/clast angularity/rounding as above (910+). Very calcareous (ev), w/ pink can. SC-SM , <i>Sandy clay loam to clay loam</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1360-1370	Clay and silty clay. Reddish brown (2.5-5YR4/4). 85% fines, 15% sand (vf-f), and trace(?) vf pbls. Very calcareous (ev), w/ pinkish gray (7.5YR6/2) <i>can.</i> CL , <i>Clay</i> . <u>Remarks: With few light gray (2.5-5YR7/1) "reduction zones"</u>
1370-1380	Clay and silty clay, as above (1360-1370).
1380-1390	Clay and silty clay, as above (1360-1380); with minor interbedded fine sand.
1390-1400	Clay and silty clay, as above (1360-1380); with few cutting fragments of micaceous silty very fine sand (light gray, 5Y7/1).
1400-1410	Sandy clay; with few very fine to medium pebbles. Variegated: Reddish gray to brown (5-7.5YR5/2) and reddish brown (2.5YR5/3 & 4/3). 52% sand (vf-c), 45% fines, and 3% vf-f pbls. Arkosic grain mineralogy, as above; w/ few weathered intermediate volcanics (?). Very calcareous (ev). SM-SC , <i>Sandy clay loam</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
1410-1420	Sandy to silty clay. Reddish brown (2.5YR4/3), with some pinkish gray (5YR6/2) high-carbonate zones. 60% fines, 40% sand (vf-vc), and trace vf-m pbls. Arkosic grain/clast mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC , <i>Sandy clay to clay loam</i> .
1420-1430	Very fine sandy to silty clay. Reddish brown (2.5YR4/3), with some pinkish gray (5YR6/2) high-carbonate zones. 70% fines and 30% sand (vf-vc). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC , <i>Clay loam to clay</i> .
1430-1440	Sandy clay; with few very fine to medium pebbles. Dark reddish gray to reddish gray (5YR4-5/2). 50% sand (vf-f) and 50% fines. Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SM-SC , <i>Sandy clay loam</i> .
1440-1450	Muddy fine sand. Reddish brown (2.5YR5/3-4) with some pinkish gray (5YR6/2) high-carbonate zones, and minor weak red (10R4/3) "bodies." 60% sand (vf-m), 40% fines, and trace vf pbls. Arkosic grain/clast mineralogy. Very calcareous (ev). SM-SC , <i>Sandy loam to sandy clay loam</i> .
1450-1460	Sandy clay. Reddish brown (5YR4/3) dominant, with reddish gray to reddish brown (5YR5/2-3). 52% sand (vf-vc), 45% fines, and 3% pbls (vf-f). Grain/clast angularity/rounding and arkosic mineralogy as above (910+); with trace gray chert. Very calcareous (ev), w/ pink <i>can.</i> SM-SC , <i>Sandy clay loam</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>
1460-1470	Sandy clay, as above (1450-1460).

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1470-1480	Silty clay. Reddish brown (2.5-5YR4/3), with some pinkish gray (5YR6/2) high-carbonate zones. 70% fines, 30% sand (vf-m) and trace vf-f pbls. Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC , <i>Clay loam to clay.</i>
1480-1490	Silty clay, as above (1470-1480); with trace ls or indurated carbonate nodules (cam).
1490-1500	Sandy to silty clay. Brown (7.5YR5/2), with some pinkish gray (7.5YR6/2) high-carbonate zones. 60% fines and 40% sand (vf-m). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC-CL , <i>Sandy clay to clay loam.</i>
1500-1510	Sandy to silty clay, as above (1490-1500). Brown (7.5YR4/3), with minor pinkish gray (7.5YR6/2) high-carbonate zones and <i>can.</i>
1510-1520	Sandy to silty clay, as above (1490-1510). Reddish brown to brown (5-7.5YR5/2), with minor pinkish gray (7.5YR6/2) high-carbonate zones and <i>can.</i>
Note: Distinct shift from reddish (2.5-5YR) to brownish (7.5YR) hues in 1,490 to 1,520-ft drill cuttings.	
1520-1530	Interbedded(?) sandy to silty clay and sand. Reddish brown (5YR5/3). Fines: 50% silty clay and 50% sand (vf-m). Sand: 85-90% (vf-vc), w/ <5% vf-c pbls and 10% fines; clast max 30mm. Moderately graded; angularity/roundness and arkosic grain/clast mineralogy (as above); w/ coarse quartzite pbl and f pbl of gray chert (Pz). Fines very calcareous (ev), w/ pink <i>can.</i> SM-SC , <i>Sandy loam to sandy clay loam</i> and SW-SP , <i>Sand.</i>
1530-1540	Pebbly, silty fine to coarse sand, moderately sorted. Sand: Reddish brown to brown (5-7.5YR5/3); fines: reddish brown (5YR5/3). 70% Sand (f-vc), 15% pbls (vf-m), and 15% fines. Moderately graded. Angularity/roundness and grain/clast mineralogy, as above (910+); w/ trace gray and black chert (Pz), and one pale yellow (2.5Y8/2) slts fragment. Fines very calcareous (ev). SW-SP , <i>Fine gravelly sand to loamy sand.</i> <u>Remarks: Sieve analysis of representative sample-split.</u>
1540-1550	Sandy to silty clay. Reddish brown (5YR5/3), with some brown to dark grayish brown (7.5-10YR4/2) zones. 60% fines, 40% sand (vf-m), and trace vf pbls. Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC , <i>Sandy clay to clay loam.</i>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1550-1560	Sandy to silty clay—dominant; with interbedded(?) silty sand. Brown to dark grayish brown (7.5-10YR4/2). Fines: 50% silty clay and 50% sand (vf-m). Sand: 80% (vf-vc), 20% fines, and trace w/ vf-f pbls. Moderately graded; angularity/roundness and arkosic grain/clast mineralogy (as above); w/ coarse quartzite pbl and f pbl of gray chert (Pz). Fines very calcareous (ev), w/ pink <i>can.</i> SM-SC , <i>Sandy loam to sandy clay loam</i> , with SM-SW , <i>Loamy sand and sand</i> .
1560-1570	Pebbly coarse sand, well sorted; with interbedded(?) silty clay. Sand: Reddish brown (5YR5/3); fines: Reddish brown (2.5-5YR4-5/3). Coarse fraction: 62% sand (m-vc) and 33% pbls (vf-c) in sieved sample. Poorly graded, w/ grain/clast angularity/rounding as above (910+). Arkosic grain/clast mineralogy, w/ trace ss, and gray and black chert (Pz). Fines very calcareous (ev). SP , <i>Fine gravelly sand</i> and SC-CL , <i>Clay loam to clay</i> . <u>Remarks: Coarser fraction of sampled-interval selected for sieve analysis.</u>

Note: Pebbly sands in the 1530-40 and 1560-70 ft sample intervals mark the basal coarse-grained (alluvial-channel) facies in the Middle Santa Fe hydrostratigraphic unit (HSU MSF, LFA's 3 and 5a[?]) and Tesuque Fm-Lithosome S.

1570-1580	Silty clay to clay. Reddish brown (2.5YR4/3)—dominant, with dark reddish gray (5YR4/2). 80% fines, 20% sand (vf-f), and trace(?) vf – f pbls, as above (1560-1570). Very calcareous (ev), w/ pink <i>can.</i> CL-ML , <i>Clay to clay loam</i> .
1580-1590	Very fine sandy to silty clay. Dark reddish gray (5YR4/2). 70% fines, 30% sand (vf-m) and trace vf-f pbls, as above (1560-1570). Very calcareous (ev), w/ pinkish gray <i>can.</i> SC-CL , <i>Clay loam to clay</i> .
1590-1600	Very fine sandy to silty clay, as above (1580-1590). Reddish brown (5YR4/3) and brown (7.5YR4/3).
1600-1610	Fine sandy to silty clay. Reddish brown (2.5YR4-5/3). 65% fines, 35% sand (vf-m, w/ minor c-vc). Arkosic grain mineralogy, as above. Very calcareous (ev). SC-CL , <i>Sandy clay to clay loam</i> . <u>Remarks: Sieve analysis of representative sample-split.</u>

Note: Better consolidation (compaction) in drill cuttings below 1,600-1,610 ft, and shift from sands and silty clays to soft sandstones to mudstones.

1610-1620	Clay to silty clay. Reddish brown to weak red (2.5YR-10R4/4), with some light gray (5Y7/1) "reduction zones." 90% fines and 10% sand (vf-f). Very calcareous (ev). CL , <i>Clay</i> .
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Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1620-1630	Clay to silty clay, as above (1610-1620—weak red); interbedded(?) with very fine sandy clay (reddish brown—2.5YR5/3). Sandy clay: 75% fines and 25% sand (vf). Very calcareous (ev). CL , <i>Clay</i> and SC , <i>Clay loam</i> .
1630-1640	Clay to silty clay. Reddish brown (2.5YR4-5/4). 85-90% fines and 10-15% sand (vf). Very calcareous (ev), w/ <i>can</i> . CL , <i>Clay</i> . <u>Remarks: With few "reduction zones," as above (1610-1630).</u>
1640-1650	Clay to silty clay, as above (1630-1640, reddish brown (2.5YR4/4).
1650-1660	Clay to silty clay. Reddish brown to red (2.5YR4/4-6) and weak red (10R4/4). 90% fines and 10% sand (vf-f, w/ trace m-c). Very calcareous (es). CL , <i>Clay</i> . <u>Remarks: With few "reduction zones," as above (1610-1650), and "MnO dendrites."</u>
1660-1670	Clay to silty clay, as above (1630-1650, reddish brown (2.5YR4/4), with minor interbedded(?) silty fine to very fine sand. Sand: Weak red (2.5YR5/2), 85% (vf-f); fines: 15%.
1670-1680	Clay to silty clay. Weak red to reddish brown (10R-2.5YR4/3). 90% fines and 10% sand (vf-f). Very calcareous (es-ev). CL , <i>Clay</i> . <u>Remarks: With trace "reduction zones," as above (1610-1670).</u>
1680-1690	Clay to silty clay, as above (1670-1680)
1690-1700	Clay to silty clay, as above (1670-1680)
1700-1710	Silty clay to clay. Weak red to reddish brown (10R-2.5YR4/3). 80% fines and 20% sand (vf-f). Very calcareous (ev) , w/ trace pink (10R8/3-4) <i>can</i> . CL , <i>Clay to clay loam</i> .

Note: Near contact of main body of the Tesuque Fm (Lithosome S) on Tesuque-Lithosome E of Johnson and others (2004). The latter grayish brown unit (upper Oligocene?), with intermediate to basaltic-volcanic clasts, is correlative with the Tesuque-Bishops Lodge Mbr (Smith,2000) and basal Santa Fe Gp deposits derived from volcanic rocks of the Cerrillos Hills area (including the Espinaso Fm and Cieneguilla Limburgite [basanite] of Disbow and Stoll (1957) and Sun and Baldwin (1958).

1710-1720 Pebbly sandy mudstone and silty fine sandstone (soft). Dark gray to dark grayish brown (10YR4/1-2) dominant, with some gray to grayish brown (10YR5/1-2), and minor reddish brown (5YR5/3). 45% fines, 45% sand (vf-c), and 10% pbls (vf-m). Well graded, w/ angular to subrounded grains and clasts. Mixed grain/clast mineralogy, including intermediate-basaltic volcanics, volcanoclastic slts and ss, quartz, K-feldspar, and arkosic lithics. Very calcareous (es-ev), w/ trace light gray (10YR7/1) "zones"/ segregations (*can*), and sparry calcite cement on some pebbles.

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1720-1730	Fine sandy mudstone (soft), as above (1710-1720). Dark gray to dark grayish brown (10YR4/1-2). 50% fines and 50% sand (vf-c), with trace vf-f pbls.
1730-1740	Fine sandy mudstone (soft), as above (1720-1730). Dark grayish brown to brown (10YR4/2-3), with minor reddish brown (5YR4/3).
1740-1750	Fine sandy mudstone (soft), as above (1720-1740). Dark grayish brown to brown (10YR4/2-3), with minor reddish brown (5YR4/3).
1750-1760	Fine sandy mudstone (soft), as above (1720-1750). Dark gray to grayish brown (10YR4-5/1-2), with minor reddish brown to brown (5-7.5YR4/3). Trace(?) vf-f pebbles.

Note: Bottom of geophysical-logged interval at about 1,760ft.

1760-1770	Fine sandy mudstone (soft), as above (1720-1760). Brown to dark grayish brown (7.5-10YR4/2), with some gray (10YR6/1) very calcareous "zones."
1770-1780	Coarse sandstone to conglomeratic (vf pbly) sandstone (hard to soft). Gray (10YR5/1). Mixed intermediate-volcanic and arkosic lithic types and minerals; w/ coarse fragments (25mm max) of gray volcanoclastic(?) ss. Non- to slightly calcareous (e).
1780-1790	Silty sandstone to fine sandy mudstone (soft), with hard volcanoclastic(?) sandstone fragments, as above (1770-1780), and trace vf-f pbls. Brown to gray (7.5YR4/2 to 10YR5/1), with minor gray (7.5YR5/1) and reddish brown (5YR4/3). Mixed arkosic-volcanic grains and clasts as above (1710-1780). Non- to very calcareous (e-ev).
1790-1800	Fine sandy mudstone and silty sandstone (soft to hard). Gray (7.5-10YR5/1) and dark gray (10YR4/1). Trace of vf-f pbls of intermediate to basaltic volcanics. Very calcareous (es-ev).

Note: Bottom of Hole at 1,802ft (elev. ~4,673 asl).

**TABLE B. INTERPRETIVE LITHOLOGIC LOG BASED ON
COMPARITIVE ANALYSES OF DRILL CUTTINGS
AND BOREHOLE GEOPHYSICS IN PILOT HOLE FOR
OBSERVATION WELL OB-A, RANCHO VIEJO**

Well Name: OB-A Pilot Hole
Location): T16N, R9E, Section 29.111
Lat/Long: 35°35'43" N, 106°01'05" W
State Plane Coordinates (est.): X=569100 (1709332) Y=1671600 (1672077)
Elevation: 6,475ft asl
Total Depth: 1,802 ft
Geophysical Logging: to 1,760 ft

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
0-20	Pebbly sand to silty sand, poorly sorted. Dark reddish gray to reddish brown (5YR4/2-4). Sand (vf-vc), with 10% vf-m pebble (pbl) gravel in upper 10ft and 25-30% silt in lower 10ft. Well graded, angular to subangular sand grains and gravel clasts. Arkosic mineralogy (quartz, K-feldspar, K-mica, and granite-gneiss/pegmatite lithics—derived from local Pre-Cambrian terrane); w/ one f pbl of brown chert noted (Pz-derived). Calcareous (e-es). SW-SM , <i>Sand to sandy loam</i> .

Note: Top (?) of Upper Santa Fe-Ancha Fm (Pliocene-Early Pleistocene) within 5-10 ft of land surface. Upper Santa Fe Hydrostratigraphic Unit (HSU) USF1, Lithofacies Assemblage (LFA) 5b

20-30	Sandy pebble gravel, poorly sorted. Reddish brown (5YR4/3). 60% pbls (vf-vc), 35% sand (vf-vc), and 5% silt. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/ mica flakes and 64mm subrounded granite pbl. Noncalcareous. GW , <i>Sandy fine gravel</i> . HSU-USF1, LFA5a
30-67	Fine pebbly sand, poorly sorted, <i>fining upward</i> into silty sand in upper 10 ft; and with interbedded silty fine to coarse sand from 50-60 ft. Reddish brown (5YR4-5/3-4). 10-15% pbls (vf-f) in 40-50 and 60-67 ft intervals; and 25-30% silt and 5% pbls in silty sand layer. Well graded, angular to subrounded grains and clasts. Arkosic-micaceous mineralogy (as above). Noncalcareous. SW , <i>Sand</i> and SM , <i>Loamy sand</i> . HSU-USF1, LFA5

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
67-80	<p>Pebbly sand, slightly silty and poorly sorted, <i>fining upward</i> into silty sand, w/ some interbedded(?) very fine sandy silt. Reddish brown (5YR4-5/3) to dark brown and brown (7.5YR3/2-5/3). 80-90% sand (vf-vc), 10-15% silt, and up to 10% vf-m pbls. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/common mica flakes. Calcareous (e-es). SM, <i>Loamy sand // SW, Sand</i>. <u>Remarks: Possible buried soil in upper 5 ft.</u> HSU-USF1, LFA5</p>
80-100	<p>Pebbly sand, poorly sorted, <i>fining upward</i> into silty to sandy clay. Reddish brown (5YR4-5/3) to reddish gray (5YR5/2). 80-85% sand (vf-vc) and 5-10% pbls (vf-m) in basal part, and 60% silt-clay fraction (fin) in upper 10 ft. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Calcareous (es-ev), with trace (mostly pink, 2.5-5YR7/3) soft carbonate segregations (<i>can</i>). SM-SC, <i>Sandy loam-sandy clay loam // SW, Sand</i>. HSU-USF1, LFA5</p>
100-130	<p>Sandy pebble gravel, poorly to moderately sorted, <i>fining upward</i> into poorly sorted silty sand. Reddish brown (5YR5/3-4), with some reddish gray (5YR5/2) silty zones. 60% pbls (vf-m) and 40% sand (f-vc) in basal part; and 80-85% sand (vf-vc) and 10-15% fines in upper 10 ft. Moderately to well graded, angular to subrounded grains and clasts; clast max: 15mm. Arkosic grain/clast mineralogy (as above). Very calcareous (ev), with trace pink <i>can</i> in upper part. SW-SM, <i>Sand to loamy sand // GW, Sandy fine gravel to</i>. HSU-USF1, LFA5</p>
130-205	<p>Pebbly sand, clean to slightly silty and poorly sorted; with interbedded pebble gravel and sand from 130-165, 175-185 and 195-205 ft. Reddish brown (5YR5/3-4). 40-70% sand (vf-vc), 30-60% pbls (vf-m), and up to 10% fines. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy, w/ minor dark quartzite and diorite). Calcareous fine fraction w/ trace <i>can</i>. SW-GW, <i>Sand to very fine gravelly sand; with interbedded</i> GW-SW, <i>Sandy fine gravel and very fine gravelly sand</i>. HSU-USF1, LFA5a</p>
205-213	<p>Coarse pebble gravel, poorly to moderately sorted. Reddish brown (5YR5/3). 75% pbls (vf-vc) and 40% sand (f-vc). Moderately to well graded, angular to subrounded grains and clasts; clast max: 45mm. Arkosic grain/clast mineralogy (as above), with gneiss, diorite, and quartzite. Noncalcareous. GW, <i>Fine gravel</i>. HSU-USF1, LFA5a</p>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
<p>Contact of Upper Santa Fe-Ancha Fm on “Lower” Santa Fe-Tesuque Fm, and top of Middle Santa Fe Hydrostratigraphic Unit (HSU) MSF2, Lithofacies Assemblage (LFA) 3at ~213 ft. Depth inferred from “drillograph” records, borehole geophysics, and major texture-mineralogy shift in drill cuttings. Driller noted very coarse gravel (“boulders”) at about 205ft and a shift to much faster bit penetration at 213 ft.</p>	
215-240	<p>Pebble gravel and sand, poorly sorted (230-240 ft), <i>fining upward</i> into silty clay to clay. Fine fraction: reddish brown (2.5YR4/4); 80 fines, >18% sand (vf-c), <2% pbls (vf). Coarse fraction: brown (7.5YR5/3) to reddish brown (5YR5/4); 50% pbls (vf-m) and 50% sand (f-vc). Well graded, w/ angular to rounded grains and angular to subrounded clasts; clast max: 15mm. Arkosic grain/clast mineralogy (quartz, K-feldspar, K-mica, and granite/gneiss lithics) w/ few Pz ss, siltstone (slts), and gray chert. Noncalcareous sand and gvl, and very calcareous (es-ev) fines. CL-ML, <i>Clay to clay loam // GW-SW</i>, <i>Sandy very fine gravel and very fine gravelly sand</i>. <u>Remarks: Interpreted as Lithosome S of the Tesuque Fm (Johnson et al., 2004; Koning and Hallett, 2001 [2006 update]).</u> HSU-MSF2, LFA3</p>
240-300	<p>Silty clay to clay—dominant (240-60, 280-300), with pebble gravel and sand from 260 to 280 ft, as above (230-240). Fines: reddish brown (2.5-5YR4/4-5/3); 70-80% silty clay and 20-30% sand (vf-c), <2% pbls (vf). Arkosic grain/clast mineralogy, as above, including weathered gneiss and/ trace light-gray chert. Slightly to very calcareous (e-ev), w/ few pink <i>can</i>. CL- SC, <i>Clay to clay loam and sandy clay loam</i>. HSU-MSF2, LFA3</p>
300-365	<p>Coarse pebbly sand—dominant, slightly silty and poorly sorted, with minor interbedded sandy clay in lower 35 ft. Reddish brown to light reddish brown (5YR5-6/3). 50-85% sand (vf-vc) and 15-40% pbls (vf-c). Sandy clay: reddish brown (2.5YR4/4). 50% fines, 35% sand (vf-vc), and 5% pbls (vf-m) Well graded, grain/clast angularity/rounding as above (230+); clast max: 30mm. Arkosic grain/clast mineralogy (as above); w/ weathered gneiss and trace quartzite and gray to black chert (Pz). Calcareous fine fraction w/ trace <i>can</i>. SW-GW, <i>Fine gravelly sand</i>. Fine fraction: Reddish brown (2.5-5YR4/4-5/3); 70-80% silty clay and 20-30% sand (vf-c), <2% pbls (vf). Calcareous fine fraction (e-ev), w/ trace <i>can</i>. SW-GW, <i>Fine gravelly sand, w/ minor CL-SC</i>, <i>Clay to clay loam and sandy clay loam</i>. HSU-MSF2, LFA1-2</p>

Note: Water table and capillary fringe in 300 to 310-ft interval.

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
365-400	<p>Fine to medium pebbly sand, poorly sorted (380-400 ft), <i>fining upward</i> into fine sandy to silty clay. Fine fraction: reddish brown (2.5YR4/4). Coarse fraction: reddish brown (5YR5/3-4); 75% sand (vf-vc), 20% pbls (vf-c), and <5% fines; well graded, grain/clast angularity/rounding as above (230+). Arkosic grain/clast mineralogy (as above); w/ highly weathered gneiss fragment, and trace coarse ss and black chert (Pz). Calcareous fine fraction (e-ev), w/ trace <i>can</i>. Sand: Non- to slightly calcareous (e). SC-CL, Clay loam to clay // SW, Fine gravelly sand. HSU-MSF2, LFA3</p>
400-420	<p>Sand, poorly to moderately sorted (410-420ft), <i>fining upward</i> into clay to silty clay. Fine fraction: weak red to reddish brown (10R4/3-2.5-5YR4/4-5); 80-90% fines and 10-20% sand (vf-c), and trace vf-f pbls. Sand: reddish brown (5YR5/3); 85-90% sand (vf-vc), 10% fines, and <5% pbls (vf-m). Well to moderately graded, grain/clast angularity/rounding as above (230+); clast max: 13mm. Arkosic grain/clast mineralogy (as above); w/ trace quartzite, and slts and light reddish brown to pink (2.5YR6-7/3) limestone (ls) fragments (Pz?). Calcareous fine fraction (e-ev), w/ trace <i>can</i>. Sand: Non- to slightly calcareous (e). CL, Clay loam to clay // SW, Sand. <u>Remarks: Some "ls" fragments here and below could be indurated carbonate segregations (cam).</u> HSU-MSF2, LFA3</p>
420-455	<p>Fine sandy to silty clay grading(?) upward into clay. Reddish brown to light reddish brown (2.5-5YR5/4-6/3), with trace weak red (10R4/3). 70-90% fines, 10-30% sand (vf-f), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/ trace slts and weathered calcareous ss (Pz?). Slightly to very calcareous (e-ev), w/ pink <i>can</i>. SC-CL, Clay loam to clay. HSU-MSF2, LFA3,9</p>
455-555	<p>Clay to silty clay—dominant; with some interbedded fine sandy clay and silty fine sand in 510-520, 550-560, and 570-600. Mostly reddish brown (2.5-5YR5/4); with variegated zones in uppermost and mid-part of interval: pale red to reddish brown (10R-2.5YR4-5/3-4), and light reddish brown (2.5YR6/4). 80-90% fines, 10-20% sand (vf-f), and trace vf-f pbls. Arkosic grain mineralogy (as above), w/ trace ls, slts, ss and chert (Pz?). Very to slightly calcareous (e-e), w/ pink <i>can</i> and some black Mn-oxide (MnO) dendrites. CL, Clay, w/ some SM&SC, loamy sand & sandy clay loam. HSU-MSF2, LFA9</p>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
555-595	Sandy and silty clay—dominant, interbedded with silty sand. Fine-grained beds: reddish brown (2.5-5YR4/3-5/4); 70-90% fines, 10-30% sand (vf-c), and trace vf pbls. Sands: reddish brown (2.5YR4/4 & 5YR5/3). 55-65% sand (vf-vc), 35-45% fines, and <5% pbls (vf-f); well graded, w/ angular to rounded sand grains and angular to subrounded pebble clasts; and arkosic grain/clast mineralogy, w/ trace quartzite and chert (Pz). Very calcareous (ev), w/ pink can. SM-SC , <i>Sandy loam to sandy clay loam</i> ; and SC-CL , <i>Sandy clay to clay</i> . HSU-MSF2, LFA3,9
595-655	Silty sand—dominant, poorly sorted, interbedded with sandy to silty clay, as above (555-595). SM-SC , <i>Sandy loam to sandy clay loam</i> ; and SC-CL , <i>Sandy clay to clay</i> . HSU-MSF2, LFA3
555-695	Sandy to silty clay—dominant, interbedded with silty sand, as above (555-595). SM-SC , <i>Sandy loam to sandy clay loam</i> ; and SC-CL , <i>Sandy clay to clay</i> . <u>Remarks: Some K-feldspar, gneiss and ss pebbles are highly weathered and split readily.</u> HSU-MSF2, LFA9,3
695-760	Silty sand—dominant, moderately to poorly sorted, interbedded with sandy to silty clay, as above (555-595). Sand: reddish brown (5YR5/3); 70-80% sand (vf-vc), <20% fines, and <10% pbls (vf-f). Fine fraction: reddish brown (2.5YR4/3-5/4); 70-90% fines, 10-30% sand (vf-c), and trace vf-f pbls. Moderately to well graded sands, grain/clast angularity/rounding as above (600-730). Arkosic grain/clast mineralogy, w/ trace quartzite, ss, and chert (Pz). Fines: very calcareous (ev), w/ pink can. SM , <i>Sandy loam</i> ; and SC-CL , <i>Sandy clay to clay</i> . HSU-MSF2, LFA3
760-870	Clay to silty clay—dominant; with some interbedded sandy clay and silty sand, and basal sand “zone” (855-874). Clays: reddish brown (2.5YR4/4-5YR5/3); 80-90% fines, 10-20% sand (vf-c). Silty sands: reddish brown (2.5-5YR5/3); 60-75% sand (vf-vc), 25-35% fines, and 1-5% pbls (vf-f). Basal sand: 90% sand, 5% pebbles (vf-m), and 5% fines; moderately to well graded, w/ angular to rounded sand grains and angular to subrounded pebble clasts; arkosic grain/clast mineralogy, w/ trace quartzite, ls, ss, and chert. Very calcareous (ev), w/ pink can. SC-CL , <i>Clay loam to clay</i> , with SC-SM , <i>Sandy clay loam to loam</i> , and basal SW , <i>Sand</i> . <u>Remarks: Variegated silty to sandy clay in 840-850 ft sample interval: Reddish brown (5YR4/4-5/3) and light brown to pink (7.5YR6-7/3).</u> HSU-MSF2, LFA9,3

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
870-905	Fine sandy to silty clay—dominant; with minor interbedded(?) silty fine sand, as above. Fines: reddish brown (2.5-5YR4-5/4); sand: reddish brown (5YR5/3). 75-80% fines and 20-25% sand (vf-f), and no(?) pebbles. Arkosic grain mineralogy. Very calcareous (ev), w/ few pink <i>can</i> . SC-CL , <i>clay loam to clay</i> , w/ SM , <i>Sandy clay loam to loam</i> . HSU-MSF2, LFA9
905-1016	Fine to medium pebbly sand, well to poorly sorted; interbedded with Fine sandy clay to clay. Sands: pinkish gray (7.5YR6/2); 70-85% sand (f-vc), 15-25% pbls (vf-m), and <5% fines. Clays: reddish brown (2.5-5YR4-5/4); 65-90% fines and 10-35% sand (vf-m), with trace vf-f pbls. Sands: poorly to well graded; clast max: 13mm; with angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (quartz, K-feldspar, and granite/gneiss lithics), w/ trace marlstone, slts, ls, ss (Fe-MnO cement), and black and brown chert (Pz). Sand: Non calcareous; fines very calcareous (ev). SP-SW , <i>Fine gravelly sand</i> and SC-CL , <i>Clay loam, fine sandy clay and clay</i> . <u>Remarks: Uppermost part of ~400-ft coarsest-grained subunit of the Tesuque Fm-"main body" (Lithosome S of Johnson et al., 2004).</u> HSU-MSF2, LFA3

Note: In samples of sands below 905 ft, well-rounded sand grains are present in only trace amounts or absent, and indicate possible shift to zone of intertonguing of distal piedmont and marginal basin-floor facies (e.g. LFA's 5 & 2-3-9) of Tesuque Lithosome S).

1016-1055 Pebbly, medium to very coarse sand, well sorted; minor interbedded(?) silty clay in lower 10ft . Reddish brown (5YR5/4). 75% sand (m-vc) and 25% pbls (vf-m); fines: weak red to reddish brown (10R4/3-4 to 2.5YR4/4). Poorly graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy, w/ trace slts, ss, ls, and gray "banded" chert (Pz). Sand: Noncalcareous; fines very calcareous (ev). **SP**, *Fine gravelly sand*, with *minor CL, Clay loam to clay*. **HSU-MSF2, LFA1-2**

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1055-1080	<p>Pebbly sand, well to moderately sorted (1070-1080), <i>fining upward</i> into clay to silty clay. Fine fraction: weak red to reddish brown (10R-2.5YR4/3-4); 80-90% fines, 10-20% sand (vf-vc), and trace vf pbls. Coarse fraction: reddish brown (5YR5/4); 73% Sand (m-vc), 25% pbls (vf-m), and 2% fines; clast max: 15mm. Poorly to moderately graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ trace f-c ss and chert (Pz), and sparry-calcite cement on some pebbles; Fines very calcareous (ev), w/ pink <i>can.</i> CL, <i>Clay to clay loam</i> // SP, <i>Fine gravelly sand</i>. HSU-MSF2, LFA3</p>
1080-1140	<p>Pebbly, medium to very coarse sand, well to moderately sorted; with some interbedded sandy pebble gravel. Sands: reddish brown (5YR5/4); fines: weak red (10R4/3). 65-80% sand (m-vc), 20-35% pbls (vf-c), and 1-2% fines. Poorly to moderately graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ trace white "marlstone," ss and chert (Pz), and few fragments of rounded, coarse pbls of metaquartzite. Noncalcareous to very calcareous (ev), w/ sparry-calcite cement on some pebbles. SP, <i>Fine gravelly sand</i>, with some GP, <i>Sandy gravel</i>. HSU-MSF2, LFA1-2</p>
1140-1200	<p>Pebbly sand to sandy pebble gravel, well sorted (1160-1200), <i>fining upward</i> into sandy to silty clay and clay; with some small-scale interbedding of sandy clay and sand. Fine fraction: weak red to reddish brown (10R-2.5YR4/3); 60-80% fines, 20-40% sand (vf-f), and trace vf-f pbls. Coarse fraction: reddish brown (5YR5/4); 50-60% sand (m-vc) and 40-50% pbls (vf-vc); poorly graded, w/ grain/clast angularity/rounding and arkosic mineralogy, as above (905+); w/ trace siliceous ss, chalcedony, and gray and brown chert (Pz), and fragment of vc gneiss pebble. Noncalcareous to very calcareous (ev), w/ pink <i>can</i>, and sparry-calcite cement on some pebbles. CL, <i>Clay loam to clay</i> // SP, <i>Fine gravelly sand</i>. HSU-MSF2, LFA3,2</p>
1200-1265	<p>Pebbly sand, moderately to well sorted, with some interbedded silty to clayey (muddy) sand (1215-1260); <i>fining upward</i> into sandy to silty clay. Fine fraction: weak to pale red (10R4/3-5/4) and reddish brown (2.5YR4-5/3-4). Sand: reddish brown (5YR5/4); 75-85% Sand (f-vc), 10-15% pbls (vf-m), and <10% fines. Moderately to poorly graded. Angularity/roundness and grain/clast mineralogy, as above (910+); w/ trace slts and chert (Pz), and fragment of coarse, rounded pbl of metaquartzite. Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev) w/ pink <i>can</i>. SW-SP, <i>Fine gravelly sand</i>. HSU-MSF2, LFA3</p>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1265-1320	<p>Pebbly sand, moderately to well sorted (1300-1320), <i>fining upward</i> into silty clay and clay, with minor interbedded sand. Clays: reddish brown (2.5YR4/3-4) and weak and pale red to reddish brown (10R-2.5YR4-5/3-4), sandy clay: reddish brown (2.5YR5/4). Sand: reddish brown (5YR5/4); 80-85% sand (vf-vc), 5-10% pbls (vf-m), and 10% fines. Moderately poorly graded. Angularity/roundness and grain/clast mineralogy, as above (910+); w/ trace ss and chert (Pz), and quartzite (pC). Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev). CL-SC, <i>Clay to sandy clay loam</i> // SW-SP, <i>Fine gravelly sand</i>. <u>Remarks: Basal part of ~400-ft thick, coarsest-grained subunit of the Tesuque Fm "main body" (Lithosome S of Johnson et al., 2004?).</u> HSU-MSF2, LFA3,9</p>
1320-1395	<p>Clay and silty clay—dominant, with minor interbedded silty sand and sandy clay. Clays: reddish brown (2.5-5YR4/4 and 5YR5/3-4); 55-85% fines, 15-45% sand (vf-m), and trace c-vc sand and vf pbls. Sand: reddish brown (5YR5/4); 75% sand (vf-m), 25% fines, and trace pbls (vf); with w/ grain angularity/rounding and mineralogy as above (910+). Very calcareous (ev), w/ pinkish gray (7.5YR6/2) <i>can.</i> SC-CL, <i>Sandy clay loam to clay</i>, with minor SM, <i>Sandy clay loam</i>. <u>Remarks: With few light gray (2.5-5YR7/1) "reduction zones," and fragments of micaceous silty very fine sand (light gray, 5Y7/1).</u> HSU-MSF2, LFA9</p>
1395-1475	<p>Sandy to silty clay—dominant, with some interbedded silty to clayey (muddy) fine sand. Clays: reddish brown (2.5-5YR4-5/3)—dominant, with variegated zones: reddish gray to brown (5-7.5YR5/2) and reddish brown (as above). 30-60% sand (vf-c), 40-70% fines, and <5% vf-m pbls. Sand: reddish brown (2.5YR5/3-4), and minor weak red (10R4/3) "bodies;" 60% sand (vf-m), 40% fines, and trace vf pbls. Arkosic grain/clast mineralogy; grain/clast angularity/rounding and arkosic mineralogy as above (910+); with trace gray chert and weathered intermediate volcanics(?). Very calcareous (ev), w/ pinkish gray (5YR6/2) high-carbonate "zones" and <i>can.</i> SC, <i>Sandy clay loam to clay</i>, and SM, <i>sandy loam to sandy loam</i>. HSU-MSF2, LFA9,3</p>
1475-1510	<p>Sandy to silty clay. Brown (7.5YR4/3-5/2)—dominant, with some pinkish gray (7.5YR6/2) high-carbonate zones, and minor reddish brown (5YR5/2) in lower 10 ft. 60% fines and 40% sand (vf-m). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC-CL, <i>Sandy clay to clay loam</i>. <u>Remarks: Distinct shift from reddish (2.5-5YR) to brownish (7.5YR) hues in 1,490 to 1,520-ft drill cuttings.</u> HSU-MSF2, LFA9</p>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1510-1575	<p>Sandy to silty clay with few sand layers (1510-30, 1540-60); interbedded with well to moderately sorted pebbly sand and sand (1530-40, 1560-75). Fine fraction: reddish brown (5YR5/3); 50% silty clay and 50% sand (vf-m). Coarse fraction: reddish brown to brown (5-7.5YR5/3); 60-85% (vf-vc), 15-35% vf-c pbls and 5-15% fines; clast max 30mm. Moderately graded; angularity/roundness and arkosic grain/clast mineralogy, as above (910+); w/ trace ss, slts, gray and black chert (Pz), and coarse quartzite pbls. Fines very calcareous (ev), w/ pink <i>can.</i> SM-SC, <i>Sandy loam to sandy clay loam</i> and SP-SW, <i>Sand and fine gravelly sand</i>. HSU-MSF2, LFA3,9</p>
<p>Note 1: Pebbly sands in the 1530-40 and 1560-70 ft sample intervals mark the basal coarse-grained (alluvial-channel) facies in Tesuque Fm-Lithosome S, and the (<i>provisional</i>) base of the Middle Santa Fe hydrostratigraphic unit (HSU MSF, <i>LFA's 3 and 5[?]</i>). Dominantly fine-grained basin fill between 1,575 and 1,685 ft in the OB-A pilot hole, and underlying beds of Lithosome S (1,685-1,743 ft) are here placed in an (informal) Lower Santa Fe hydrostratigraphic unit (HSU LSF).</p> <p>Note 2: Better consolidation (compaction) in drill cuttings below 1,600-ft sample interval, and shift from sands and silty clays to <i>soft</i> sandstones to mudstones.</p>	
1575-1615	<p>Fine sandy to silty clay. Reddish brown (2.5YR4-5/3)—dominant, with dark reddish gray (5YR4/2) and brown (7.5YR4/3). 65-80% fines, 20-35% sand (vf-m, w/ minor c-vc). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC-CL, <i>Sandy clay to clay loam</i>. HSU-LSF, LFA9,3</p>
1615-1685	<p>Clay to silty clay—dominant, with some interbedded very fine sandy clay. Weak red to reddish brown (10R-2.5YR4/3)—dominant; with variegated “zones:” reddish brown to weak red and red (2.5YR4-5/3-4 to 10R4/4 and 2.5YR4/6), and some light gray (5Y7/1) “reduction zones” and black MnO “dendrites.” 80-90% fines and 10-20% sand (vf-f). Very calcareous (ev), w/ trace pink (10R8/3-4) <i>can.</i> CL-SC, <i>Clay, w/ sandy clay</i>. HSU-LSF, LFA9</p>

Description and Classification of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
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Note: Near contact of main body of the Tesuque Fm (Lithosome S) on Tesuque-Lithosome E of Johnson and others (2004) at 1,685 ft. The latter grayish brown unit (upper Oligocene?), with intermediate to basaltic volcanic clasts, is correlative with the Tesuque-Bishops Lodge Mbr (Smith, 2000) and basal Santa Fe Gp deposits derived from volcanic rocks of the Cerrillos Hills area (including the Espinaso Fm and Cieneguilla Limburgite [basanite] of Disbow and Stoll (1957) and Sun and Baldwin (1958). This interpretation is based on visual analysis of drill cuttings and information from borehole geophysical logs (primarily resistivity, conductivity, and gamma ray).

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| 1685-1695 | Pebbly sandy mudstone and silty fine sandstone (soft). Dark gray to dark grayish brown (10YR4/1-2) dominant, with some gray to grayish brown (10YR5/1-2), and minor reddish brown (5YR5/3). 45% fines, 45% sand (vf-c), and 10% pbls (vf-m). Well graded, w/ angular to subrounded grains and clasts. Mixed grain/clast mineralogy (andesite-latitude porphyry, basalt(?), volcanoclastic slts and ss, quartz, K-feldspar, and arkosic lithics. Very calcareous (es-ev), w/ trace light gray (10YR7/1) "zones"/ segregations (<i>can</i>), and sparry calcite cement on some pebbles. HSU-LSF, LFA9(R) |
| 1695-1743 | Fine sandy mudstone (soft), as above (1710-1720 sample interval). Dark gray to dark grayish brown and brown (10YR4-5/1-3); with brown to dark grayish brown (7.5-10YR4/2) beds. 50% fines and 50% sand (vf-c), with trace vf-f pbls. Very calcareous (es-ev), w/ <i>can</i> and light gray (10YR6-7/1) "zones" in lower 10 ft.
<u>Remarks: Bottom of geophysical-logging interval at about 1,760ft.</u>
HSU-LSF, LFA9 |

Note: Drilling records show major shift to harder material and slower drilling at about 1,743 ft (probably hard sandstones in 1770-1780 sample interval). Unit penetrated below 1,743 ft here interpreted as either basal Tesuque Fm—Bishops Lodge Mbr or pre-Santa Fe Gp volcanoclastic bedrock correlative with the upper Espinaso Fm and/or the Cieneguilla "basanite."

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| 1743-1800 | Coarse sandstone to conglomeratic (vf pibly) sandstone (hard to soft), and fine sandy mudstone and silty sandstone (soft and hard). Gray to brown (10YR5/1 to 7.5YR4/2-5/1) and dark gray (10YR4/1), with minor reddish brown (5YR4/3). Mixed intermediate-volcanic to basaltic, and arkosic lithic types and minerals; w/ coarse fragments (25mm max) of gray volcanoclastic(?) ss. Non- to very calcareous (e-ev). HSU-LSF(?), LFA9(R) |
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TABLE C. SUMMARY OF HYDROSTRATIGRAPHIC AND LITHOFACIES INTERPRETATIONS BASED ON COMPARTIVE ANALYSES OF DRILL CUTTINGS AND BOREHOLE GEOPHYSICS IN THE OB-A PILOT HOLE, RANCHO VIEJO

Well Name: OB-A Pilot Hole

Location): T16N, R9E, Section 29.111; **Lat/Long:** 35°35'43" N, 106°01'05" W

State Plane Coordinates (est.): X=569100 (1709332) Y=1671600 (1672077)

Elevation: 6,475ft asl

Total Depth: 1,802 ft

Geophysical Logging: to 1,760 ft

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
0-20	Pebbly sand to silty sand, poorly sorted. Dark reddish gray to reddish brown (5YR4/2-4). Sand (vf-vc), with 10% vf-m pebble (pbl) gravel in upper 10ft and 25-30% silt in lower 10ft. Well graded, angular to subangular sand grains and gravel clasts. Arkosic mineralogy (quartz, K-feldspar, K-mica, and granite-gneiss/pegmatite lithics—derived from local Pre-Cambrian terrane); w/ one f pbl of brown chert noted (Pz-derived). Calcareous (e-es). SW-SM , <i>Sand to sandy loam</i> .
Note: Top (?) of Upper Santa Fe-Ancha Fm (Pliocene-Early Pleistocene) within 5-10 ft of land surface. Upper Santa Fe Hydrostratigraphic Unit (HSU) USF1, Lithofacies Assemblage (LFA) 5b	
20-30	Sandy pebble gravel, poorly sorted. Reddish brown (5YR4/3). 60% pbls (vf-vc), 35% sand (vf-vc), and 5% silt. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/ mica flakes and 64mm subrounded granite pbl. Noncalcareous. GW , <i>Sandy fine gravel</i> . HSU-USF1, LFA5a
30-67	Fine pebbly sand, poorly sorted, <i>fining upward</i> into silty sand in upper 10 ft; and with interbedded silty fine to coarse sand from 50-60 ft. Reddish brown (5YR4-5/3-4). 10-15% pbls (vf-f) in 40-50 and 60-67 ft intervals; and 25-30% silt and 5% pbls in silty sand layer. Well graded, angular to subrounded grains and clasts. Arkosic-micaceous mineralogy (as above). Noncalcareous. SW , <i>Sand</i> and SM , <i>Loamy sand</i> . HSU-USF1, LFA5

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
67-80	<p>Pebbly sand, slightly silty and poorly sorted, <i>fining upward</i> into silty sand, w/ some interbedded(?) very fine sandy silt. Reddish brown (5YR4-5/3) to dark brown and brown (7.5YR3/2-5/3). 80-90% sand (vf-vc), 10-15% silt, and up to 10% vf-m pbls. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above), w/common mica flakes. Calcareous (e-es). SM, <i>Loamy sand</i> // SW, <i>Sand</i>. <u>Remarks: Possible buried soil in upper 5 ft.</u> HSU-USF1, LFA5</p>
80-100	<p>Pebbly sand, poorly sorted, <i>fining upward</i> into silty to sandy clay. Reddish brown (5YR4-5/3) to reddish gray (5YR5/2). 80-85% sand (vf-vc) and 5-10% pbls (vf-m) in basal part, and 60% silt-clay fraction (fin) in upper 10 ft. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above). Calcareous (es-ev), with trace (mostly pink, 2.5-5YR7/3) soft carbonate segregations (<i>can</i>). SM-SC, <i>Sandy loam-sandy clay loam</i> // SW, <i>Sand</i>. HSU-USF1, LFA5</p>
100-130	<p>Sandy pebble gravel, poorly to moderately sorted, <i>fining upward</i> into poorly sorted silty sand. Reddish brown (5YR5/3-4), with some reddish gray (5YR5/2) silty zones. 60% pbls (vf-m) and 40% sand (f-vc) in basal part; and 80-85% sand (vf-vc) and 10-15% fines in upper 10 ft. Moderately to well graded, angular to subrounded grains and clasts; clast max: 15mm. Arkosic grain/clast mineralogy (as above). Very calcareous (ev), with trace pink <i>can</i> in upper part. SW-SM, <i>Sand to loamy sand</i> // GW, <i>Sandy fine gravel</i> to. HSU-USF1, LFA5</p>
130-205	<p>Pebbly sand, clean to slightly silty and poorly sorted; with interbedded pebble gravel and sand from 130-165, 175-185 and 195-205 ft. Reddish brown (5YR5/3-4). 40-70% sand (vf-vc), 30-60% pbls (vf-m), and up to 10% fines. Well graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy, w/ minor dark quartzite and diorite). Calcareous fine fraction w/ trace <i>can</i>. SW-GW, <i>Sand to very fine gravelly sand</i>; with interbedded GW-SW, <i>Sandy fine gravel and very fine gravelly sand</i>. HSU-USF1, LFA5a</p>
205-213	<p>Coarse pebble gravel, poorly to moderately sorted. Reddish brown (5YR5/3). 75% pbls (vf-vc) and 40% sand (f-vc). Moderately to well graded, angular to subrounded grains and clasts; clast max: 45mm. Arkosic grain/clast mineralogy (as above), with gneiss, diorite, and quartzite. Noncalcareous. GW, <i>Fine gravel</i>. HSU-USF1, LFA5a</p>

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
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Note: Contact of Upper Santa Fe-Ancha Fm on “Lower” Santa Fe-Tesuque Fm, and top of Middle Santa Fe Hydrostratigraphic Unit (HSU) MSF2, Lithofacies Assemblage (LFA) 3at ~213 ft. Depth inferred from “drillograph” records, borehole geophysics, and major texture-mineralogy shift in drill cuttings. Driller noted very coarse gravel (“boulders”) at about 205ft and a shift to much faster bit penetration at 213 ft.

215-240	<p>Pebble gravel and sand, poorly sorted (230-240 ft), <i>fining upward</i> into silty clay to clay. Fine fraction: reddish brown (2.5YR4/4); 80 fines, >18% sand (vf-c), <2% pbls (vf). Coarse fraction: brown (7.5YR5/3) to reddish brown (5YR5/4); 50% pbls (vf-m) and 50% sand (f-vc). Well graded, w/ angular to rounded grains and angular to subrounded clasts; clast max: 15mm. Arkosic grain/clast mineralogy (quartz, K-feldspar, K-mica, and granite/gneiss lithics) w/ few Pz ss, siltstone (slts), and gray chert. Noncalcareous sand and gvl, and very calcareous (es-ev) fines. CL-ML, <i>Clay to clay loam</i> // GW-SW, <i>Sandy very fine gravel and very fine gravelly sand</i>. <u>Remarks: Interpreted as Lithosome S of the Tesuque Fm (Johnson et al., 2004; Koning and Hallett, 2001 [2006 update]).</u> HSU-MSF2, LFA3</p>
240-300	<p>Silty clay to clay—dominant (240-60, 280-300), with pebble gravel and sand from 260 to 280 ft, as above (230-240). Fines: reddish brown (2.5-5YR4/4-5/3); 70-80% silty clay and 20-30% sand (vf-c), <2% pbls (vf). Arkosic grain/clast mineralogy, as above, including weathered gneiss and/ trace light-gray chert. Slightly to very calcareous (e-ev), w/ few pink <i>can</i>. CL- SC, <i>Clay to clay loam and sandy clay loam</i>. HSU-MSF2, LFA3</p>
300-365	<p>Coarse pebbly sand—dominant, slightly silty and poorly sorted, with minor interbedded sandy clay in lower 35 ft. Reddish brown to light reddish brown (5YR5-6/3). 50-85% sand (vf-vc) and 15-40% pbls (vf-c). Sandy clay: reddish brown (2.5YR4/4). 50% fines, 35% sand (vf-vc), and 5% pbls (vf-m) Well graded, grain/clast angularity/rounding as above (230+); clast max: 30mm. Arkosic grain/clast mineralogy (as above); w/ weathered gneiss and trace quartzite and gray to black chert (Pz). Calcareous fine fraction w/ trace <i>can</i>. SW-GW, <i>Fine gravelly sand</i>. Fine fraction: Reddish brown (2.5-5YR4/4-5/3); 70-80% silty clay and 20-30% sand (vf-c), <2% pbls (vf). Calcareous fine fraction (e-ev), w/ trace <i>can</i>. SW-GW, <i>Fine gravelly sand, w/ minor</i> CL-SC, <i>Clay to clay loam and sandy clay loam</i>. HSU-MSF2, LFA1-2</p>

Note: Water table and capillary fringe in 300 to 310-ft interval.

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
365-400	Fine to medium pebbly sand, poorly sorted (380-400 ft), <i>fining upward</i> into fine sandy to silty clay. Fine fraction: reddish brown (2.5YR4/4). Coarse fraction: reddish brown (5YR5/3-4); 75% sand (vf-vc), 20% pbls (vf-c), and <5% fines; well graded, grain/clast angularity/rounding as above (230+). Arkosic grain/clast mineralogy (as above); w/ highly weathered gneiss fragment, and trace coarse ss and black chert (Pz). Calcareous fine fraction (e-ev), w/ trace <i>can</i> . Sand: Non- to slightly calcareous (e). SC-CL , <i>Clay loam to clay // SW</i> , <i>Fine gravelly sand</i> . HSU-MSF2, LFA3
400-420	Sand, poorly to moderately sorted (410-420ft), <i>fining upward</i> into clay to silty clay. Fine fraction: weak red to reddish brown (10R4/3-2.5-5YR4/4-5); 80-90% fines and 10-20% sand (vf-c), and trace vf-f pbls. Sand: reddish brown (5YR5/3); 85-90% sand (vf-vc), 10% fines, and <5% pbls (vf-m). Well to moderately graded, grain/clast angularity/rounding as above (230+); clast max: 13mm. Arkosic grain/clast mineralogy (as above); w/ trace quartzite, and slts and light reddish brown to pink (2.5YR6-7/3) limestone (ls) fragments (Pz?). Calcareous fine fraction (e-ev), w/ trace <i>can</i> . Sand: Non- to slightly calcareous (e). CL , <i>Clay loam to clay // SW</i> , <i>Sand</i> . <u>Remarks: Some "ls" fragments here and below could be indurated carbonate segregations (<i>cam</i>).</u> HSU-MSF2, LFA3
420-455	Fine sandy to silty clay grading(?) upward into clay. Reddish brown to light reddish brown (2.5-5YR5/4-6/3), with trace weak red (10R4/3). 70-90% fines, 10-30% sand (vf-f), and trace vf-f pbls. Arkosic grain/clast mineralogy (as above), w/ trace slts and weathered calcareous ss (Pz?). Slightly to very calcareous (e-ev), w/ pink <i>can</i> . SC-CL , <i>Clay loam to clay</i> . HSU-MSF2, LFA3,9
455-555	Clay to silty clay—dominant; with some interbedded fine sandy clay and silty fine sand in 510-520, 550-560, and 570-600. Mostly reddish brown (2.5-5YR5/4); with variegated zones in uppermost and mid-part of interval: pale red to reddish brown (10R-2.5YR4-5/3-4), and light reddish brown (2.5YR6/4). 80-90% fines, 10-20% sand (vf-f), and trace vf-f pbls. Arkosic grain mineralogy (as above), w/ trace ls, slts, ss and chert (Pz?). Very to slightly calcareous (e-e), w/ pink <i>can</i> and some black Mn-oxide (MnO) dendrites. CL , <i>Clay</i> , w/ some SM&SC , <i>loamy sand & sandy clay loam</i> . HSU-MSF2, LFA9

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
555-595	<p>Sandy and silty clay—dominant, interbedded with silty sand. Fine-grained beds: reddish brown (2.5-5YR4/3-5/4); 70-90% fines, 10-30% sand (vf-c), and trace vf pbls. Sands: reddish brown (2.5YR4/4 & 5YR5/3). 55-65% sand (vf-vc), 35-45% fines, and <5% pbls (vf-f); well graded, w/ angular to rounded sand grains and angular to subrounded pebble clasts; and arkosic grain/clast mineralogy, w/ trace quartzite and chert (Pz). Very calcareous (ev), w/ pink <i>can</i>. SM-SC, <i>Sandy loam to sandy clay loam</i>; and SC-CL, <i>Sandy clay to clay</i>. HSU-MSF2, LFA3,9</p>
595-655	<p>Silty sand—dominant, poorly sorted, interbedded with sandy to silty clay, as above (555-595). SM-SC, <i>Sandy loam to sandy clay loam</i>; and SC-CL, <i>Sandy clay to clay</i>. HSU-MSF2, LFA3</p>
555-695	<p>Sandy to silty clay—dominant, interbedded with silty sand, as above (555-595). SM-SC, <i>Sandy loam to sandy clay loam</i>; and SC-CL, <i>Sandy clay to clay</i>. <u>Remarks: Some K-feldspar, gneiss and ss pebbles are highly weathered and split readily.</u> HSU-MSF2, LFA9,3</p>
695-760	<p>Silty sand—dominant, moderately to poorly sorted, interbedded with sandy to silty clay, as above (555-595). Sand: reddish brown (5YR5/3); 70-80% sand (vf-vc), <20% fines, and <10% pbls (vf-f). Fine fraction: reddish brown (2.5YR4/3-5/4); 70-90% fines, 10-30% sand (vf-c), and trace vf-f pbls. Moderately to well graded sands, grain/clast angularity/rounding as above (600-730). Arkosic grain/clast mineralogy, w/ trace quartzite, ss, and chert (Pz). Fines: very calcareous (ev), w/ pink <i>can</i>. SM, <i>Sandy loam</i>; and SC-CL, <i>Sandy clay to clay</i>. HSU-MSF2, LFA3</p>
760-870	<p>Clay to silty clay—dominant; with some interbedded sandy clay and silty sand, and basal sand “zone” (855-874). Clays: reddish brown (2.5YR4/4-5YR5/3); 80-90% fines, 10-20% sand (vf-c). Silty sands: reddish brown (2.5-5YR5/3); 60-75% sand (vf-vc), 25-35% fines, and 1-5% pbls (vf-f). Basal sand: 90% sand, 5% pebbles (vf-m), and 5% fines; moderately to well graded, w/ angular to rounded sand grains and angular to subrounded pebble clasts; arkosic grain/clast mineralogy, w/ trace quartzite, ls, ss, and chert. Very calcareous (ev), w/ pink <i>can</i>. SC-CL, <i>Clay loam to clay</i>, with SC-SM, <i>Sandy clay loam to loam</i>, and basal SW, <i>Sand</i>. <u>Remarks: Variegated silty to sandy clay in 840-850 ft sample interval: Reddish brown (5YR4/4-5/3) and light brown to pink (7.5YR6-7/3).</u> HSU-MSF2, LFA9,3</p>

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
870-905	<p>Fine sandy to silty clay—dominant; with minor interbedded(?) silty fine sand, as above. Fines: reddish brown (2.5-5YR4-5/4); sand: reddish brown (5YR5/3). 75-80% fines and 20-25% sand (vf-f), and no(?) pebbles. Arkosic grain mineralogy. Very calcareous (ev), w/ few pink <i>can.</i> SC-CL, <i>clay loam to clay</i>, w/ SM, <i>Sandy clay loam to loam</i>. HSU-MSF2, LFA9</p>
905-1016	<p>Fine to medium pebbly sand, well to poorly sorted; interbedded with Fine sandy clay to clay. Sands: pinkish gray (7.5YR6/2); 70-85% sand (f-vc), 15-25% pbls (vf-m), and <5% fines. Clays: reddish brown (2.5-5YR4-5/4); 65-90% fines and 10-35% sand (vf-m), with trace vf-f pbls. Sands: poorly to well graded; clast max: 13mm; with angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (quartz, K-feldspar, and granite/gneiss lithics), w/ trace marlstone, slts, ls, ss (Fe-MnO cement), and black and brown chert (Pz). Sand: Non calcareous; fines very calcareous (ev). SP-SW, <i>Fine gravelly sand</i> and SC-CL, <i>Clay loam, fine sandy clay and clay</i>. <u>Remarks: Uppermost part of ~400-ft coarsest-grained subunit of the Tesuque Fm-“main body” (Lithosome S of Johnson et al., 2004).</u> HSU-MSF2, LFA3</p>

Note: In samples of sands below 905 ft, well-rounded sand grains are present in only trace amounts or absent, and indicate possible shift to zone of intertonguing of distal piedmont and marginal basin-floor facies (e.g. LFA's 5 & 2-3-9) of Tesuque Lithosome S).

1016-1055 Pebbly, medium to very coarse sand, well sorted; minor interbedded(?) silty clay in lower 10ft . Reddish brown (5YR5/4). 75% sand (m-vc) and 25% pbls (vf-m); fines: weak red to reddish brown (10R4/3-4 to 2.5YR4/4). Poorly graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy, w/ trace slts, ss, ls, and gray “banded” chert (Pz). Sand: Noncalcareous; fines very calcareous (ev). **SP**, *Fine gravelly sand*, with *minor CL, Clay loam to clay*. **HSU-MSF2, LFA1-2**

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1055-1080	<p>Pebbly sand, well to moderately sorted (1070-1080), <i>fining upward</i> into clay to silty clay. Fine fraction: weak red to reddish brown (10R-2.5YR4/3-4); 80-90% fines, 10-20% sand (vf-vc), and trace vf pbls. Coarse fraction: reddish brown (5YR5/4); 73% Sand (m-vc), 25% pbls (vf-m), and 2% fines; clast max: 15mm. Poorly to moderately graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ trace f-c ss and chert (Pz), and sparry-calcite cement on some pebbles; Fines very calcareous (ev), w/ pink <i>can</i>. CL, <i>Clay to clay loam</i> // SP, <i>Fine gravelly sand</i>. HSU-MSF2, LFA3</p>
1080-1140	<p>Pebbly, medium to very coarse sand, well to moderately sorted; with some interbedded sandy pebble gravel. Sands: reddish brown (5YR5/4); fines: weak red (10R4/3). 65-80% sand (m-vc), 20-35% pbls (vf-c), and 1-2% fines. Poorly to moderately graded, angular to subrounded grains and clasts. Arkosic grain/clast mineralogy (as above); w/ trace white "marlstone," ss and chert (Pz), and few fragments of rounded, coarse pbls of metaquartzite. Noncalcareous to very calcareous (ev), w/ sparry-calcite cement on some pebbles. SP, <i>Fine gravelly sand</i>, with some GP, <i>Sandy gravel</i>. HSU-MSF2, LFA1-2</p>
1140-1200	<p>Pebbly sand to sandy pebble gravel, well sorted (1160-1200), <i>fining upward</i> into sandy to silty clay and clay; with some small-scale interbedding of sandy clay and sand. Fine fraction: weak red to reddish brown (10R-2.5YR4/3); 60-80% fines, 20-40% sand (vf-f), and trace vf-f pbls. Coarse fraction: reddish brown (5YR5/4); 50-60% sand (m-vc) and 40-50% pbls (vf-vc); poorly graded, w/ grain/clast angularity/rounding and arkosic mineralogy, as above (905+); w/ trace siliceous ss, chalcedony, and gray and brown chert (Pz), and fragment of vc gneiss pebble. Noncalcareous to very calcareous (ev), w/ pink <i>can</i>, and sparry-calcite cement on some pebbles. CL, <i>Clay loam to clay</i> // SP, <i>Fine gravelly sand</i>. HSU-MSF2, LFA3,2</p>
1200-1265	<p>Pebbly sand, moderately to well sorted, with some interbedded silty to clayey (muddy) sand (1215-1260); fining upward into sandy to silty clay. Fine fraction: weak to pale red (10R4/3-5/4) and reddish brown (2.5YR4-5/3-4). Sand: reddish brown (5YR5/4); 75-85% Sand (f-vc), 10-15% pbls (vf-m), and <10% fines. Moderately to poorly graded. Angularity/roundness and grain/clast mineralogy, as above (910+); w/ trace slts and chert (Pz), and fragment of coarse, rounded pbl of metaquartzite. Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev) w/ pink <i>can</i>. SW-SP, <i>Fine gravelly sand</i>. HSU-MSF2, LFA3</p>

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1265-1320	<p>Pebbly sand, moderately to well sorted (1300-1320), <i>fining upward</i> into silty clay and clay, with minor interbedded sand. Clays: reddish brown (2.5YR4/3-4) and weak and pale red to reddish brown (10R-2.5YR4-5/3-4), sandy clay: reddish brown (2.5YR5/4). Sand: reddish brown (5YR5/4); 80-85% sand (vf-vc), 5-10% pbls (vf-m), and 10% fines. Moderately poorly graded. Angularity/roundness and grain/clast mineralogy, as above (910+); w/ trace ss and chert (Pz), and quartzite (pC). Sand: Noncalcareous; sparry-calcite cement on some pebbles; fines very calcareous (ev). CL-SC, <i>Clay to sandy clay loam</i> // SW-SP, <i>Fine gravelly sand</i>. <u>Remarks: Basal part of ~400-ft thick, coarsest-grained subunit of the Tesuque Fm "main body" (Lithosome S of Johnson et al., 2004?).</u> HSU-MSF2, LFA3,9</p>
1320-1395	<p>Clay and silty clay—dominant, with minor interbedded silty sand and sandy clay. Clays: reddish brown (2.5-5YR4/4 and 5YR5/3-4); 55-85% fines, 15-45% sand (vf-m), and trace c-vc sand and vf pbls. Sand: reddish brown (5YR5/4); 75% sand (vf-m), 25% fines, and trace pbls (vf); with w/ grain angularity/rounding and mineralogy as above (910+). Very calcareous (ev), w/ pinkish gray (7.5YR6/2) <i>can.</i> SC-CL, <i>Sandy clay loam to clay</i>, with minor SM, <i>Sandy clay loam</i>. <u>Remarks: With few light gray (2.5-5YR7/1) "reduction zones," and fragments of micaceous silty very fine sand (light gray, 5Y7/1).</u> HSU-MSF2, LFA9</p>
1395-1475	<p>Sandy to silty clay—dominant, with some interbedded silty to clayey (muddy) fine sand. Clays: reddish brown (2.5-5YR4-5/3)—dominant, with variegated zones: reddish gray to brown (5-7.5YR5/2) and reddish brown (as above). 30-60% sand (vf-c), 40-70% fines, and <5% vf-m pbls. Sand: reddish brown (2.5YR5/3-4), and minor weak red (10R4/3) "bodies;" 60% sand (vf-m), 40% fines, and trace vf pbls. Arkosic grain/clast mineralogy; grain/clast angularity/rounding and arkosic mineralogy as above (910+); with trace gray chert and weathered intermediate volcanics(?). Very calcareous (ev), w/ pinkish gray (5YR6/2) high-carbonate "zones" and <i>can.</i> SC, <i>Sandy clay loam to clay</i>, and SM, <i>sandy loam to sandy loam</i>. HSU-MSF2, LFA9,3</p>
1475-1510	<p>Sandy to silty clay. Brown (7.5YR4/3-5/2)—dominant, with some pinkish gray (7.5YR6/2) high-carbonate zones, and minor reddish brown (5YR5/2) in lower 10 ft. 60% fines and 40% sand (vf-m). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC-CL, <i>Sandy clay to clay loam</i>. <u>Remarks: Distinct shift from reddish (2.5-5YR) to brownish (7.5YR) hues in 1,490 to 1,520-ft drill cuttings.</u> HSU-MSF2, LFA9</p>

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
1510-1575	<p>Sandy to silty clay with few sand layers (1510-30, 1540-60); interbedded with well to moderately sorted pebbly sand and sand (1530-40, 1560-75). Fine fraction: reddish brown (5YR5/3); 50% silty clay and 50% sand (vf-m). Coarse fraction: reddish brown to brown (5-7.5YR5/3); 60-85% (vf-vc), 15-35% vf-c pbls and 5-15% fines; clast max 30mm. Moderately graded; angularity/roundness and arkosic grain/clast mineralogy, as above (910+); w/ trace ss, slts, gray and black chert (Pz), and coarse quartzite pbls. Fines very calcareous (ev), w/ pink <i>can.</i> SM-SC, <i>Sandy loam to sandy clay loam</i> and SP-SW, <i>Sand and fine gravelly sand</i>. HSU-MSF2, LFA3,9</p>
<p>Note 1: Pebbly sands in the 1530-40 and 1560-70 ft sample intervals mark the basal coarse-grained (alluvial-channel) facies in Tesuque Fm-Lithosome S, and the (<i>provisional</i>) base of the Middle Santa Fe hydrostratigraphic unit (HSU MSF, LFA's 3 and 5[?]). Dominantly fine-grained basin fill between 1,575 and 1,685 ft in the OB-A pilot hole, and underlying beds of Lithosome S (1,685-1,743 ft) are here placed in an (informal) Lower Santa Fe hydrostratigraphic unit (HSU LSF).</p> <p>Note 2: Better consolidation (compaction) in drill cuttings below 1,600-ft sample interval, and shift from sands and silty clays to <i>soft</i> sandstones to mudstones.</p>	
1575-1615	<p>Fine sandy to silty clay. Reddish brown (2.5YR4-5/3)—dominant, with dark reddish gray (5YR4/2) and brown (7.5YR4/3). 65-80% fines, 20-35% sand (vf-m, w/ minor c-vc). Arkosic grain mineralogy, as above. Very calcareous (ev), w/ pinkish gray <i>can.</i> SC-CL, <i>Sandy clay to clay loam</i>. HSU-LSF, LFA9,3</p>
1615-1685	<p>Clay to silty clay—dominant, with some interbedded very fine sandy clay. Weak red to reddish brown (10R-2.5YR4/3)—dominant; with variegated “zones:” reddish brown to weak red and red (2.5YR4-5/3-4 to 10R4/4 and 2.5YR4/6), and some light gray (5Y7/1) “reduction zones” and black MnO “dendrites.” 80-90% fines and 10-20% sand (vf-f). Very calcareous (ev), w/ trace pink (10R8/3-4) <i>can.</i> CL-SC, <i>Clay, w/ sandy clay</i>. HSU-LSF, LFA9</p>

Description and Interpretation of Major Lithologic Units

Depth (ft)	Description, Classification, and Remarks
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Note: Near contact of main body of the Tesuque Fm (Lithosome S) on Tesuque-Lithosome E of Johnson and others (2004) at 1,685 ft. The latter grayish brown unit (upper Oligocene?), with intermediate to basaltic volcanic clasts, is correlative with the Tesuque-Bishops Lodge Mbr (Smith,2000) and basal Santa Fe Gp deposits derived from volcanic rocks of the Cerrillos Hills area (including the Espinaso Fm and Cieneguilla Limburgite [basanite] of Disbow and Stoll (1957) and Sun and Baldwin (1958). This interpretation is based on visual analysis of drill cuttings and information from borehole geophysical logs (primarily resistivity, conductivity, and gamma ray).

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| 1685-1695 | Pebbly sandy mudstone and silty fine sandstone (soft). Dark gray to dark grayish brown (10YR4/1-2) dominant, with some gray to grayish brown (10YR5/1-2), and minor reddish brown (5YR5/3). 45% fines, 45% sand (vf-c), and 10% pbls (vf-m). Well graded, w/ angular to subrounded grains and clasts. Mixed grain/clast mineralogy (andesite-latitude porphyry, basalt(?), volcanoclastic slts and ss, quartz, K-feldspar, and arkosic lithics. Very calcareous (es-ev), w/ trace light gray (10YR7/1) "zones"/ segregations (<i>can</i>), and sparry calcite cement on some pebbles. HSU-LSF, LFA9(R) |
| 1695-1743 | Fine sandy mudstone (soft), as above (1710-1720 sample interval). Dark gray to dark grayish brown and brown (10YR4-5/1-3); with brown to dark grayish brown (7.5-10YR4/2) beds. 50% fines and 50% sand (vf-c), with trace vf-f pbls. Very calcareous (es-ev), w/ <i>can</i> and light gray (10YR6-7/1) "zones" in lower 10 ft.
<u>Remarks: Bottom of geophysical-logging interval at about 1,760ft.</u>
HSU-LSF, LFA9 |

Note: Drilling records show major shift to harder material and slower drilling at about 1,743 ft (probably hard sandstones in 1770-1780 sample interval). Unit penetrated below 1,743 ft here interpreted as either basal Tesuque Fm—Bishops Lodge Mbr or pre-Santa Fe Gp volcanoclastic bedrock correlative with the upper Espinaso Fm and/or the Cieneguilla "basanite."

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| 1743-1800 | Coarse sandstone to conglomeratic (vf pbly) sandstone (hard to soft), and fine sandy mudstone and silty sandstone (soft and hard). Gray to brown (10YR5/1 to 7.5YR4/2-5/1) and dark gray (10YR4/1), with minor reddish brown (5YR4/3). Mixed intermediate-volcanic to basaltic, and arkosic lithic types and minerals; w/ coarse fragments (25mm max) of gray volcanoclastic(?) ss. Non- to very calcareous (e-ev). <u>Remarks: Bottom of hole at 1,802 ft.</u> HSU-LSF, LFA9(?) |
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PRELIMINARY NOTES ON CCX1 AND OB-A CORRELATIONS (3/24/2006):

1. The lowermost part of the main body of the Tesuque Fm occurs at a depths of ~ 1,500ft in CCX1 (elev. 4,970ft asl) and 1,700ft (elev. 4,775ft asl) in OB-A, respectively, as inferred from both borehole geophysics and drill cutting analysis.
2. Pebbly sands in the 1530-1570ft interval in OB-A (elev. 4945-4,905ft asl) mark the basal coarse-grained (alluvial-channel) facies in the Middle Santa Fe hydrostratigraphic unit (**HSU MSF, LFA's 5a and 3**) and Tesuque Fm-Lithosomes A & S (see **Appendix**). This zone appears to correlate with the basal arkosic sand sequence penetrated in CCX1 between about 1,330-1,380ft (elev 5,220-5,170ft asl). This also indicates that the "average" westward dip of the lower Tesuque Fm is only about 2 to 3° (3.5-5%) in this part of the basin (**which agrees with current interpretations by USGS geophysicists and NMBGMR geologists**).
3. A maximum westward dip of about 2 to 3° in the main body of the Tesuque Fm between the CCX1 and OB-A well sites definitely indicates that the major aquifer zones screened in these wells (~900 to 1,300ft in OB-A, and 740 to 1,300ft in CCX1) are interconnected. This is corroborated by correlations of thick clayey zones encountered in both wells (e.g. 310-425ft and 600-720ft in CCX1, with 455-555ft and 760-905ft in OB-A).
4. The possible hydraulic effects of a small (down-to-the-east, N-trending) fault identified in USGS aeromagnetic surveys between the two well sites has not been evaluated in this phase of the study.

TABLE D. DISTRIBUTION OF MAJOR LITHOFACIES ASSEMBLAGES AND HYDROSTRATIGRAPHIC UNITS IN THE OB-A PILOT HOLE, RANCHO VIEJO— SUMMARY OF HYDROGEOLOGIC INTERPRETATIONS FOR MODEL DEVELOPMENT (FIG. 1, TABLES 1 to 3)

Well Name: OB-A Pilot Hole (Rancho Viejo Project)

Location: T16N, R9E, Section 29.111; **Lat/Long:** 35°35'43" N, 106°01'05" W

State Plane Coordinates (est.): X=569100 (1709332) Y=1671600 (1672077)

Elevation: 6,475ft asl

Total Depth: 1,802 ft

Depth (feet)	Elevation (top, ft)	Lithofacies Assemblage/ Tesuque Fm Lithosome	Hydrostratigraphic Unit
0-10	6,475	b/5	PA/ USF1
10-142	6,465	5,5a	USF1
142-213	6,333	5a	USF1
213-280	6,262	3/S	MSF2
280-300	6,195	9/S	MSF2
300-365	6,175	1-2/S	MSF2
365-455	6,110	3/S	MSF2
455-555	6,020	9/S	MSF2
555-760	5,920	3/S	MSF2
760-870	5,715	9,3/S	MSF2
870-905	5,605	9/S	MSF2
905-1016	5,570	3/S	MSF2
1016-1140	5,459	1-3/S	MSF2
1140-1265	5,335	3/S	MSF2
1265-1320	5,210	3,9/S	MSF2
1320-1395	5,155	9/S	MSF2
1395-1475	5,080	9,3/S	MSF2
1475-1510	5,000	9/S	MSF2
1510-1575	4,965	3,9/S	MSF2
1575-1615	4,900	9,3/S	LSF
1615-1685	4,860	9/S	LSF
1685-1743	4,790	*9/Ttbl-E?	LSF
1743-1802	4,732	*9/Ttbl-E?	LSF
Bottom of Hole	4,673		

Ttbl-E?* Probably Bishop Lodge Mbr, or possibly Lithosome E of the "lower" Tesuque Fm. See **Appendix (p. 49-51).

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APPENDIX: TESUQUE FORMATION LITHOSOME CLASSIFICATION

Lithosomes A and B (Cavazza, 1986; Koning, 2004)

Lithosome A

Lithosome A units are associated with piedmont-slope alluvial depositional environments of the Tesuque Fm along the western base of the Southern Sangre de Cristo Mountains (Santa Fe Range). "These units are characterized by medium to thick, tabular to broadly lenticular beds of silty sandstone interbedded with various proportions of coarser channel deposits of pebbly sandstone, sandstone, and pebble conglomerate. The gravel of lithosome A is generally dominated by granite, with subordinate quartzite, and the sand fraction has abundant pinkish potassium feldspar. Lithosome A is further subdivided according to texture. Finer units (silty very-fine to medium sandstone and siltstone with less than 5-7% coarser sand and gravel channel deposits) are interpreted to generally represent the distal alluvial slope. Coarser units, composed of slightly muddy very-fine to very-coarse sandstone with greater than 5-7% gravelly sand channel deposits, are interpreted to generally represent the medial and proximal alluvial slope (Koning, 2004, p. 103)."

Comment by JWH: In the Rancho Viejo study area (CCX and Injection Well sites), distal piedmont slopes form the primary depositional environments of Tesuque Fm—Lithosome A. *Main-body* and *lower* Tesuque deposits associated with these units correspond to the **Lithofacies Assemblages (LFAs) 5, 5a, & 5b**, and *informal Hydrostratigraphic Units (HSUs) MSF1 and LSF[1]* used herein (see Fig. 1 and Table 1; Hawley and Kernodle, 2000; Hawley and Cook, 2003).

Lithosome B (Not Present in Southern Española Basin)

Lithosome B units are associated with basin-floor fluvial depositional environments of the Tesuque Fm near the axis of an early-stage northern Española Basin (including the "old" Buckman well field and area to the north. These units "are characterized by siltstone, claystone [mudstones], and fine sandstone floodplain deposits interbedded with subordinate, relatively broad channel deposits of sandstone and conglomerate (Koning, 2004, p. 103)." In the northern and central parts of the basin, Cavazza (1986) and Koning note that gravel-clast composition is "heterolithic," and includes clasts derived from Tertiary volcanic, Paleozoic sedimentary, and Proterozoic granitic/metamorphic source terranes to the north and northeast (e.g. Peñasco embayment and southern San Luis Basin).

Lithosomes S and E (Koning, 2006)

Lithosome S

The basin-floor—distal piedmont-slope equivalent of Lithosome B In the Rancho Viejo study area is now designated **Lithosome S** (see Koning 2006 [below], Johnson et al. 2005); and most, if not all of these *main-body* Tesuque deposits are derived from an ancestral southern Santa Fe Range source area that was dominated by basement-granitic/metamorphic bedrock units, with relatively small areas of exposed Paleozoic sedimentary units and Oligocene volcanics.

Comment by JWH: In the Rancho Viejo study area, inferred depositional environments represented by Lithosome S include both fluvial-channels and broad floodplains located near the southern end of basin. *Main-body* Tesuque deposits associated with these environments correspond to the **Lithofacies Assemblages (LFAs) 2, 3, & 9**, and **informal Hydrostratigraphic Units (HSUs) MSF2 and LSF[2]** used herein (see Fig. 1 and Table 1; Hawley and Kernodle, 2000; Hawley and Cook, 2003).

Lithosome E

A relatively thin, volcanic-derived and volcanoclastic **basal-Tesuque** unit is now designated **Lithosome E** by Koning (2006) and Johnson and others (2004). It is generally correlative with the Tesuque-Bishops Lodge Mbr of Spiegel and Baldwin (1963), and it is transitional westward with the uppermost parts of the Espinazo Fm (volcanics) and Cieneguilla Limburgite (basanite) of Disbrow and Stoll (1957) and Sun and Baldwin (1958).

Lithosome AS Complex (My informal unit that may be useful for detailed correlation of facies units in the Rancho Viejo [CDX and OB-A pilot hole] area—not used in this report)

Stacked units associated with shifting depositional environments in inferred areas of piedmont-toeslope/basin-floor transition. In the Rancho Viejo-CCX-Well study area, the **Lithosome AS Complex** includes *main-body* Tesuque deposits corresponding to the **Lithofacies Assemblages (LFAs) 3,5 & 5,3**, and **informal Hydrostratigraphic Units (HSUs) MSF and LSF** used herein (see Fig. 1 and Table 1; Hawley and Kernodle, 2000; Hawley and Cook, 2003).

Selections from E-mail communications from Dan J. Koning on February 27 and March 26, 2006 on: Lithosomes in the Southern Española Basin.

February 26, 12:52 PM:

Lithosome B is associated with a south-sloping basin floor facies and a provenance of the Peñasco embayment and San Luis basin. It has a composition of mixed Paleozoic + felsic-intermediate volcanic + granitic detritus (the latter increases to the south). I have not found lithosome B anywhere near

Santa Fe; the furthest south I see it is in the old Buckman well field north of the new city wells.

Lithosome S is [primarily] arkosic pebbly sand and sand, but there [are] more than trace amounts of yellowish Paleozoic sandstone + limestone grains + Proterozoic quartzite grains (including a dark, cherty grain). Also, generally there are intercalated mudstone beds in lithosome S, although we have found places, such as at the fairgrounds, where such mudstone beds are relatively minor. Lithosome S was deposited by an ancestral Santa Fe River on a piedmont slope; and back in Miocene-time, the upper reaches of this river extended eastwards across the Picuris-Pecos fault. In this area, piedmont-slope sediment of lithosome A, [which] lacks Paleozoic sedimentary + Proterozoic quartzite detritus, seems to be of relatively narrow extent south of lithosome S. It seems that granitic hills south of the ancestral Santa Fe River were not sufficiently [high] or of wide extent as to produce much lithosome A sediment south of the river on the piedmont slope.

Recently, I have designated Lithosome E for Oligocene-Miocene volcanoclastic sediment derived from erosion of paleo-highlands that ringed the south, southwestern, and western part of the Santa Fe embayment. The recent Jail well went through this lithosome at ~550-1214 ft, and I see it in many Nuclear Dynamic wells west of the Rancho Viejo well(s). Lithosome E consists of sand, muddy sand, and muddy pebbly sand; and the composition of the volcanics is mixed basalt + latite (because of erosion of both the Cieneguilla basanite and the Espinazo Fm). Perhaps what you called Espinazo Fm is really lithosome E. The basalts usually are a dark gray to black color and olivine is usually seen; the color of the latite is generally a lighter gray.

March 27, 8:13 AM:

I looked at the boxed cuttings from this well late last week. I also stopped by the ABQ office to look at the 1710-1800 ft interval with Sean's petrographic scope. I changed my interpretation of this interval: After looking at these cuttings in detail, I would call it Bishop's Lodge Member of Tesuque Fm (equivalent to upper Espinazo Fm). The cuttings are more tuffaceous than the lithosome E, are composed predominately of dacite clasts (only one clast/grain that might be basalt), are relatively consolidated, and the upper contact seems more sharp than gradational. Usually, [the] upper lithosome E has muddy beds near its gradational top, but that is not the case here. Do the down-hole geophysical logs show a sharp contact or muddy interbeds in the 1710-1800 ft interval? Also, do the gamma ray curves indicate any ash beds in the upper or middle part of the hole?

. . . . Having an Espinazo Fm-Bishop's Lodge Mbr interpretation for 1710-1800 ft interval is going to require that I change my cross-section again! I'll forward you a copy when I'm done with the revision.

Thanks a lot for letting me look at the samples!

APPENDIX C

INJECTION AND OBSERVATION WELL TEST SUMMARIES

RANCHO VIEJO

WATER PLAN

TABLE G1. OBSERVATION WELL A TEST SUMMARY (SINGLE-DRILL HOLE, MULTIPLE-SCREEN SETTINGS)

Tested Zone	Test Date	Screen Setting of Tested Interval (ft below ground)	Pre-Test Water Level ⁴ (ft below ground)	Tested Rate (gpm)	Test Duration (hr)	Packer Depth (ft below ground)	Test Zone Drawdown (ft)	Observation Zone Drawdown (ft)			Local Test Zone Properties ⁸			Recovery Period (hours)	Late-Time Recovery Transmissivity ⁹ (ft ² /d)
								Above Packer ⁵	Intermediate Piezometer ⁶	Deep Piezometer ⁷	Transmissivity (ft ² /d)	Test Zone Thickness (Screen Length) (ft)	Hydraulic Conductivity (ft/d)		
Deep ¹	3/1/2006	1500 to 1580	280.95	28	3.8	1391	137.4	1.26	--	--	48	80	0.6	19	30
Intermediate ²	3/6/2006	1020 to 1300	290.11	43	3.3	706	18.3	0.36	--	7.9	126	180	0.7	10	40
Shallow ³	3/8/2006	580 to 620	284.49	30	4.1	None	27.7	--	17.0	4.3	150	40	3.8	113	8

¹Deep zone isolated with inflatable wellbore packer set at 1391 feet below ground.

²Before intermediate zone test, deep zone screen backfilled with gravel and sealed with 20-foot thick bentonite plug. Intermediate zone isolated with inflatable wellbore packer set at 706 feet below ground.

³Before shallow zone test, intermediate zone screen backfilled with gravel and sealed with 20-foot thick bentonite plug.

⁴Pre-test water levels were recovering from previous tests and from wellbore sealing operations. The pre-test and post-test hydraulic head in the deep zone is higher than intermediate and shallow zones. The pre-test head in the shallow zone is higher than the intermediate zone head, but recovers to about one foot lower. Final gradient is upward from deep to shallow zone.

⁵Change in water level above packer during deep and intermediate zone tests is interpreted as leakage around packer. No leakage through annular bentonite seals is indicated.

⁶Response at intermediate piezometer during shallow zone test may be from movement and bypass of bentonite plug inside casing.

⁷Response at deep piezometer during intermediate and shallow zone tests may be from movement and bypass of bentonite plugs inside casing.

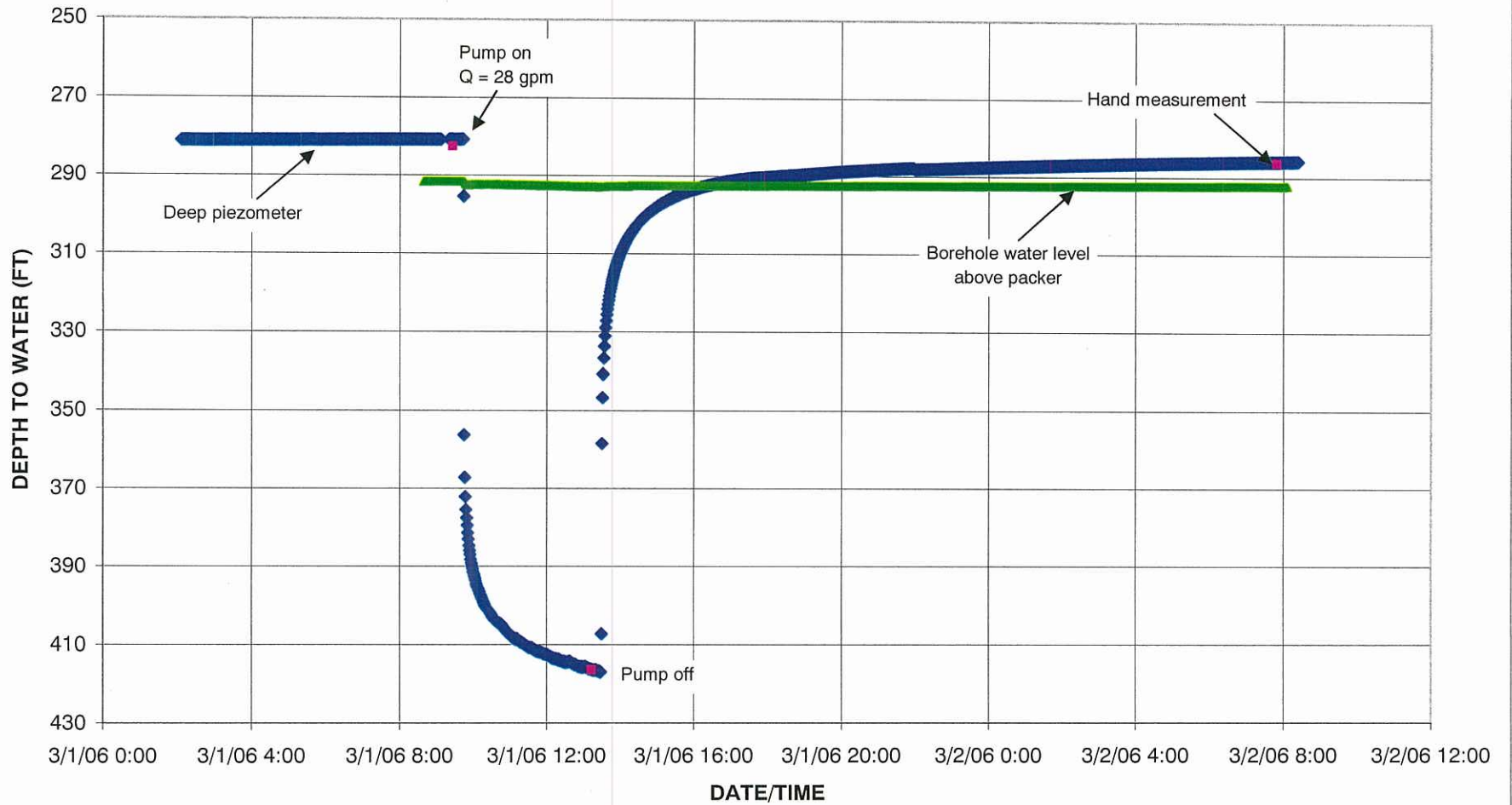
⁸Local test zones in screened sands are tested radii of influence, ranging 400 to 800 feet.

⁹Barrier boundaries of fine-grained sediment enclosing channel sands are indicated by late-time recovery transmissivity at intermediate and shallow zones.

Conclusions: Hydraulic conductivity of screened sands decreases with depth from several feet per day at 600 feet to several tenths of a foot per day at 1500 feet. Fine-grained sediments enclosing channel sands are one-half to one-tenth of the hydraulic conductivity of the sands. Vertical hydraulic gradient is upward.

WATER PLAN

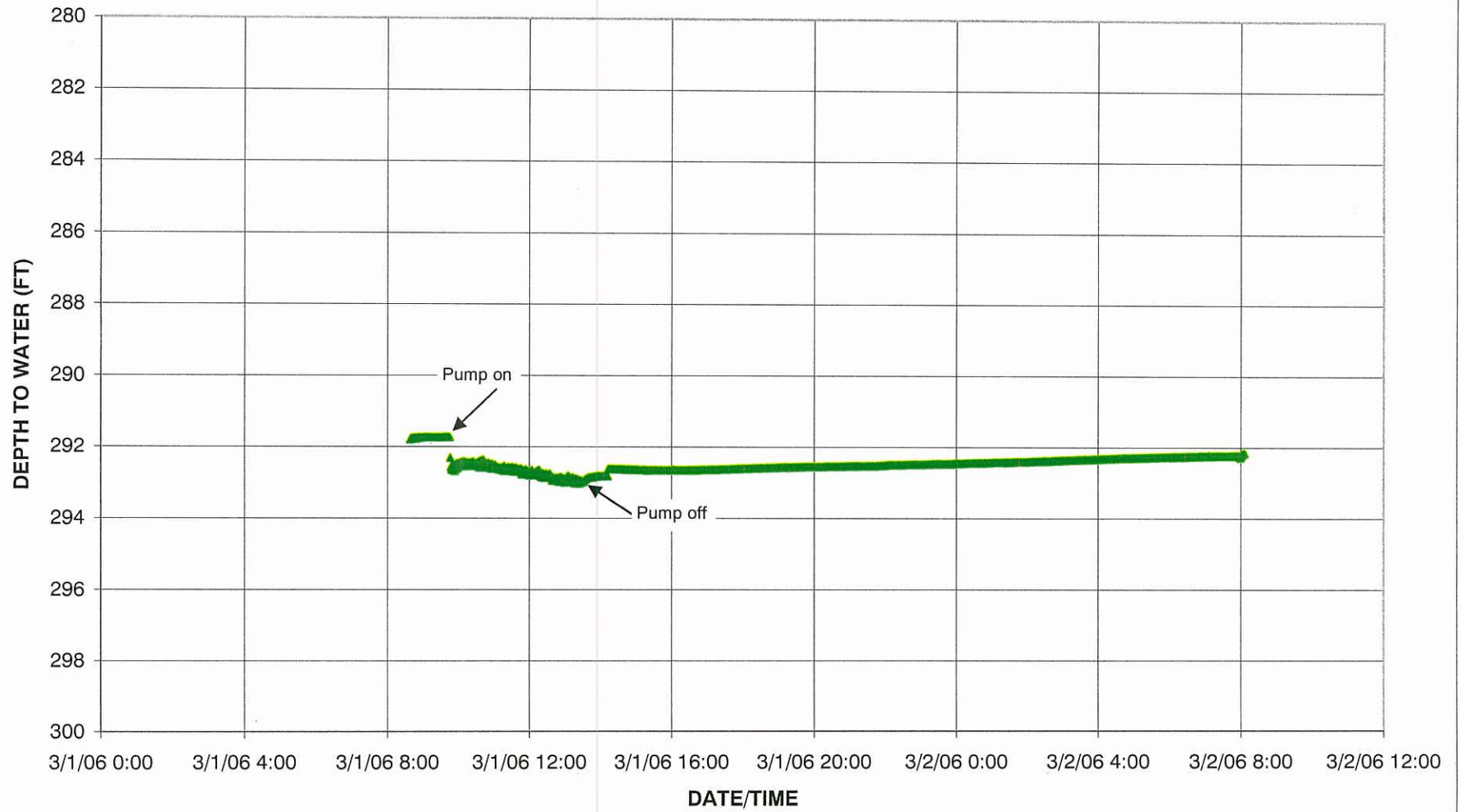
FIGURE G1
CCD-OWA DEEP ZONE TEST
TEST HYDROGRAPH



RANCHO VIEJO

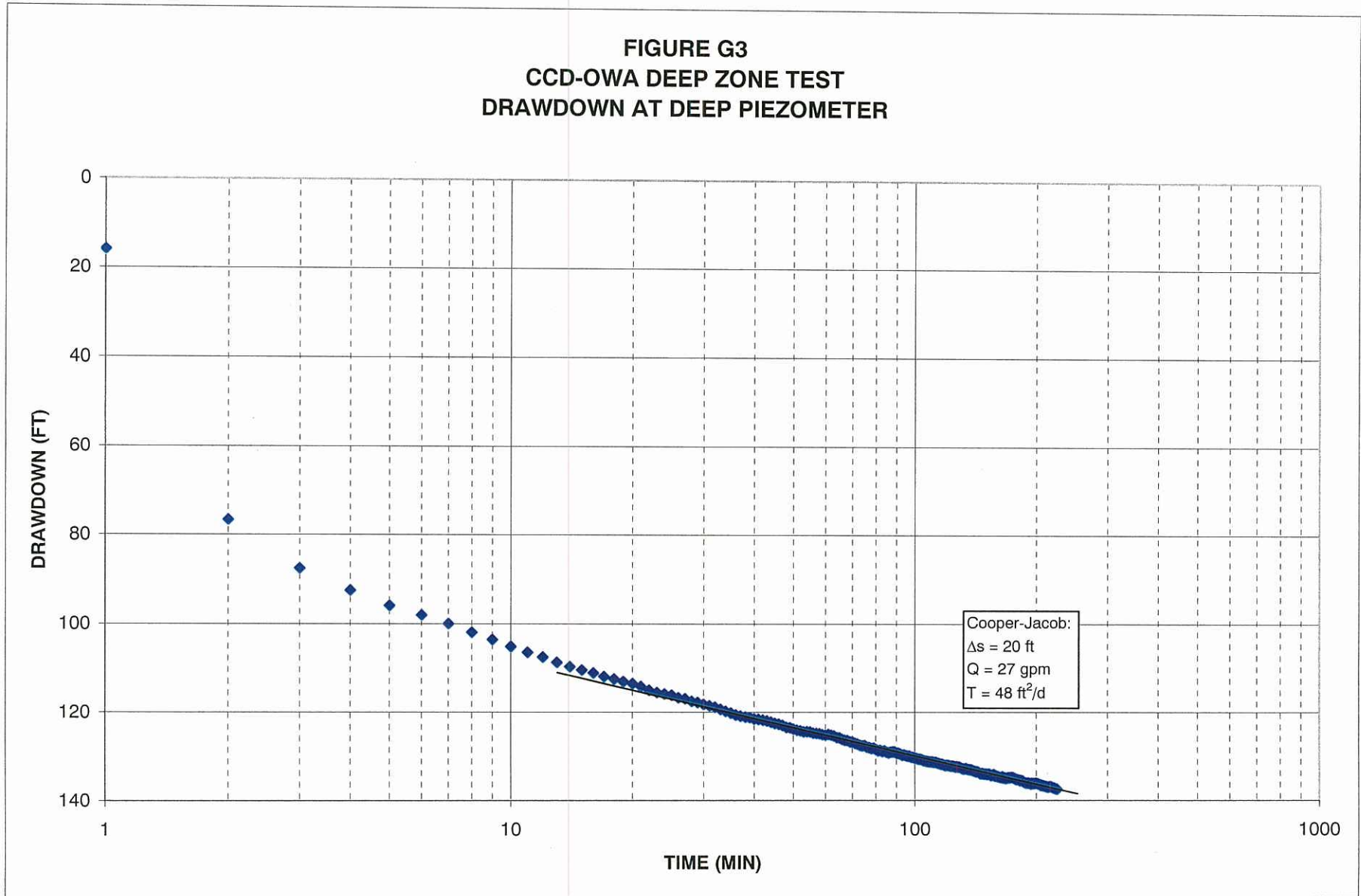
WATER PLAN

FIGURE G2
CCD-OWA DEEP ZONE TEST
RESPONSE IN WELLBORE ABOVE PACKER



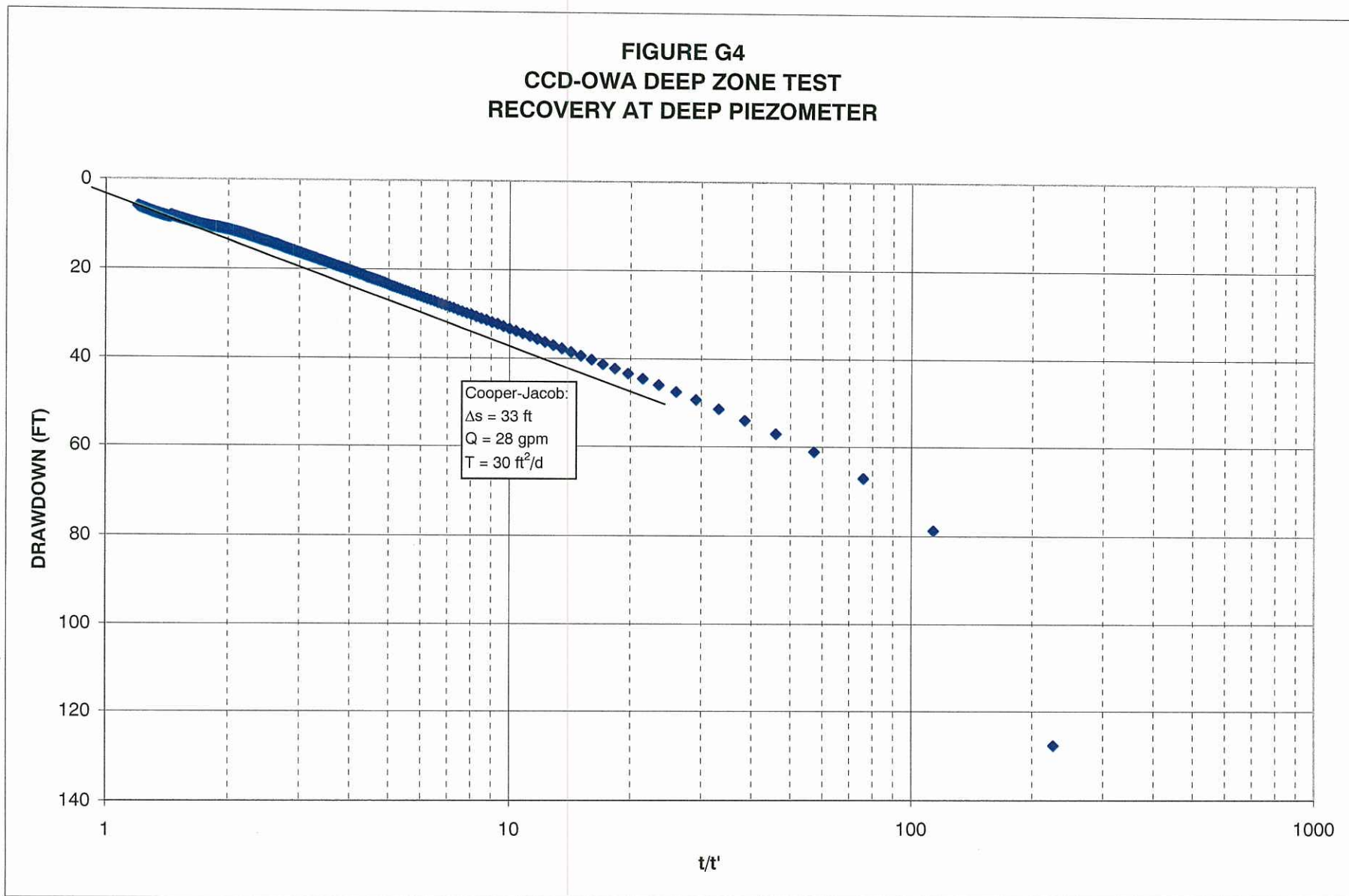
WATER PLAN

FIGURE G3
CCD-OWA DEEP ZONE TEST
DRAWDOWN AT DEEP PIEZOMETER



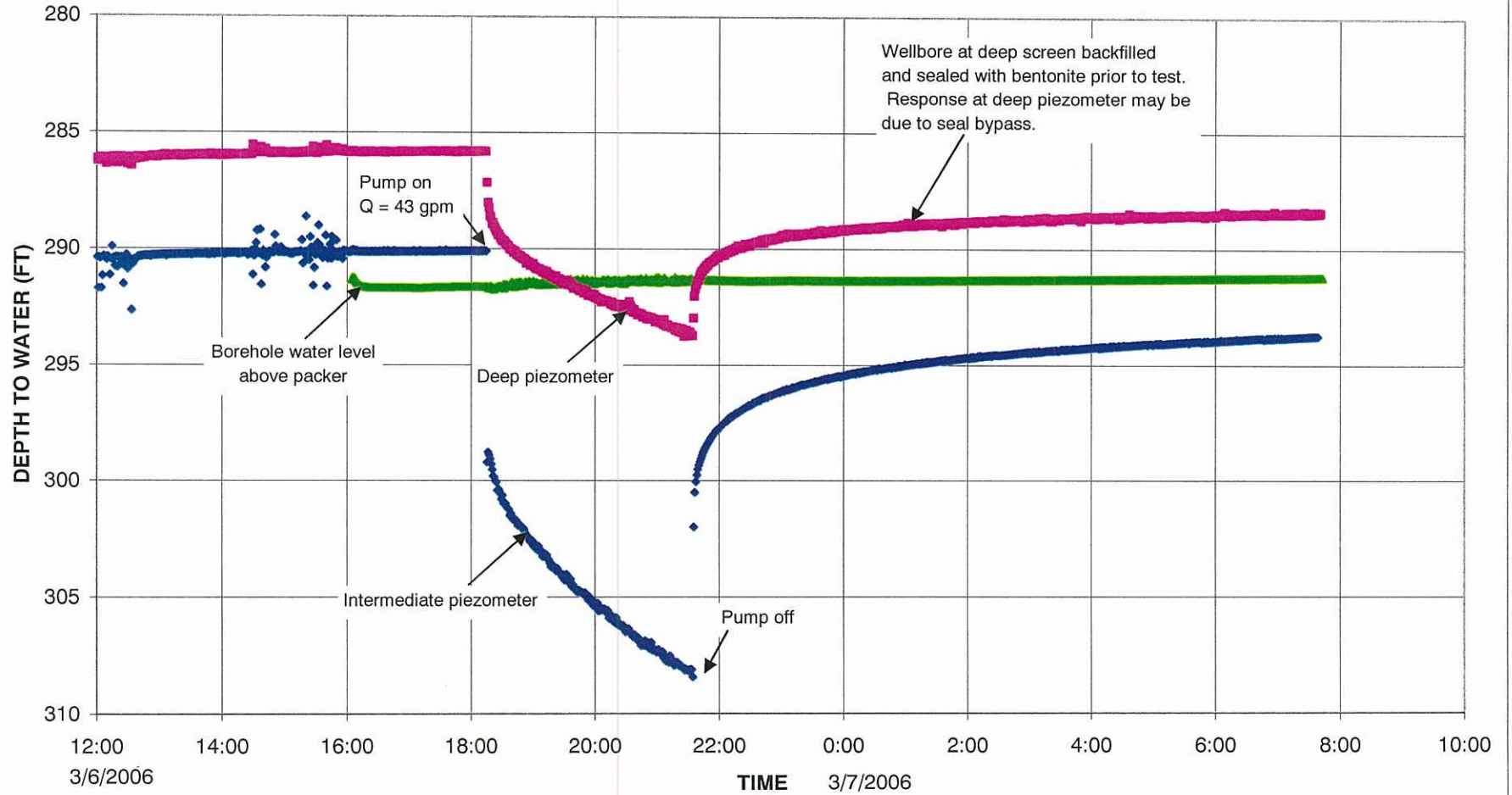
WATER PLAN

FIGURE G4
CCD-OWA DEEP ZONE TEST
RECOVERY AT DEEP PIEZOMETER



WATER PLAN

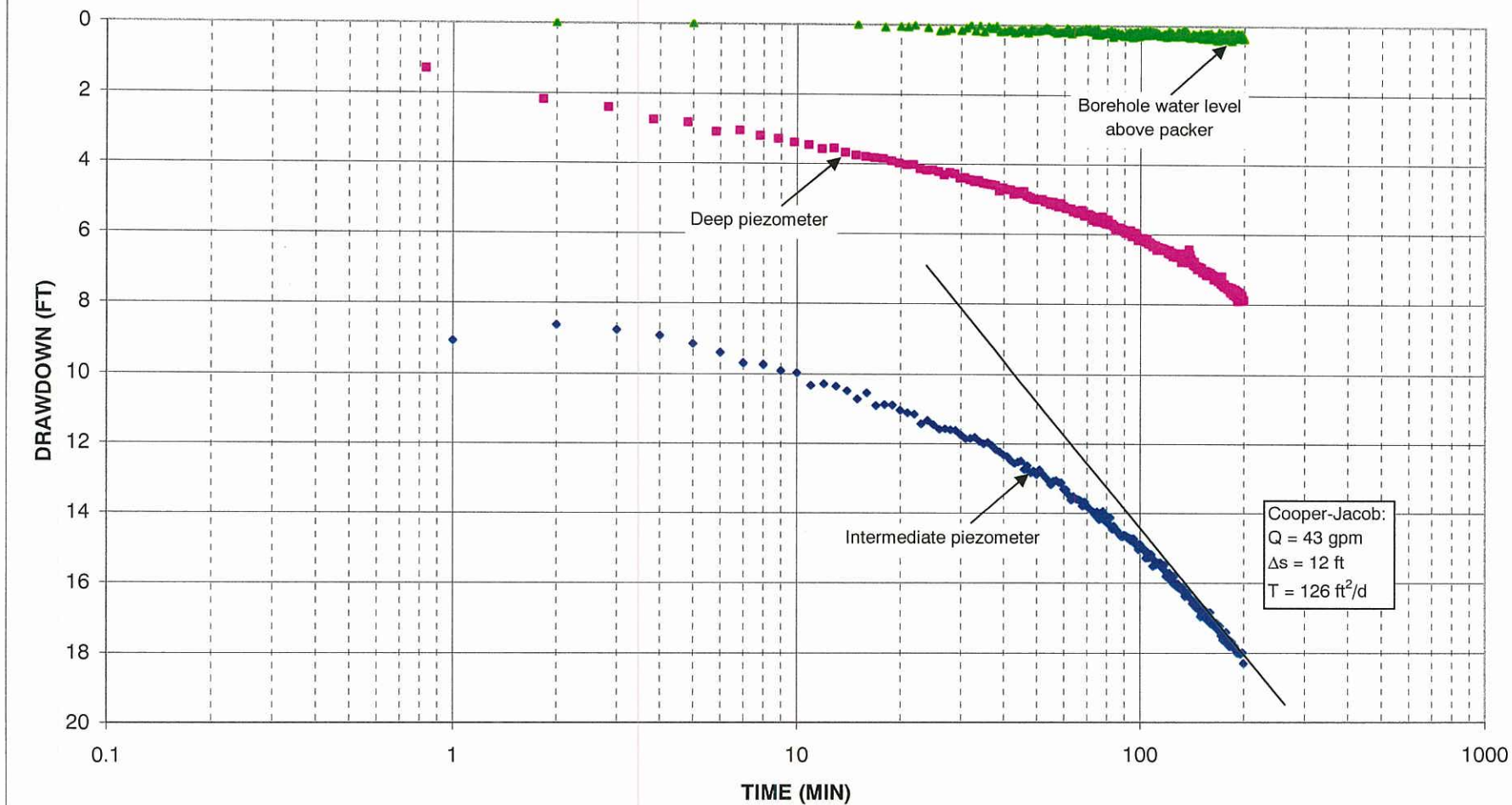
FIGURE G5
CCD-OWA INTERMEDIATE ZONE TEST
TEST HYDROGRAPH



RANCHO VIEJO

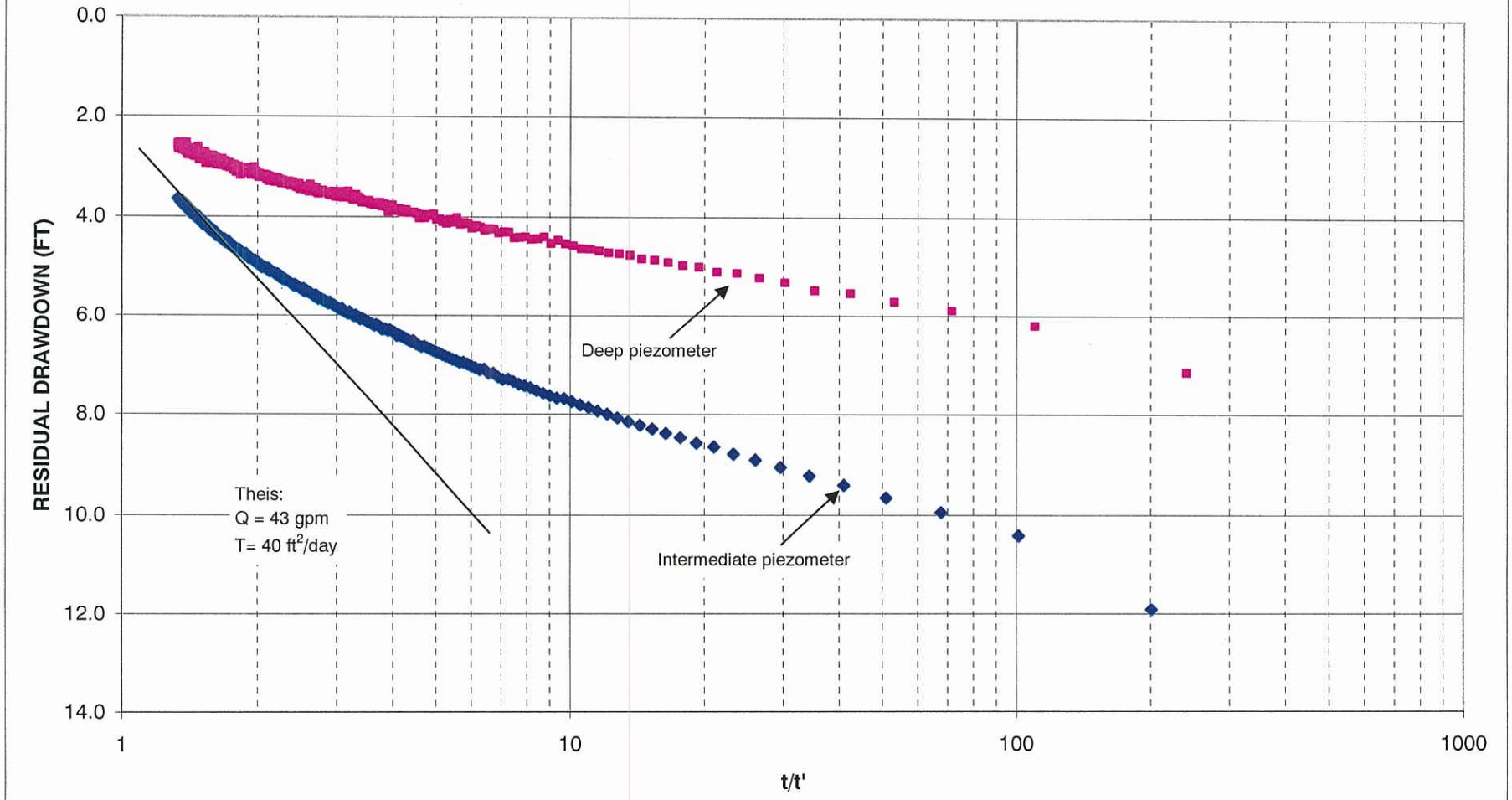
WATER PLAN

FIGURE G6
CCD-OWA INTERMEDIATE ZONE TEST
DRAWDOWN IN DEEP AND INTERMEDIATE PIEZOMETERS AND ABOVE PACKER



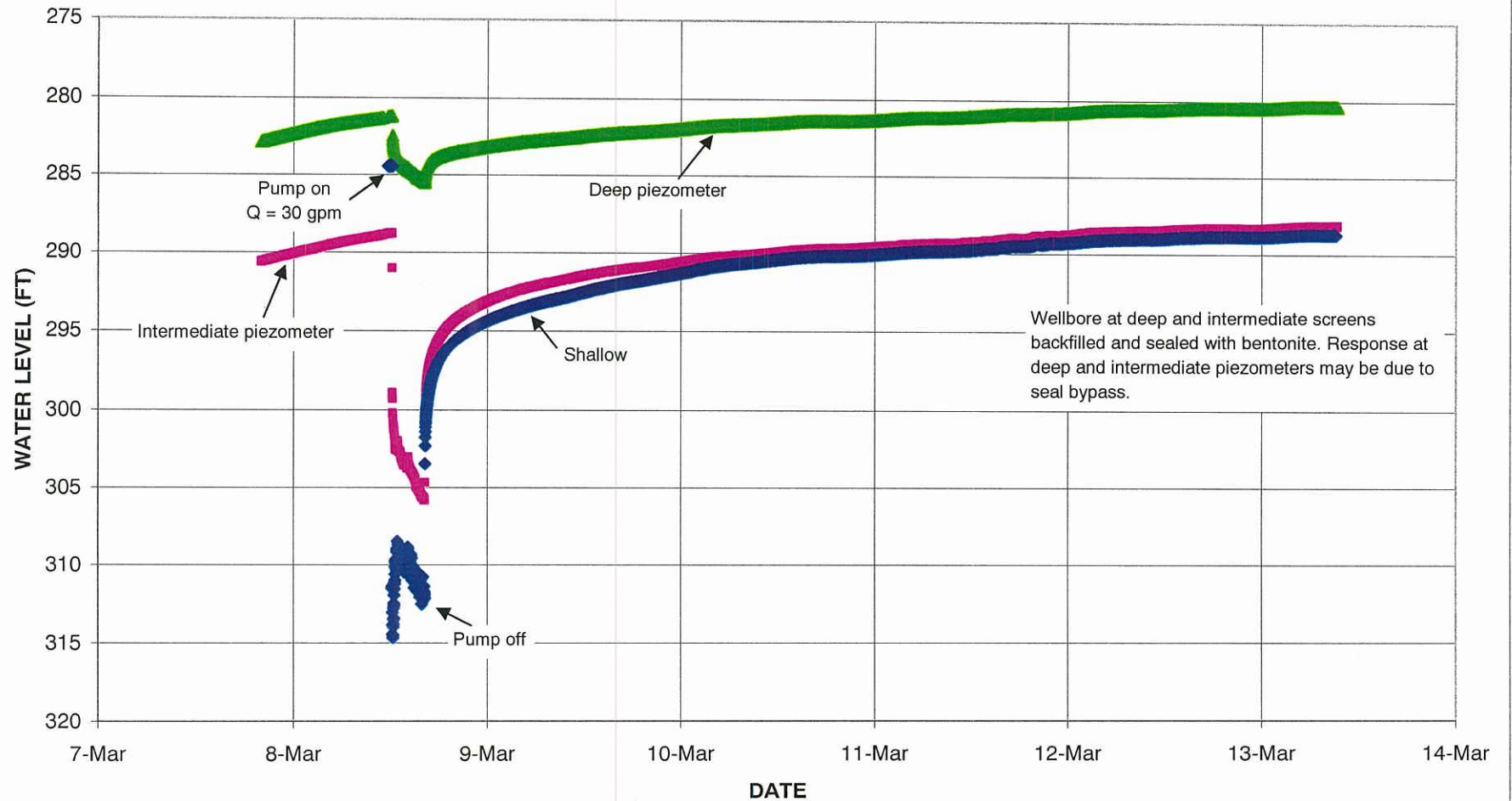
WATER PLAN

FIGURE G7
CCD-OWA INTERMEDIATE ZONE TEST
RECOVERY



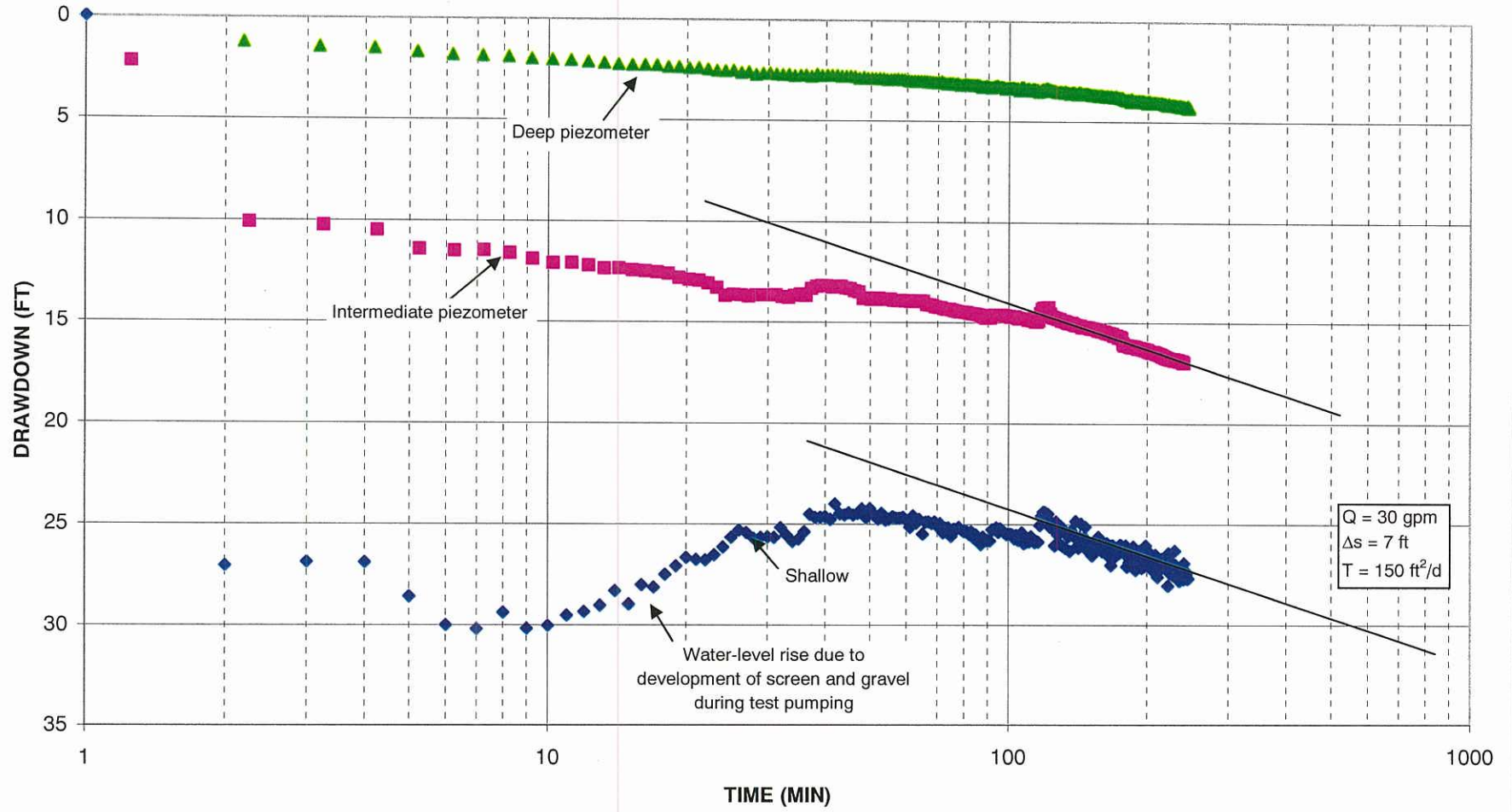
WATER PLAN

FIGURE G8
CCD-OWA SHALLOW ZONE TEST
TEST HYDROGRAPH



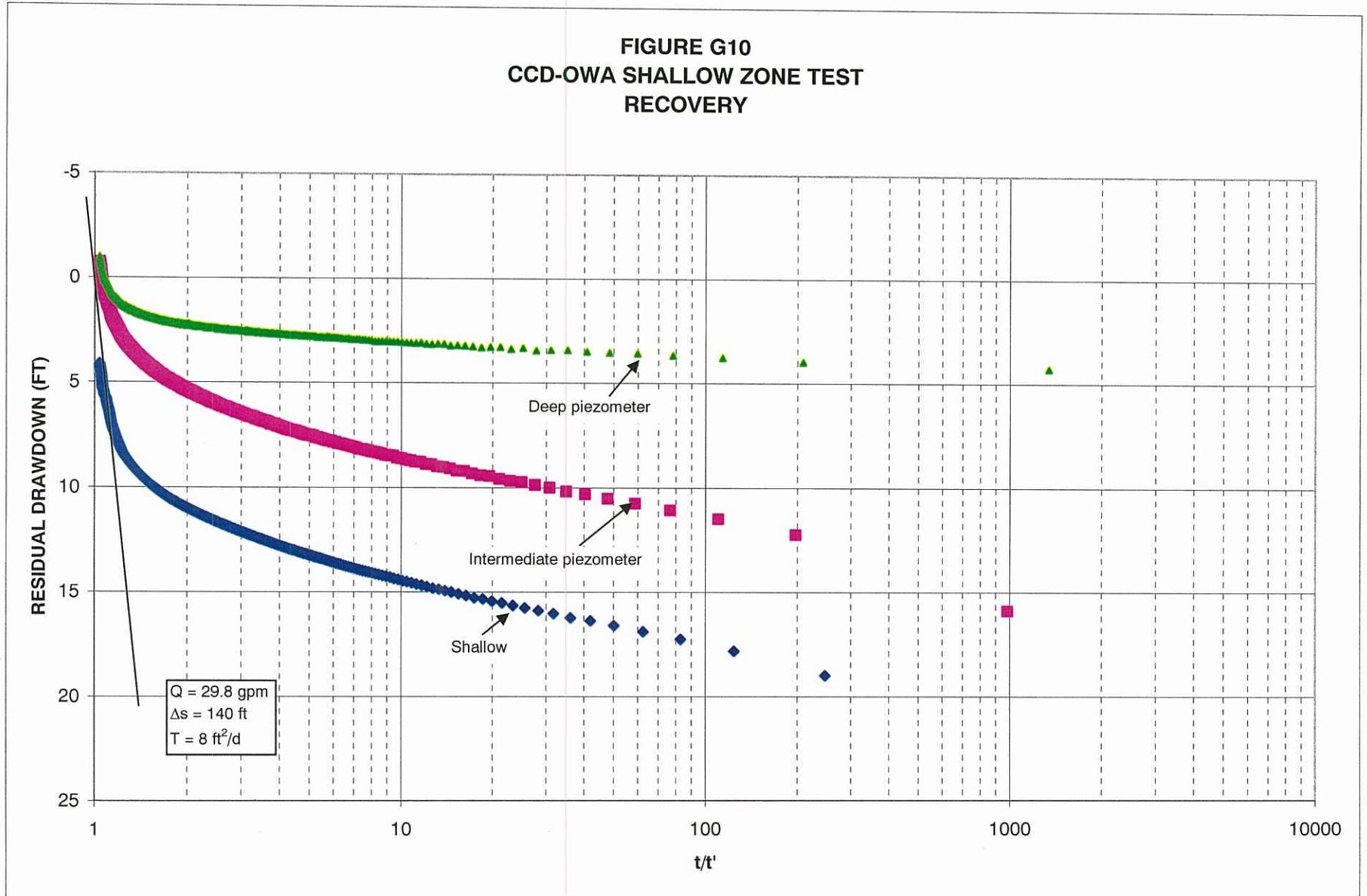
WATER PLAN

FIGURE G9
CCD-OWA SHALLOW ZONE TEST
DRAWDOWN AT DEEP AND INTERMEDIATE PIEZOMETERS AND AT SHALLOW 5-INCH SCREEN



WATER PLAN

FIGURE G10
CCD-OWA SHALLOW ZONE TEST
RECOVERY



RANCHO VIEJO

WATER PLAN

TABLE F1. SUMMARY OF CCD-11 PUMPING TEST

Well	Purpose	Distance from Test Well (ft)	Pre-Test Water Level (ft below ground)	End of Test Drawdown (ft)	Tested Parameters ^{2,3}			
					T (ft ² /d)	S	n	Late-time Recovery T (ft ² /d)
Injection Well	Test Well ¹	--	297.2	175.7	1100	2.5x10 ⁻⁵	1.3	73
OWA Shallow	Observation	110	297.7	92.2	--	--	--	70
OWA Intermediate	Observation	110	297.5	147.1	1100	0.00013	1.1	70
OWA Deep	Observation	110	294.9	78.0	--	--	--	70
OWB	Observation	482	302.0	22.2 ⁵	1100	0.003	1.3	155
OWC	Observation	1985	260.3	3.5 ⁵	1100	0.005	1.3	390
CCD-P1	Observation	5400	250.1	0.5	100	0.0015	2.6	--

¹Tested at 200 gpm for 7 days from May 15-27, 2006.

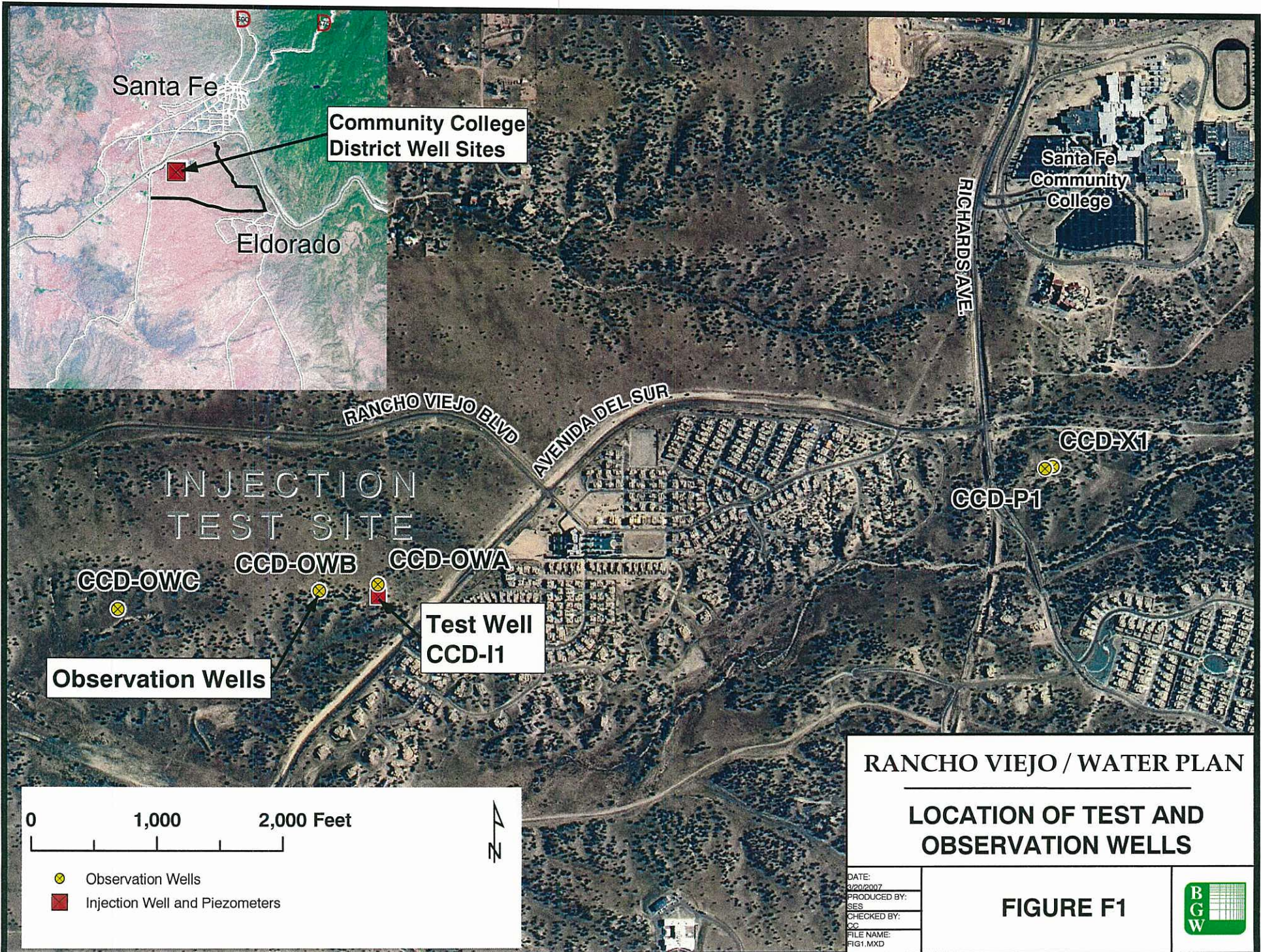
²Drawdown analyzed with methods of Walker, D.D., and R.M. Roberts, 2003, Flow dimensions corresponding to hydrogeologic conditions in Water Resources Research, Vol. 39, No. 12, p. 1329.

³Recovery analyzed with methods of Theis C.V., 1935, The Relation Between the Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Ground-Water Storage: American Geophysical Union, Volume 16, pp. 519-524.

⁴Hydraulic conductivity (k) of test zone = T/screen length = 1100/720 = 1.5 ft/d.

⁵Corrected for background water level rise.

Conclusion: Tested aquifer consists of channel sands (k = 1.5 ft/d) enclosed by fine-grained over bank deposits with less permeability (based on recovery). Flow dimension of enclosing boundary is n = 1.1 to 1.3 (approximating a linear channel). Response at CCD-P1 one mile distant was observed 35 days after test start. Matching parameters T = 100 ft²/d and n = 2.3 is compatible with a boundary between the test and observation wells and induced leakage at late time over a distance of 5,400 feet.



Santa Fe

Community College District Well Sites

Eldorado

Santa Fe Community College

RICHARDS AVE

RANCHO VIEJO BLVD
AVENIDA DEL SUR

INJECTION TEST SITE

CCD-X1

CCD-P1

CCD-OWC

CCD-OWB

CCD-OWA

Test Well CCD-I1

Observation Wells

RANCHO VIEJO / WATER PLAN

LOCATION OF TEST AND OBSERVATION WELLS

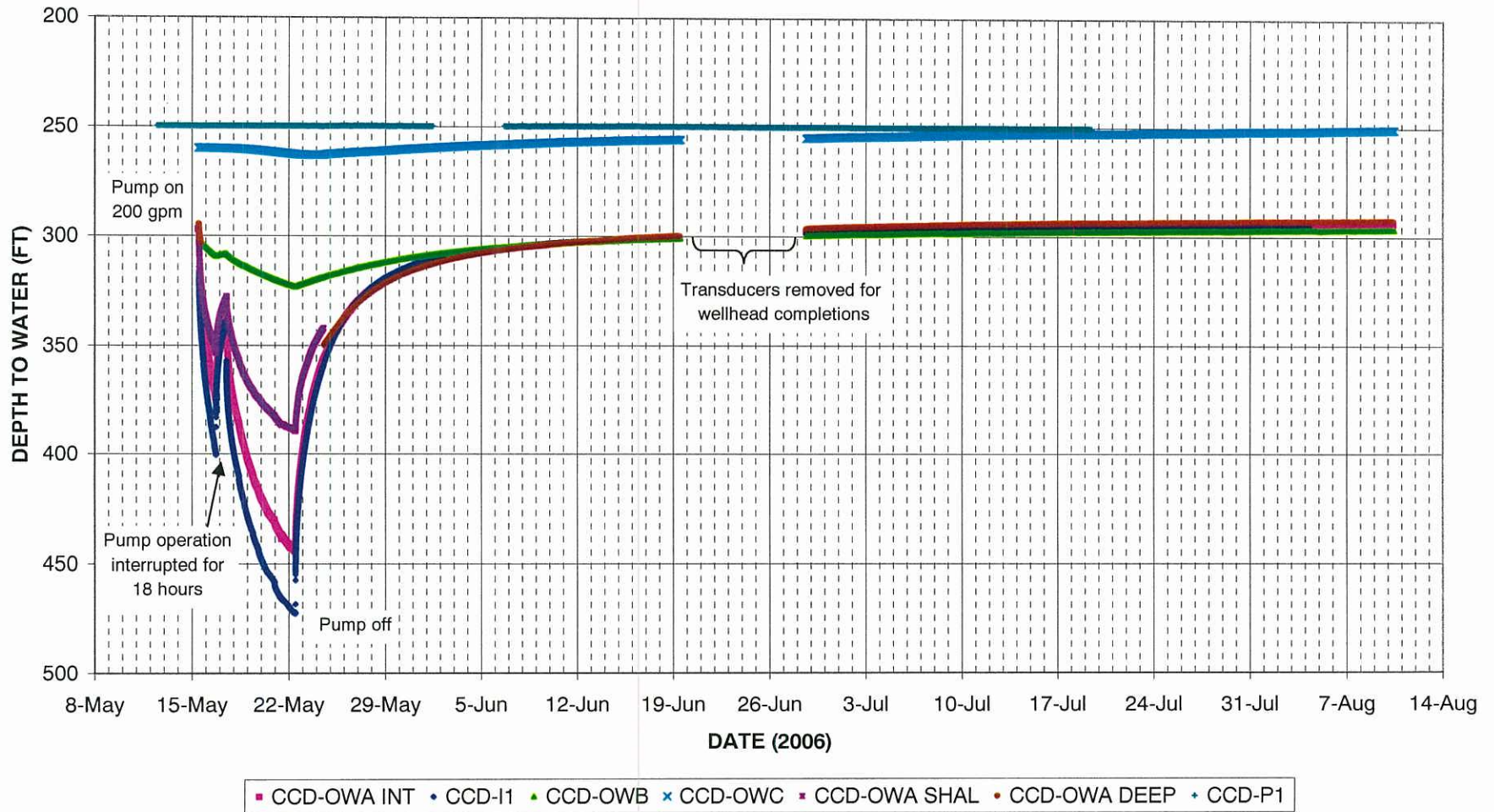
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FIG1.MXD

FIGURE F1



WATER PLAN

FIGURE F2
INJECTION WELL SEVEN-DAY PUMPING TEST
TEST AND OBSERVATION WELL HYDROGRAPHS



RANCHO VIEJO

WATER PLAN

FIGURE F3
INJECTION WELL SEVEN-DAY PUMPING TEST
DISTANCE-DRAWDOWN AT END OF TEST

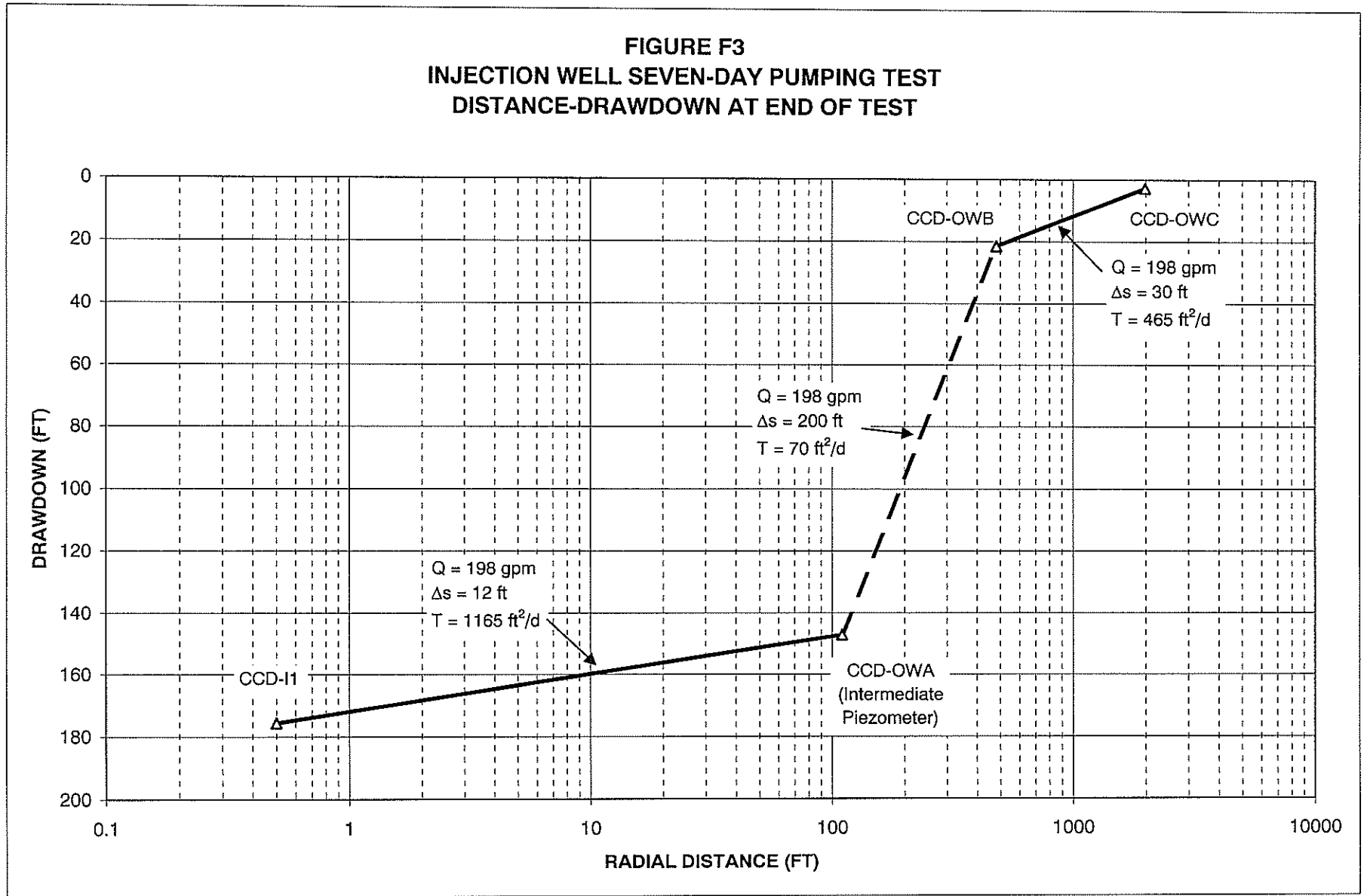


FIGURE F4
INJECTION WELL SEVEN-DAY PUMPING TEST
TEST WELL DRAWDOWN

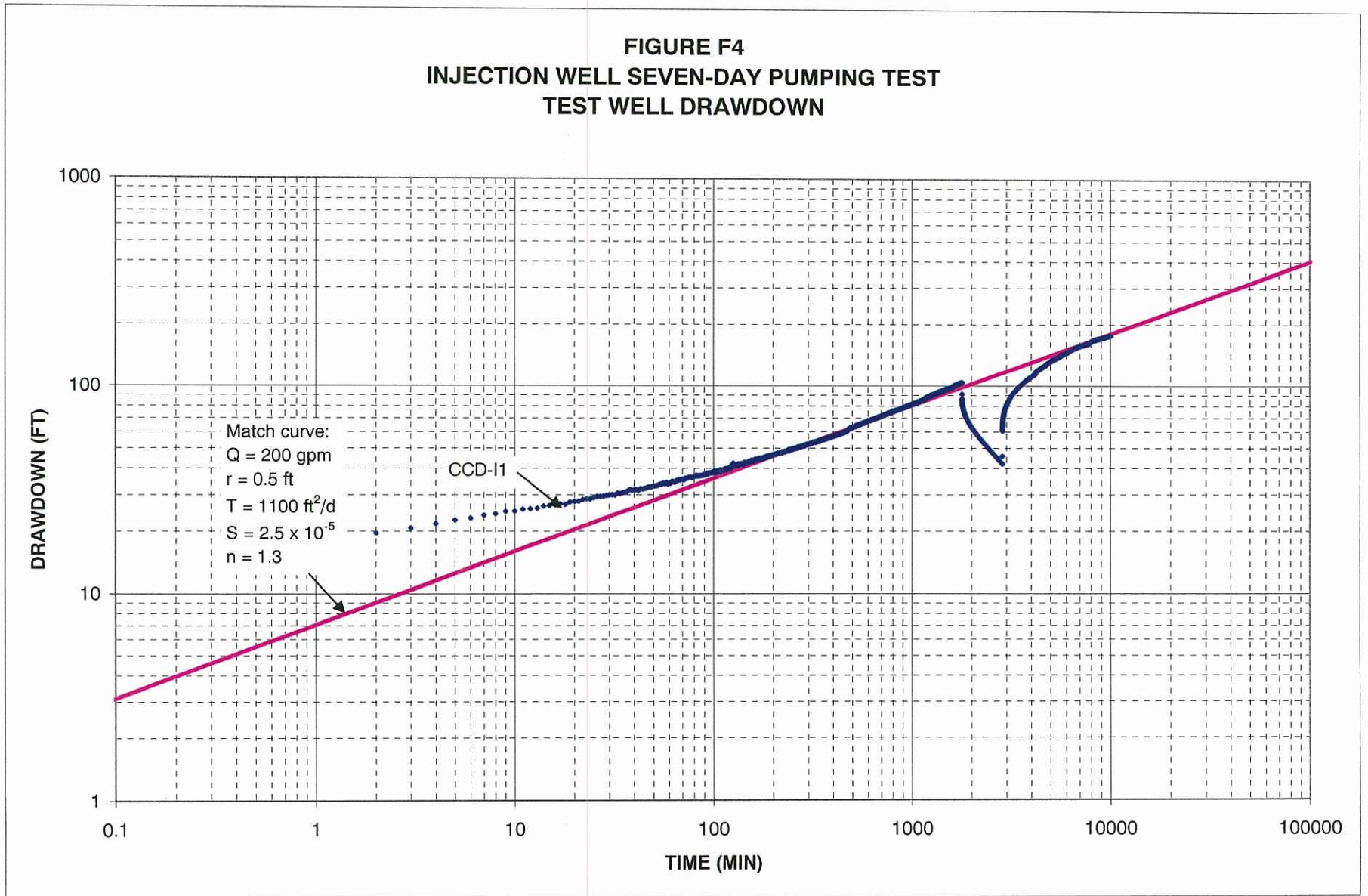
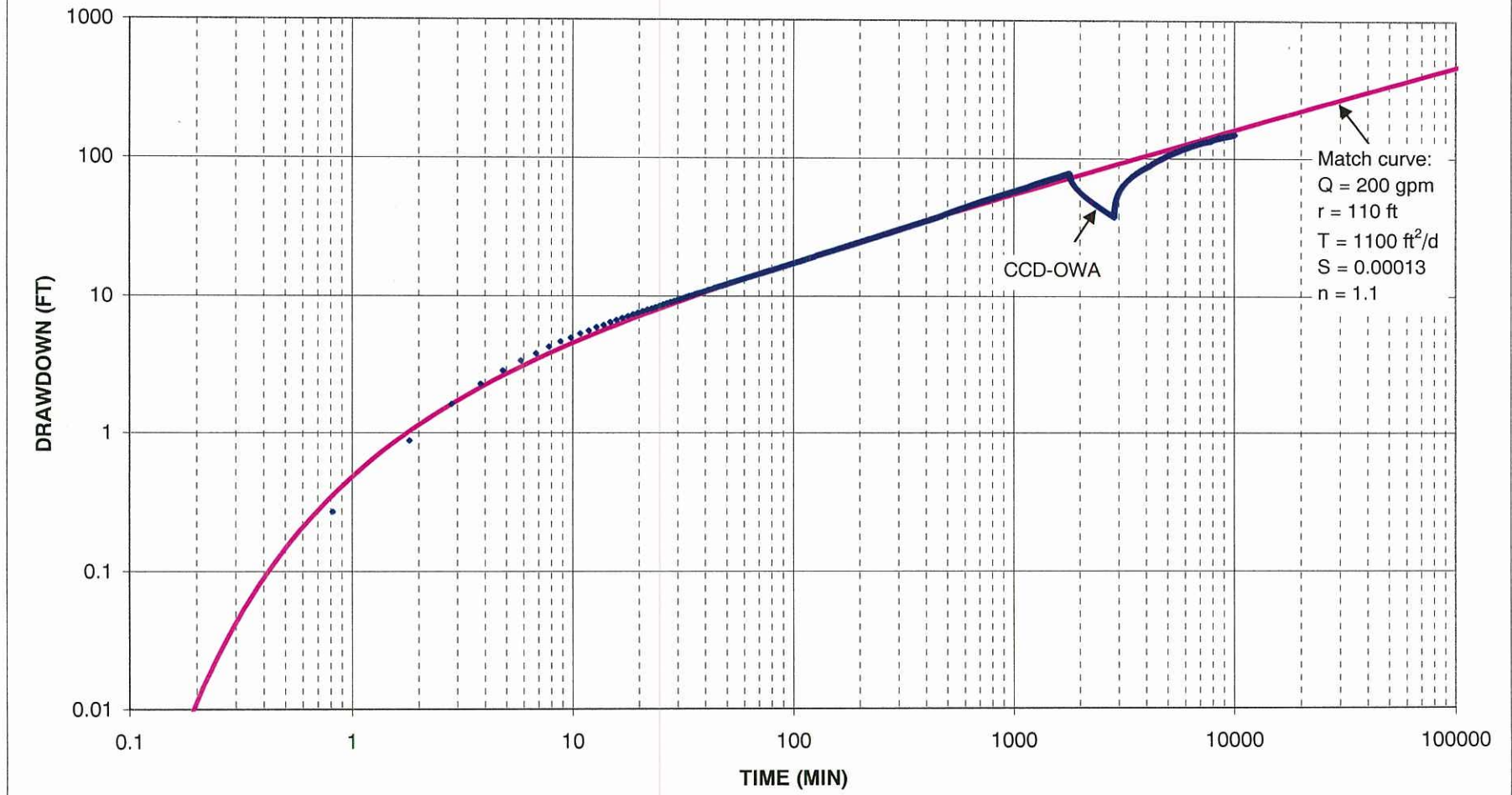
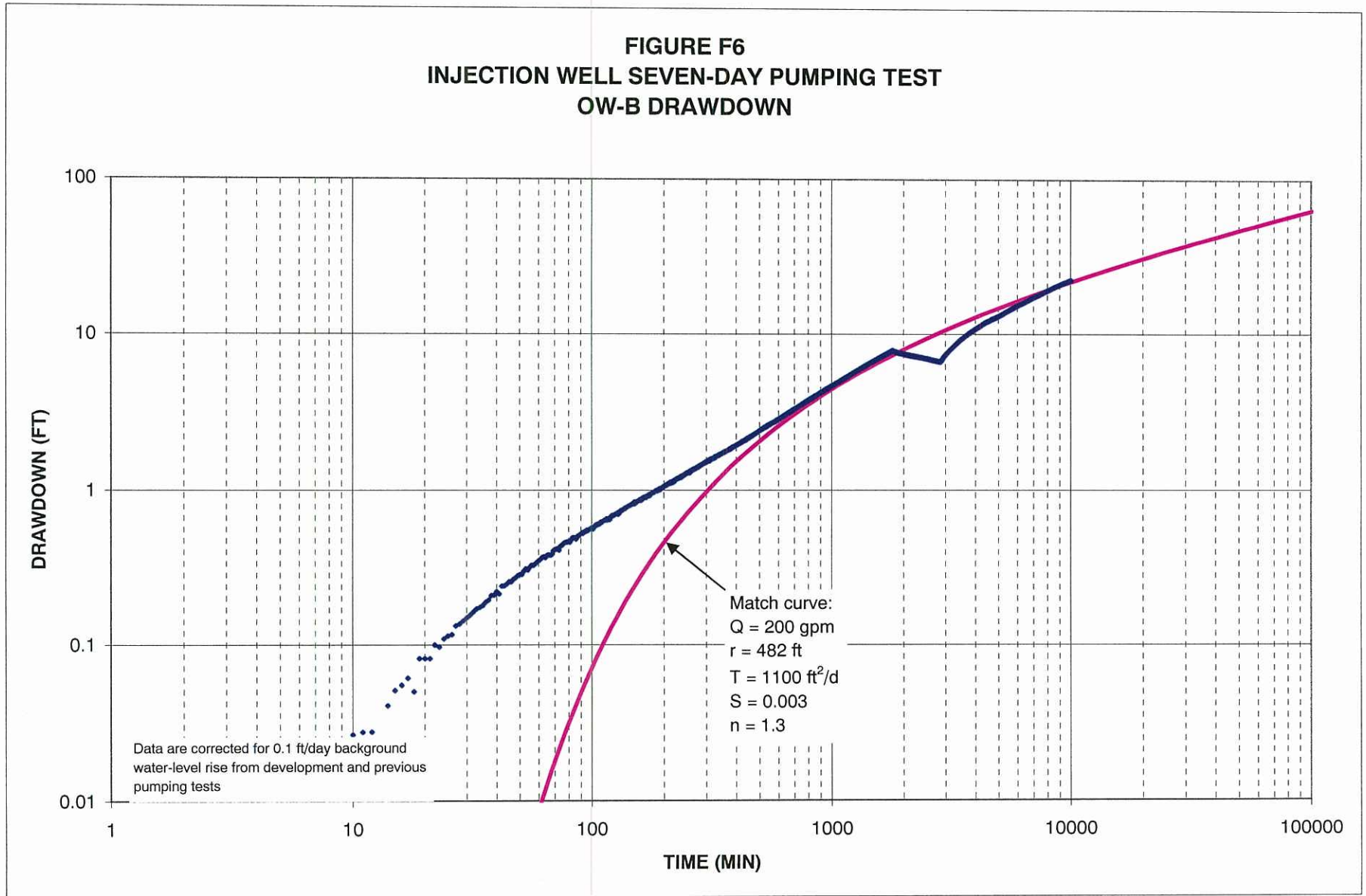


FIGURE F5
INJECTION WELL SEVEN-DAY PUMPING TEST
OW-A INTERMEDIATE PIEZOMETER DRAWDOWN



WATER PLAN

FIGURE F6
INJECTION WELL SEVEN-DAY PUMPING TEST
OW-B DRAWDOWN



WATER PLAN

FIGURE F7
INJECTION WELL SEVEN-DAY PUMPING TEST
OW-C DRAWDOWN

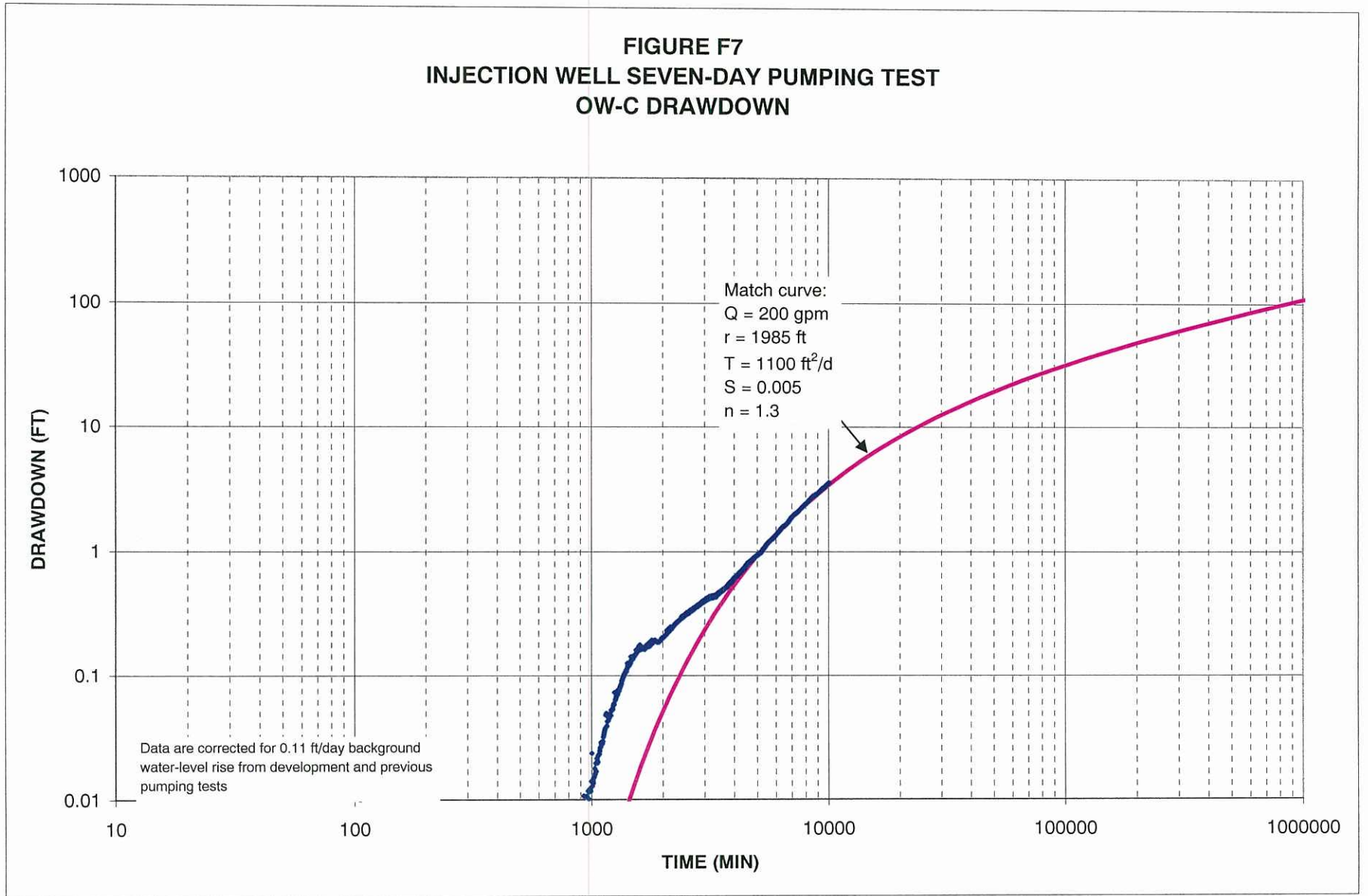


FIGURE F8
INJECTION WELL SEVEN-DAY PUMPING TEST
CCD-P1 DRAWDOWN

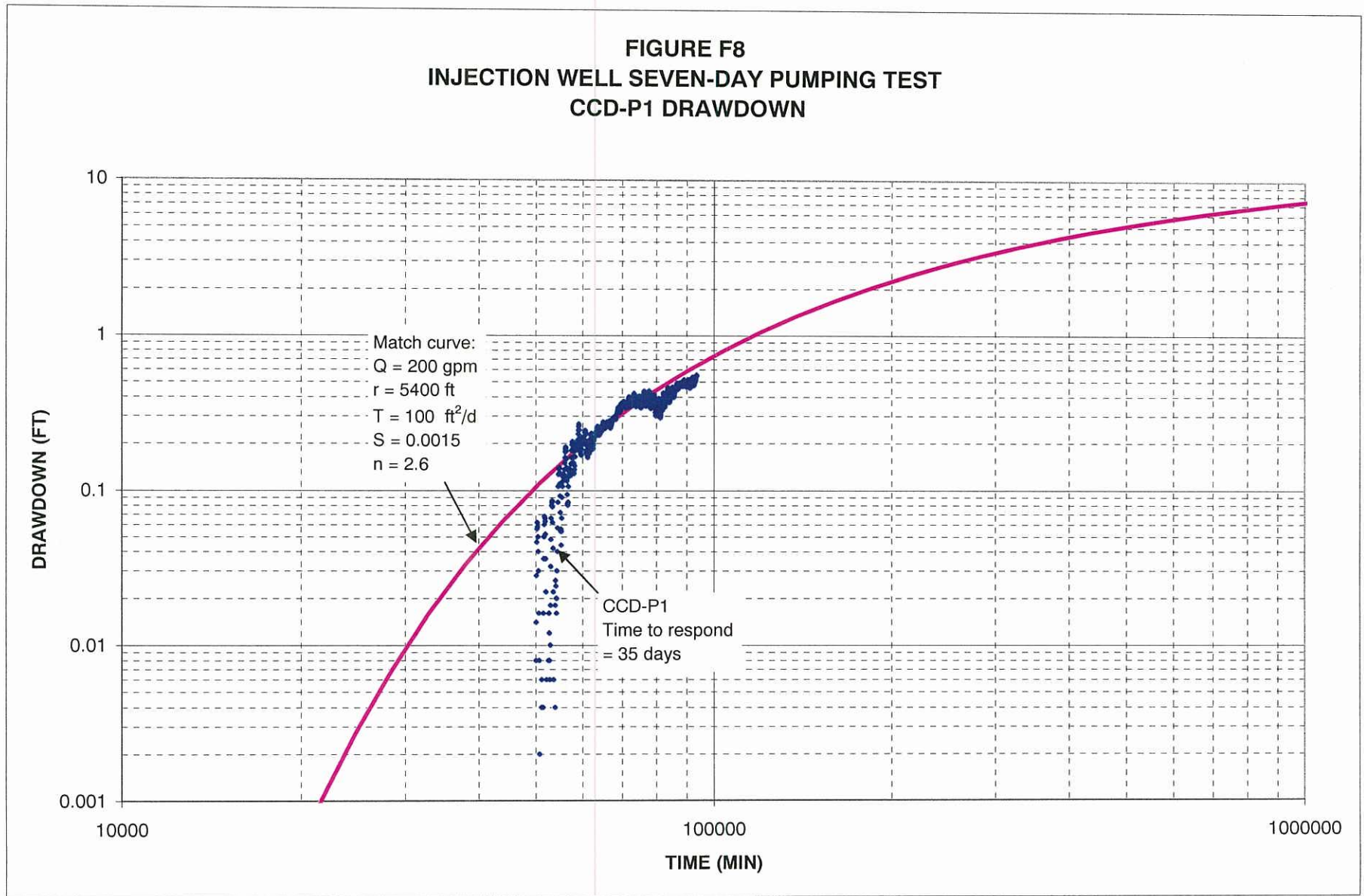


FIGURE F9
INJECTION WELL SEVEN-DAY PUMPING TEST
TEST WELL RECOVERY

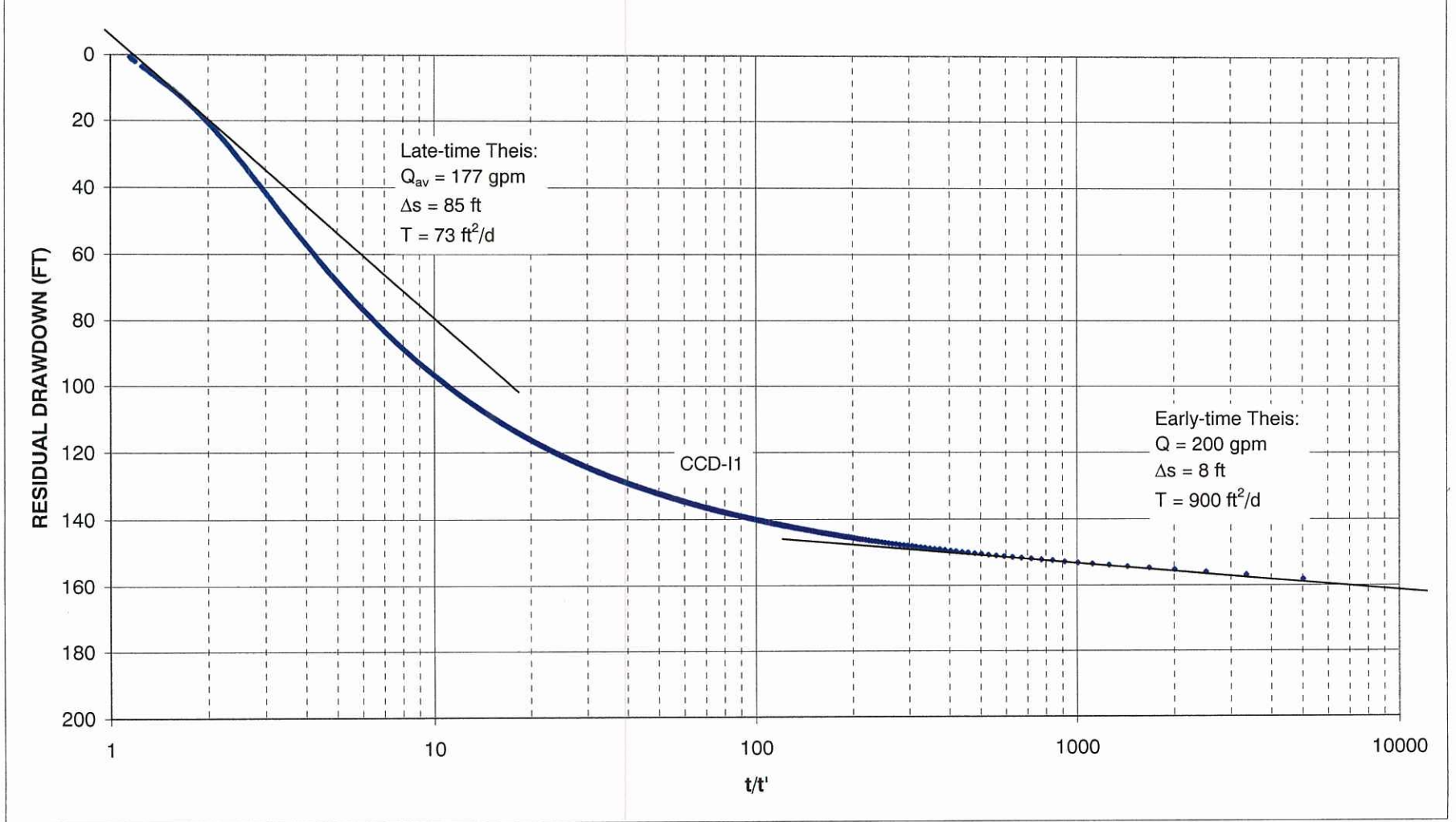


FIGURE F10
INJECTION WELL SEVEN-DAY PUMPING TEST
OW-A RECOVERY

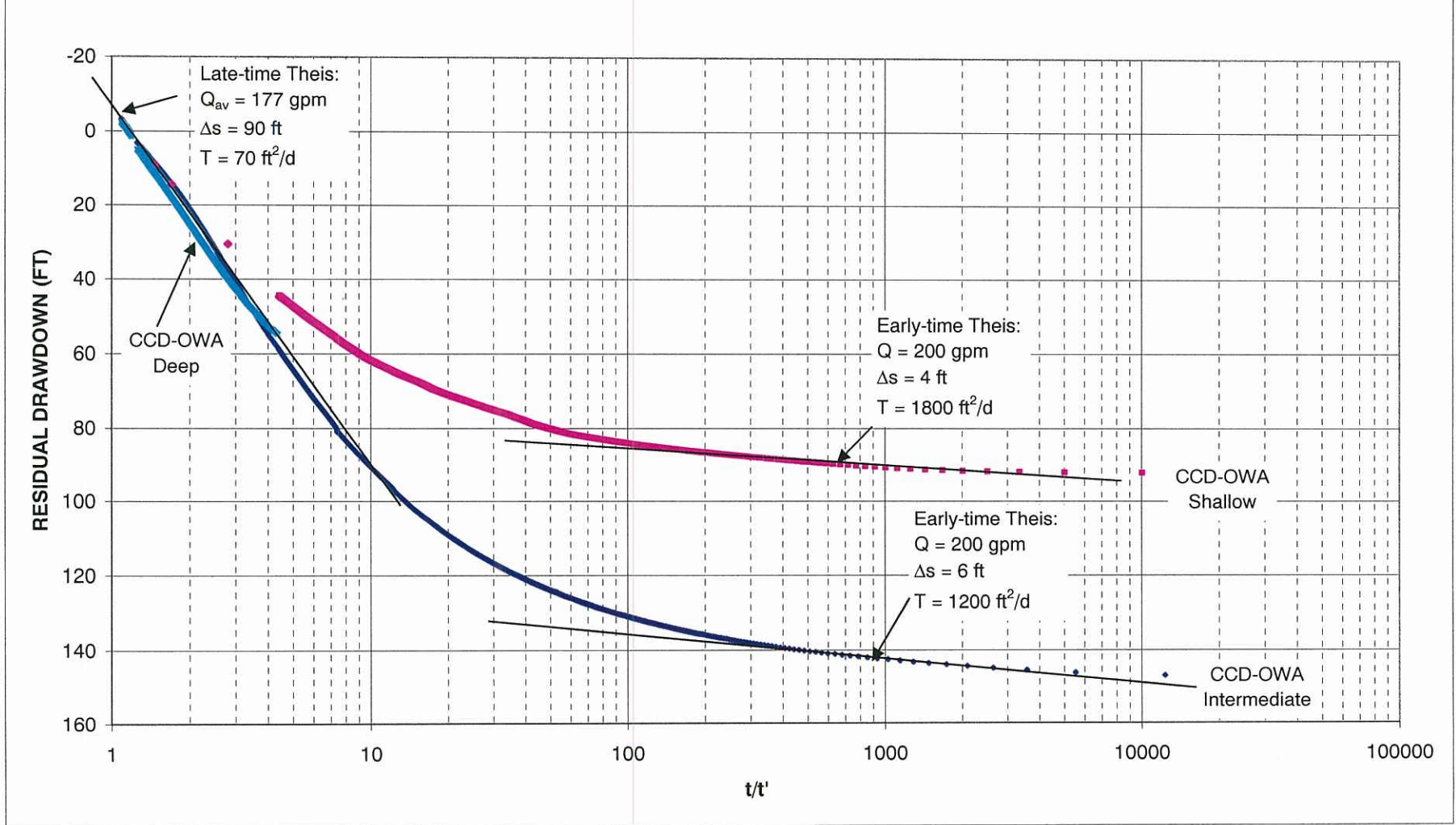
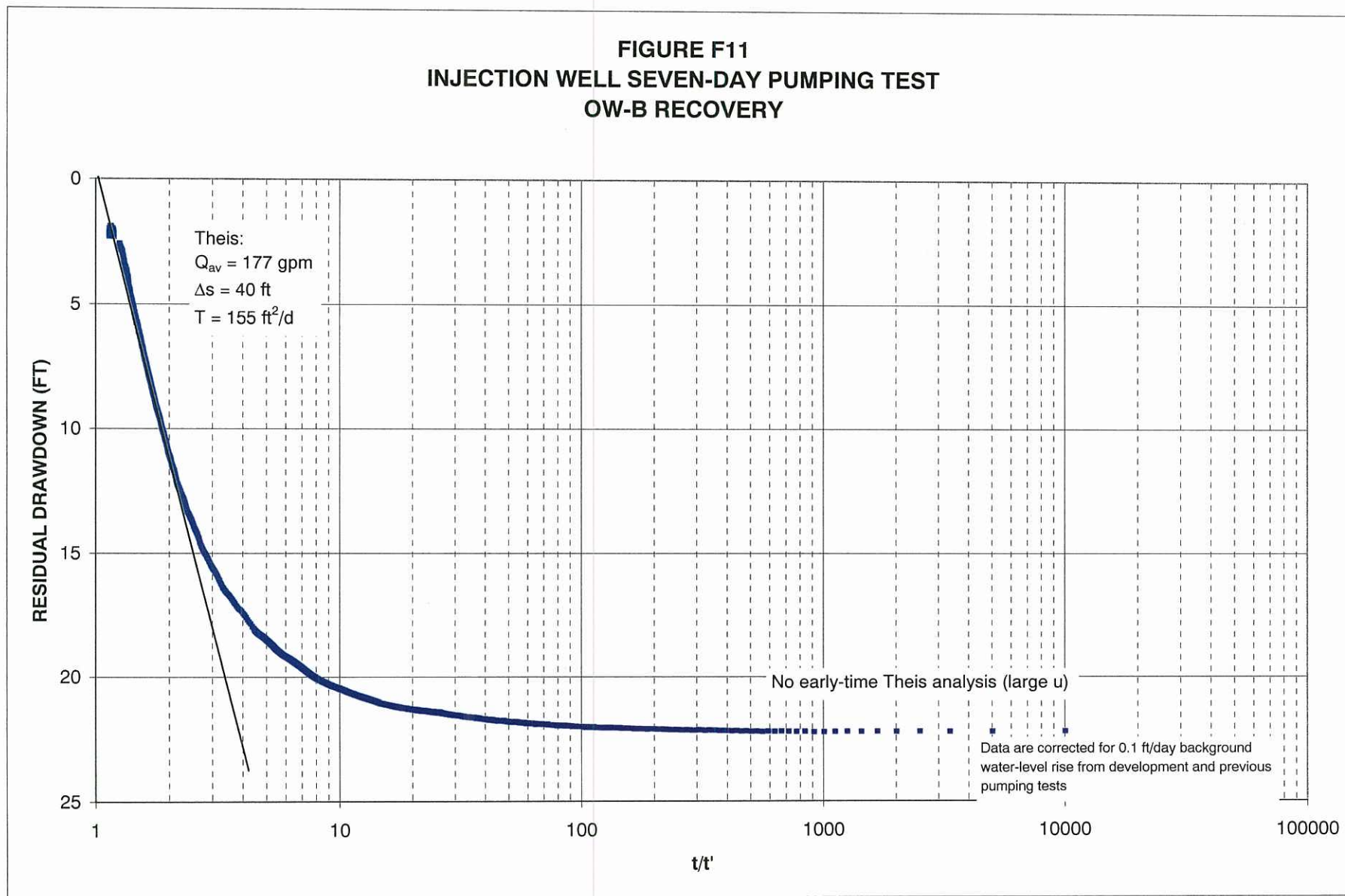
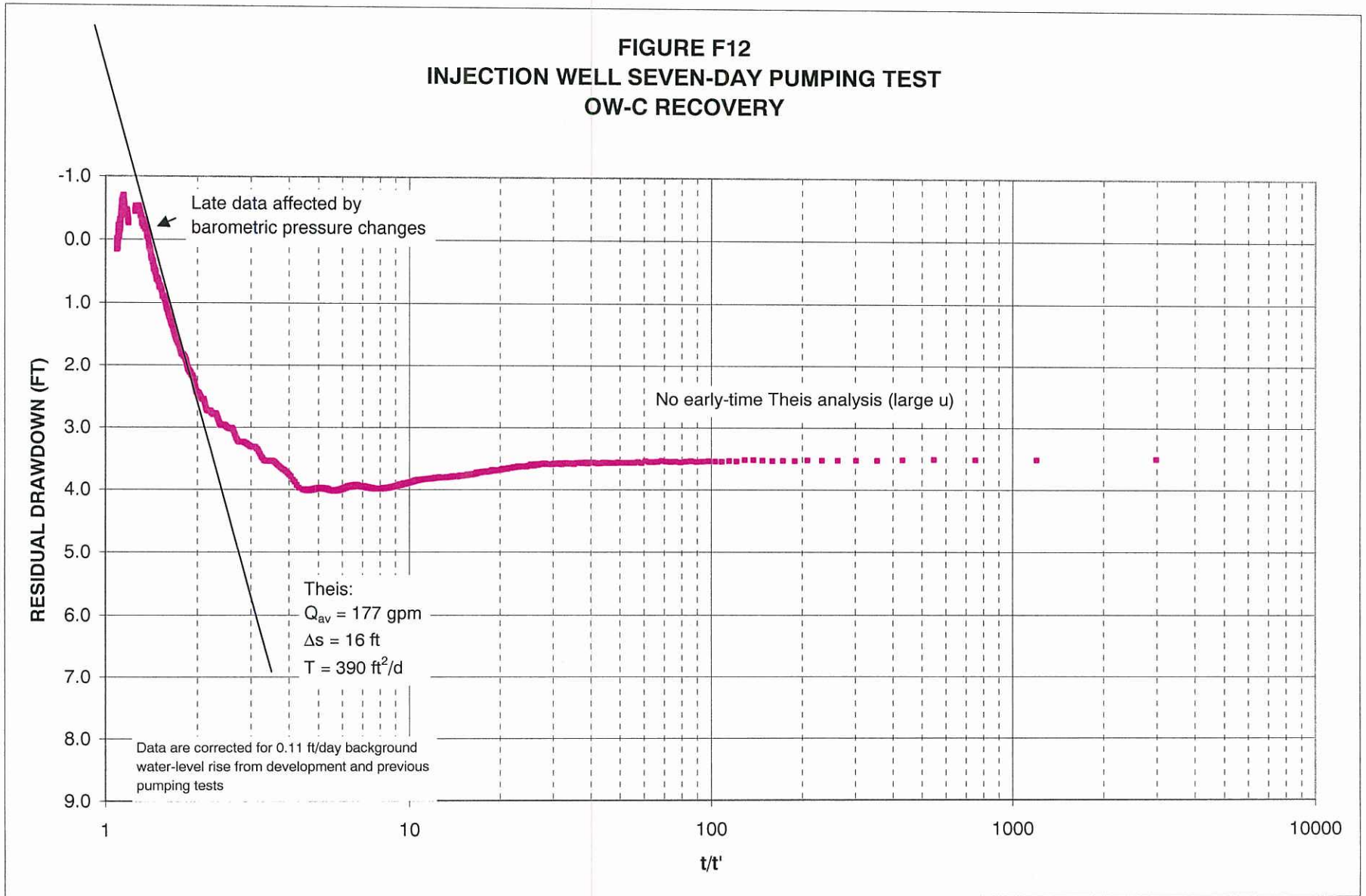


FIGURE F11
INJECTION WELL SEVEN-DAY PUMPING TEST
OW-B RECOVERY



WATER PLAN

FIGURE F12
INJECTION WELL SEVEN-DAY PUMPING TEST
OW-C RECOVERY



RANCHO VIEJO

WATER PLAN

TABLE F1. SUMMARY OF CCD-OWB PUMPING TEST

Well	Purpose	Distance from Test Well (ft)	Pre-Test Water Level (ft below ground)	End of Test Drawdown (ft)	Tested Parameters ^{2,3}			
					T (ft ² /d)	S	n	Late Time Recovery T (ft ² /d)
OWB	Test Well ¹	--	300.7	14.5	1600 ⁴	0.0013	2.0	30
OWA Shallow	Observation	473	298.6	0.33	1600	0.0013	--	590
OWA Intermediate	Observation	473	267.5	0.27	1600	0.0016	2.0	590
OWA Deep	Observation	473	292.0	0	--	--	--	--
Injection Well	Observation	483	296.8	0.17	2000	0.002	2.0	--
OWC	Observation	1513	259.7	0.02	3000	0.0009	2.0	--

¹Tested at 30 gpm for 4.4 hours on May 9, 2006.

²Drawdown analyzed by methods of Walker, D.D., and R.M. Roberts, 2003, Flow dimensions corresponding to hydrogeologic conditions in Water Resources Research, Vol. 39, 1

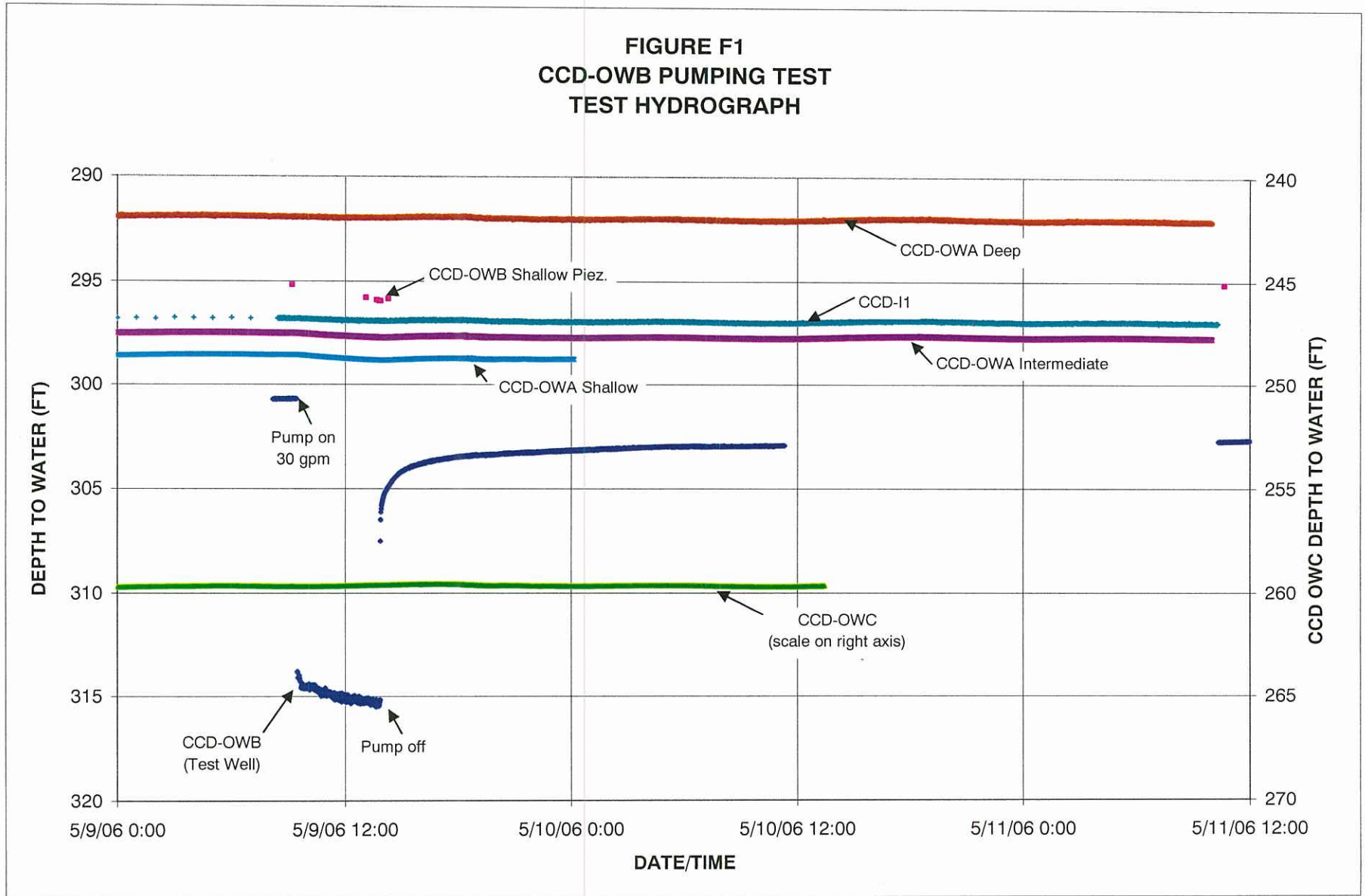
³Drawdown and recovery analyzed by methods of Theis C.V., 1935, The Relation Between the Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Ground-Water Storage: American Geophysical Union, Volume 16, pp. 519-524.

⁴Hydraulic conductivity (k) of test zone = T/screen length = 1600/720 = 2.2 ft/d.

Conclusion: Tested aquifer consists of channel sands (k = 2.2 ft/d) enclosed by fine-grained over bank deposits with less permeability as indicated by late-time recovery data. Flow dimension (n) of 2.0 at observation wells indicates radial flow response compatible with Theis (1935).

WATER PLAN

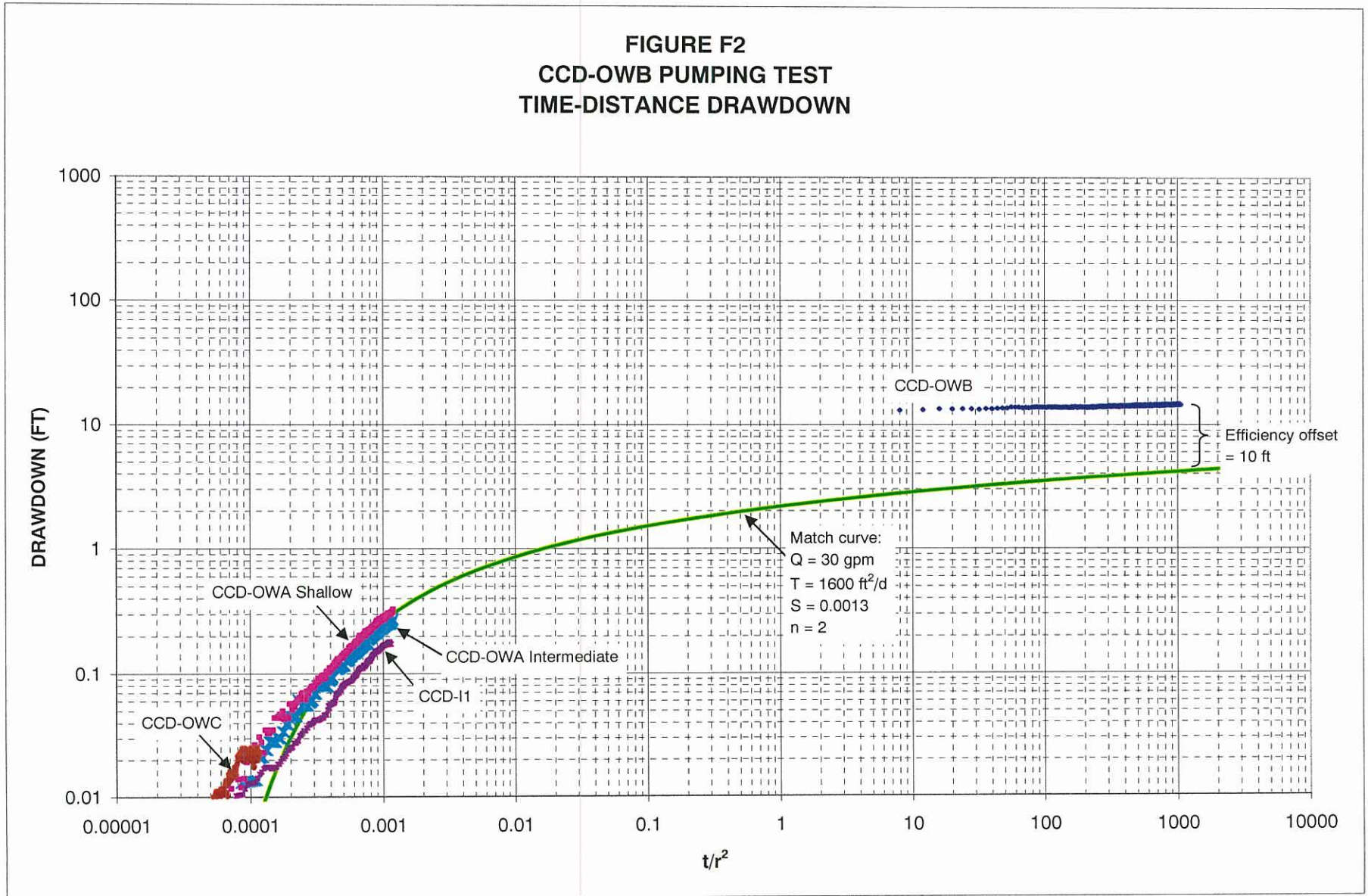
FIGURE F1
CCD-OWB PUMPING TEST
TEST HYDROGRAPH



RANCHO VIEJO

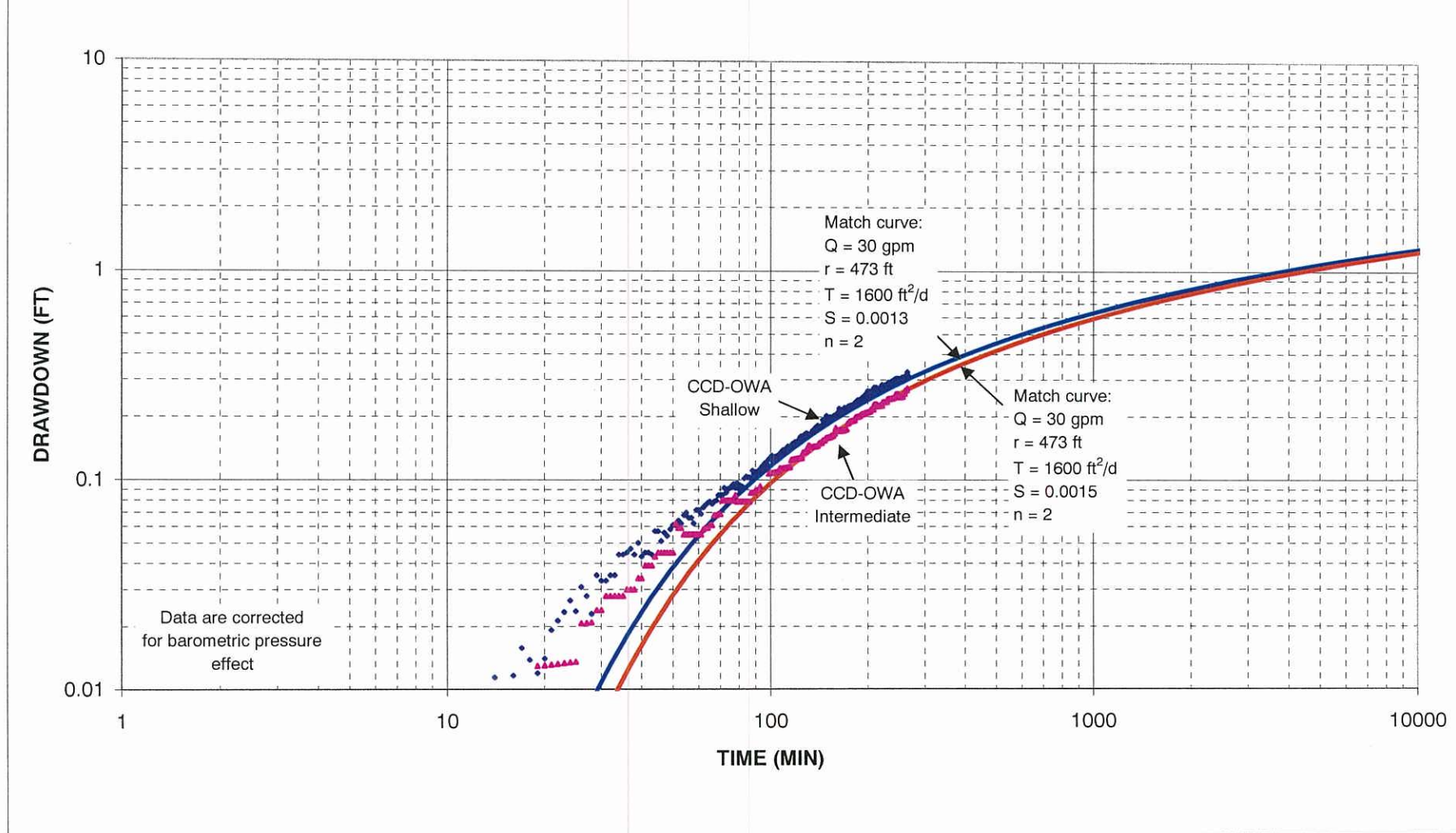
WATER PLAN

FIGURE F2
CCD-OWB PUMPING TEST
TIME-DISTANCE DRAWDOWN



WATER PLAN

**FIGURE F3
CCD-OWB PUMPING TEST
DRAWDOWN AT OBSERVATION WELL CCD-OWA**



WATER PLAN

FIGURE F4
CCD-OWB PUMPING TEST
DRAWDOWN AT OBSERVATION WELL CCD-11

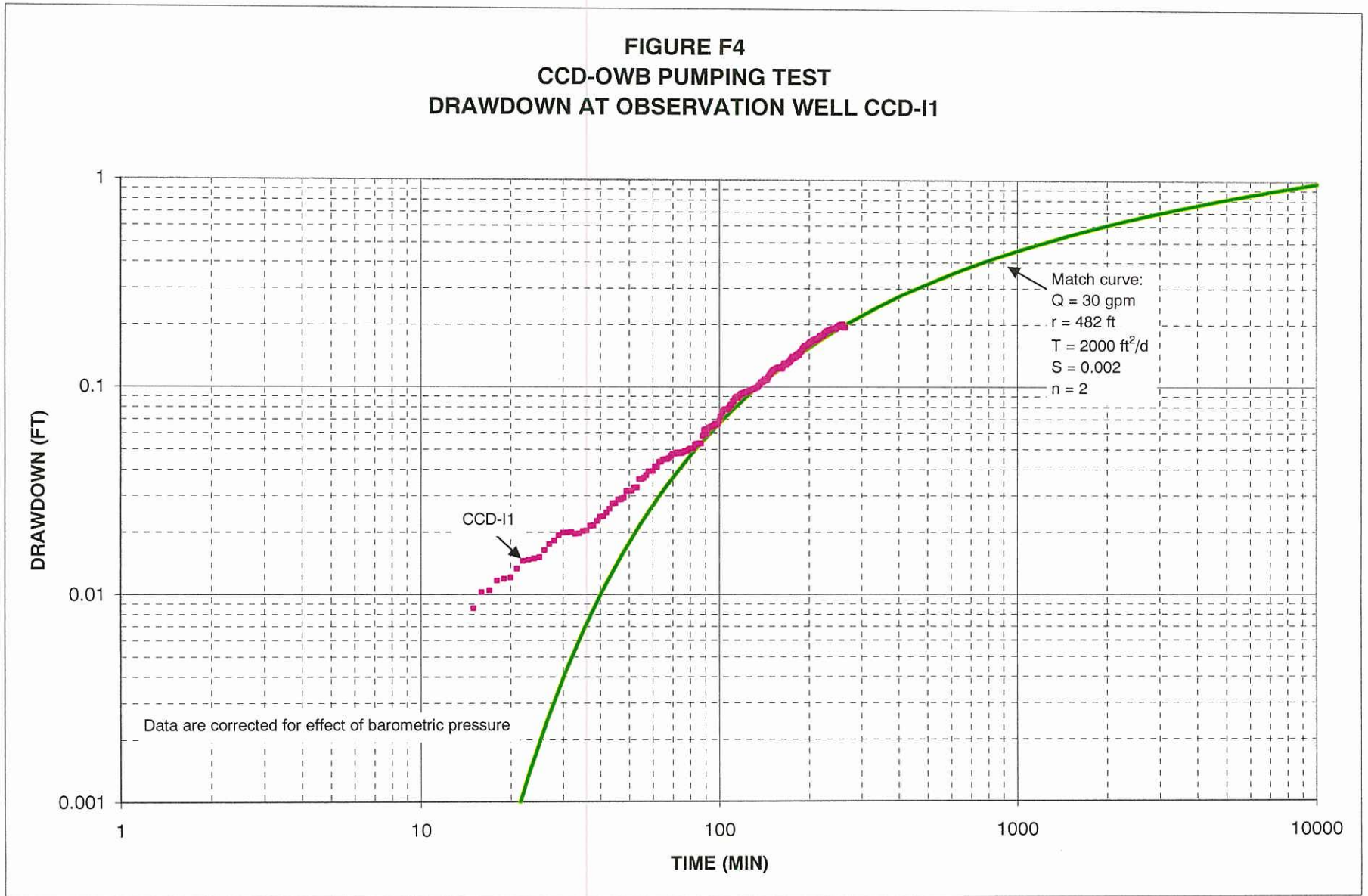
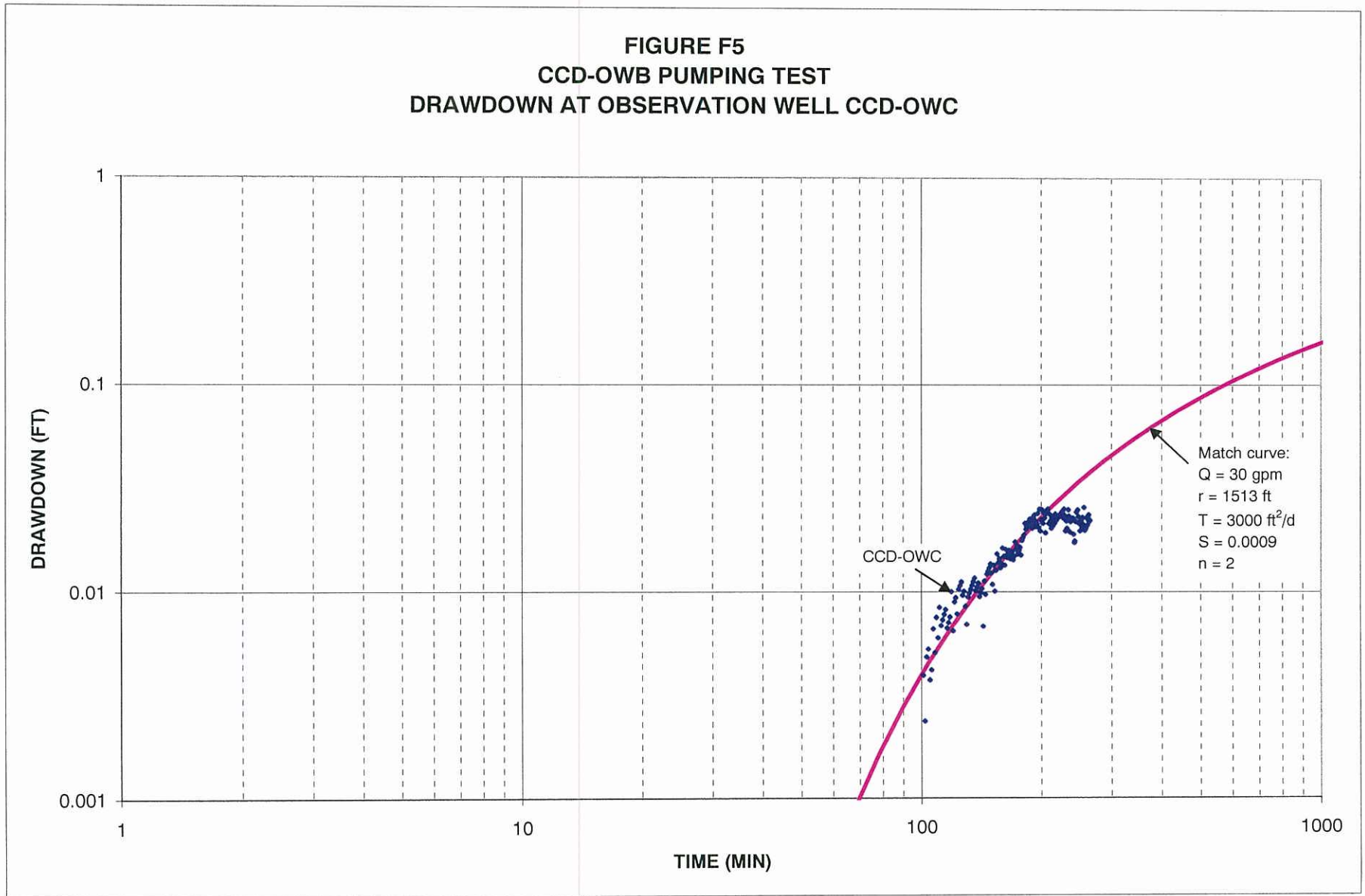
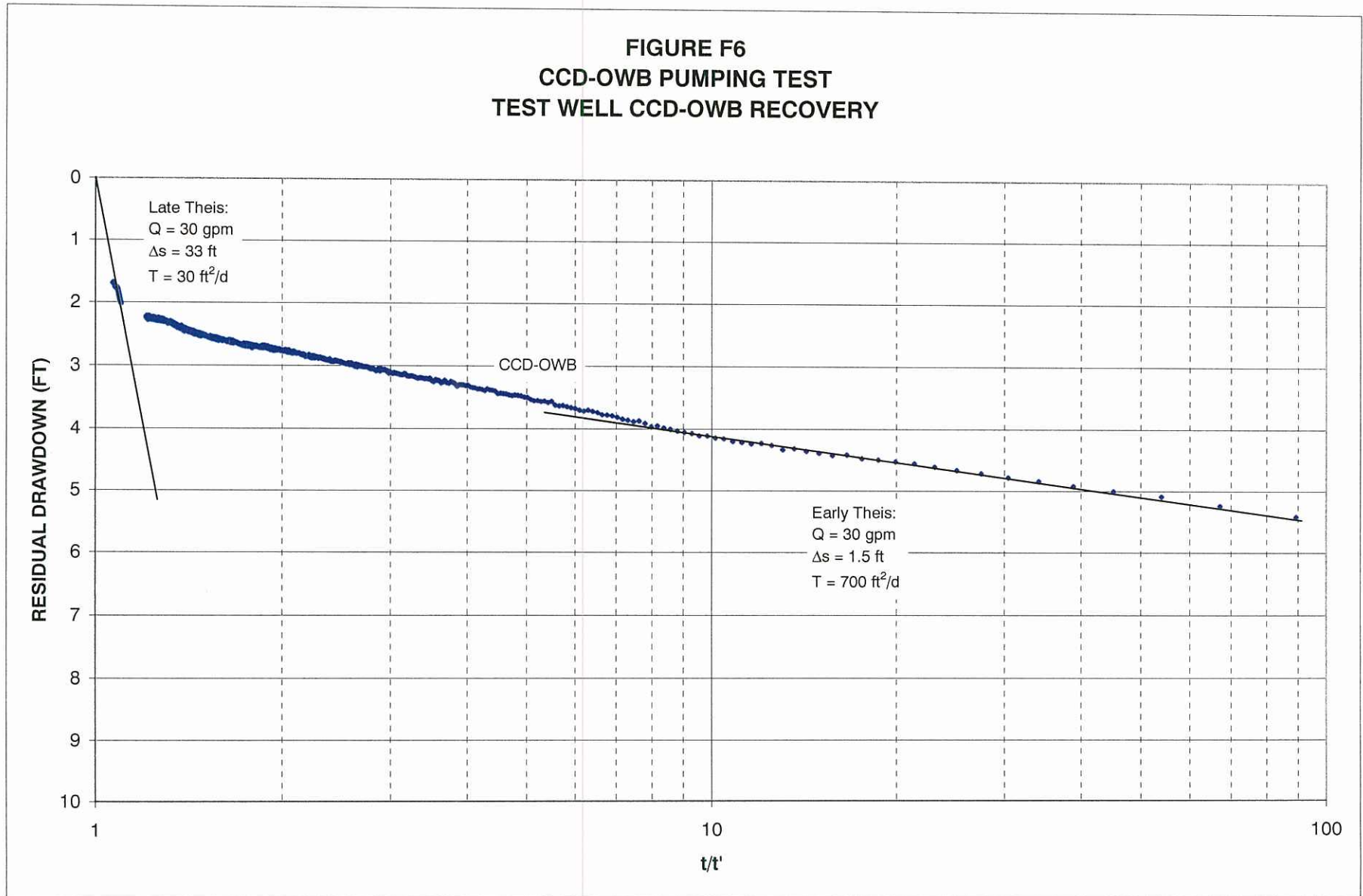


FIGURE F5
CCD-OWB PUMPING TEST
DRAWDOWN AT OBSERVATION WELL CCD-OWC

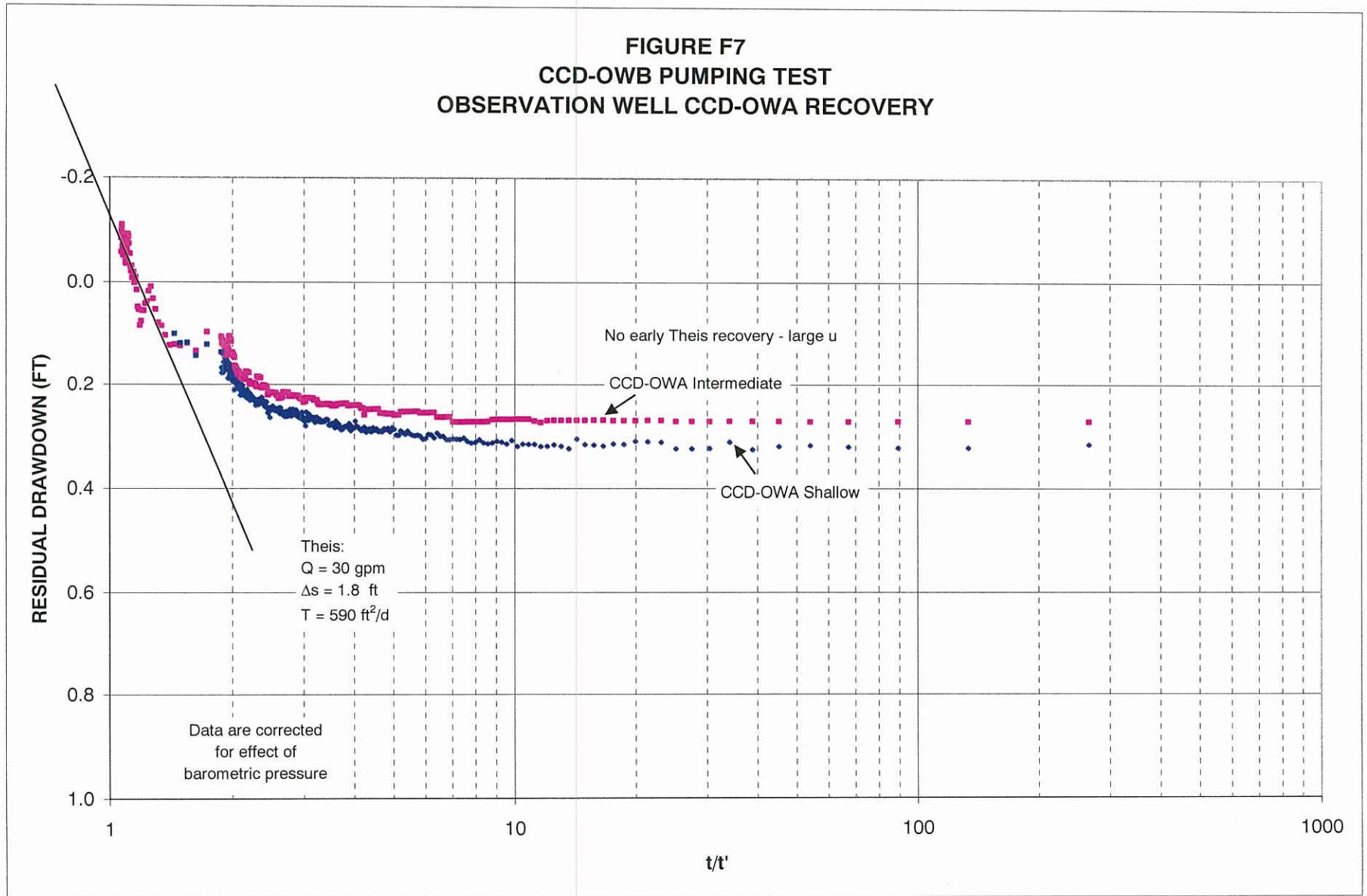


WATER PLAN

FIGURE F6
CCD-OWB PUMPING TEST
TEST WELL CCD-OWB RECOVERY



**FIGURE F7
CCD-OWB PUMPING TEST
OBSERVATION WELL CCD-OWA RECOVERY**



RANCHO VIEJO

WATER PLAN

TABLE F1. SUMMARY OF CCD-OWC PUMPING TEST

Well	Purpose	Distance from Test Well (ft)	Pre-Test Water Level (ft below ground)	End of Test Drawdown (ft)	Tested Parameters ^{2,3}			
					T (ft ² /d)	S	n	Late Time T (ft ² /d)
OWC	Test Well ¹	--	259.61	14.82	635 ⁵	0.0001	2.3	55
OWB	Observation ⁴	1513	302.20	0	--	--	--	--

¹Tested at 36 gpm for 4 hours on May 11, 2006.

²Drawdown analyzed by methods of Walker, D.D., and R.M. Roberts, 2003, Flow dimensions corresponding to hydrogeologic conditions in Water Resources Research, Vol. 39, No. 12, p. 1329.

³Recovery analyzed by methods of Theis C.V., 1935, The Relation Between the Lowering of the Piezometric Surface and the Rate and Duration of Discharge of a Well Using Ground-Water Storage: American Geophysical Union, Volume 16, pp. 519-524.

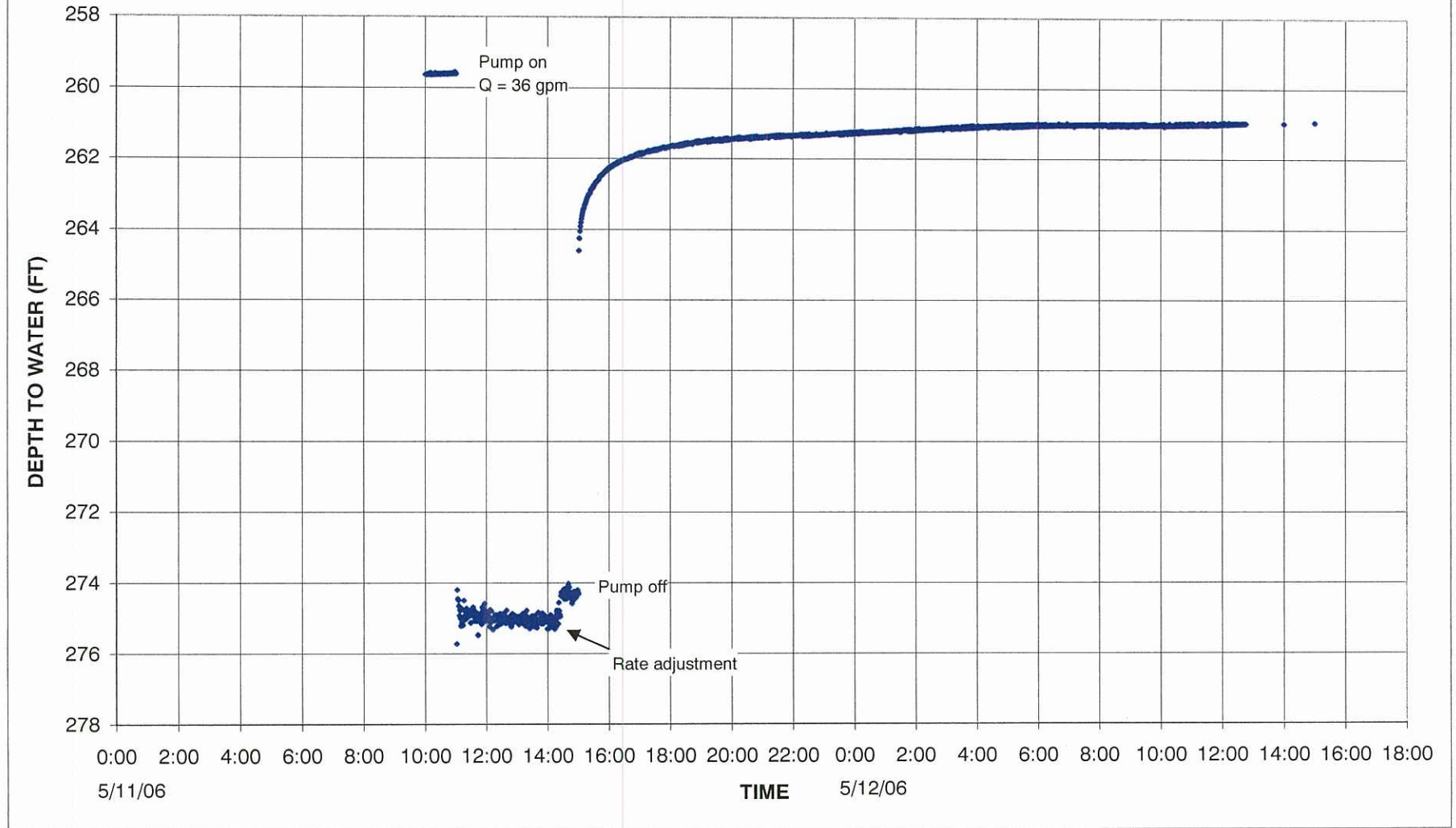
⁴CCD-I1 and OWA also were instrumented during test. No response was observed.

⁵Hydraulic conductivity (k) of test zone = T/screen length = 635/680 = ~1 ft/d.

Conclusion: Tested aquifer consists of channel sands (k = ~1 ft/d) enclosed by fine-grained over bank deposits at about 1/10 permeability based on late-time recovery. Flow dimension (n) of channel sands is 2.3 (leaky radial flow).

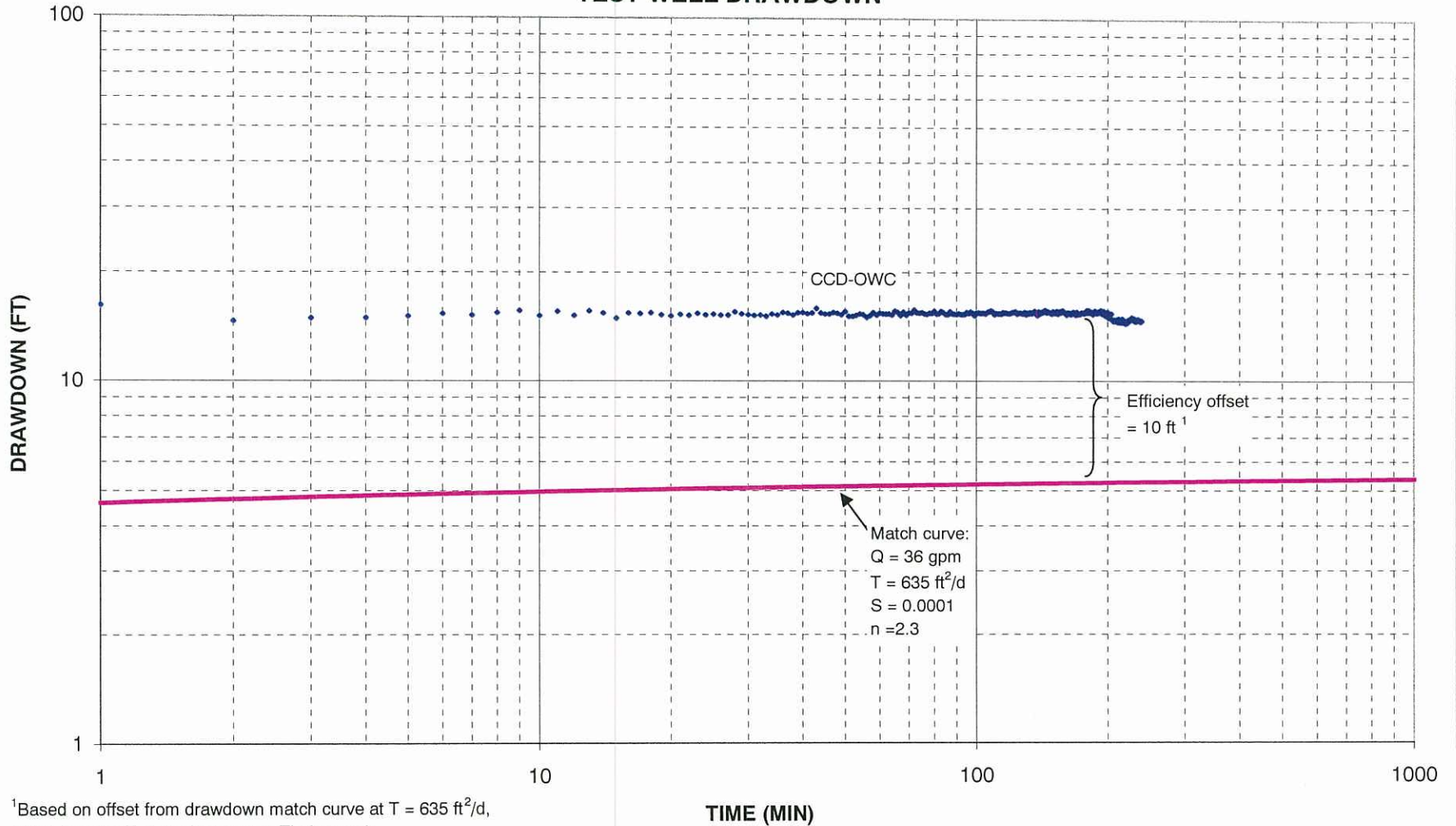
WATER PLAN

FIGURE F1
CCD-OWC PUMPING TEST
TEST HYDROGRAPH



WATER PLAN

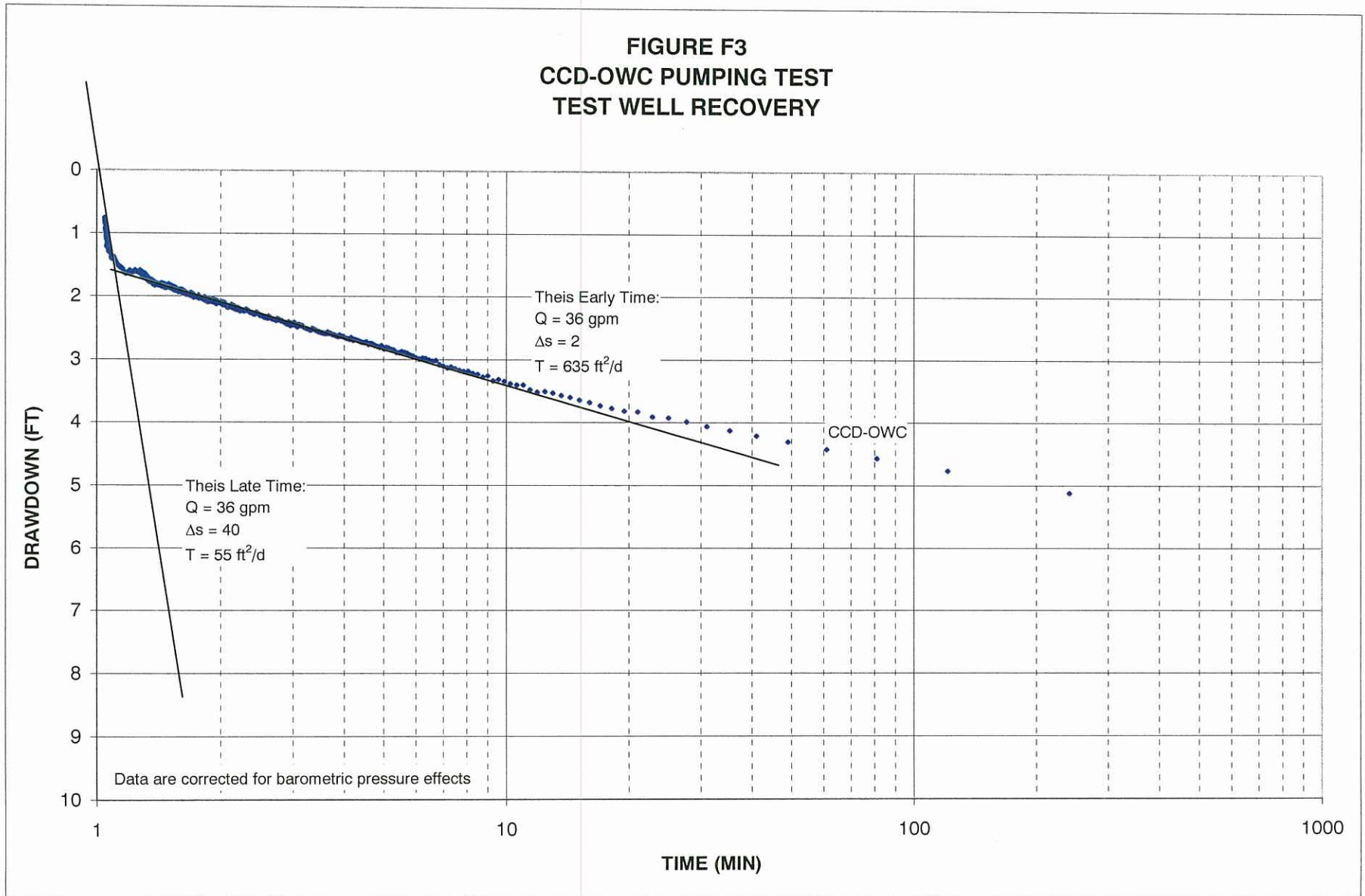
FIGURE F2
CCD-OWC PUMPING TEST
TEST WELL DRAWDOWN



¹Based on offset from drawdown match curve at T = 635 ft²/d, which is same T as early recovery This match.

WATER PLAN

FIGURE F3
CCD-OWC PUMPING TEST
TEST WELL RECOVERY



APPENDIX D

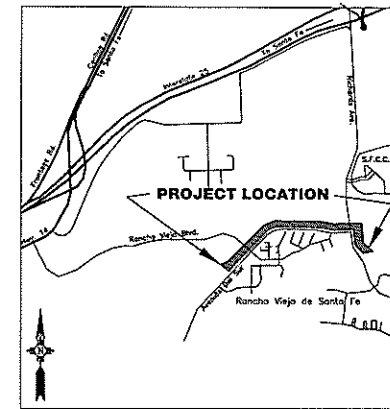
SCHEMATICS OF INJECTION SYSTEM

RANCHO VIEJO DE SANTA FE AQUIFER STORAGE & RECOVERY PROJECT



GENERAL NOTES:

- ALL WORK DETAILED ON THE PROJECT TO BE PERFORMED UNDER THIS CONTRACT SHALL EXCEPT AS OTHERWISE STATED OR PROVIDED FOR HEREIN, BE CONSTRUCTED IN ACCORDANCE WITH THE NEW MEXICO PUBLIC WORKS STANDARD SPECIFICATIONS, 1997 EDITION.
- CONTRACTOR SHALL NOTIFY THE OWNER'S REPRESENTATIVE NOT LESS THAN SEVEN (7) DAYS PRIOR TO STARTING WORK IN ORDER THAT THE OWNER'S REPRESENTATIVE MAY TAKE NECESSARY MEASURES TO ENSURE THE PRESERVATION OF SURVEY MONUMENTS. CONTRACTOR SHALL NOT DISTURB PERMANENT SURVEY MONUMENTS WITHOUT THE CONSENT OF THE OWNER'S REPRESENTATIVE AND SHALL BEAR THE EXPENSE OF REPLACING ANY THAT MAY BE DISTURBED WITHOUT PERMISSION. REPLACEMENT SHALL BE DONE ONLY BY OWNER'S REPRESENTATIVE. WHEN A CHANGE IS MADE IN ANY ROADWAY IN WHICH A PERMANENT SURVEY MONUMENT IS LOCATED, CONTRACTOR SHALL, AT HIS OWN EXPENSE, ADJUST THE MONUMENT COVER TO THE NEW GRADE UNLESS OTHERWISE SPECIFIED.
- ALL EXISTING UTILITIES SHOWN HERE WERE OBTAINED AS ACCURATELY AS POSSIBLE FROM RECORD DRAWINGS AND SURFACE INDICATIONS. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO PROTECT, MAINTAIN IN SERVICE, AND VERIFY EXACT LOCATIONS OF ALL AFFECTED UTILITIES DURING CONSTRUCTION OF THIS PROJECT.
- THE CONTRACTOR SHALL NOTIFY ALL UTILITY COMPANIES WHEN WORKING NEAR THEIR SYSTEMS. TWO DAYS PRIOR TO ANY EXCAVATION, CONTRACTOR MUST CONTACT NEW MEXICO ONE-CALL SYSTEM (1-800-321-ALERT(2537)) FOR LOCATION OF EXISTING UTILITIES.
- PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL EXCAVATE AND VERIFY THE HORIZONTAL AND VERTICAL LOCATIONS OF ALL OBSTRUCTIONS. SHOULD A CONFLICT EXIST, THE CONTRACTOR SHALL NOTIFY THE PROJECT MANAGER SO THAT THE CONFLICT CAN BE RESOLVED WITH MINIMUM AMOUNT OF DELAY.
- ACCESS TO LOCAL BUSINESS AND RESIDENCES SHALL BE KEPT OPEN AT ALL TIMES. TEMPORARY ACCESS CLOSURES, IF REQUIRED, SHALL BE SCHEDULED AT LEAST TWENTY-FOUR (24) HOURS IN ADVANCE WITH PROPERTY OWNER AND APPROVED BY THE PROJECT MANAGER.
- THE CONTRACTOR SHALL DISPOSE OF ALL UNSUITABLE MATERIAL IN AN ENVIRONMENTALLY ACCEPTABLE MANNER AT A LOCATION ACCEPTABLE TO THE PROJECT MANAGER. THERE WILL BE NO DIRECT COMPENSATION FOR THIS WORK.
- CONTRACTOR SHALL BE RESPONSIBLE FOR ANY DAMAGE TO LANDSCAPING AND IRRIGATION SYSTEMS WITHIN WORK AREA NOT COVERED IN THE PLANS.
- CONTRACTOR IS RESPONSIBLE FOR SUPPORTING ANY EXISTING UTILITIES EXPOSED DURING REQUIRED EXCAVATIONS.



VICINITY MAP
NOT TO SCALE

UTILITY COMPANY CONTACTS

ENM - SANTA FE
GAS AND ELECTRIC
STEVE ALGAR (505) 473-3234
P.O. BOX 1288
SANTA FE, NM 87504

QWEST LOCAL NETWORK NDRIN
COMCAST CABLE - SANTA FE
TIM HOY (505) 285-3448
GREAT PLAINS LOCATING SERVICE
4401 ANAHEIM AVE.
ALBUQUERQUE, NM 87113

SANTA FE COUNTY WATER RESOURCES DEPT.
205 MONTEZUMA AVE.
SANTA FE, NM 87501
OFFICE: (505) 992-6870
AFTER HOURS EMERGENCY NUMBER: (505) 885-6623

INDEX TO DRAWINGS

SHEET NO.	DRAWING NO.	DESCRIPTION
1	G-1	TITLE SHEET
2	G-2	QUANTITY SHEET
3	C-1	PLAN
4	C-2	PROFILE
5	C-3	PIPELINE ROAD CROSSING RANCHO VIEJO BLVD.
6	C-4	PIPELINE ROAD CROSSING RICHARDS AVE. AT AVE. DEL SUR
7	P-1	LEGENDS AND SCHEDULES PROCESS FLOW DIAGRAM
8	M-1	PRODUCTION AND INJECTION WELL PIPING PLANS
9	M-2	MECHANICAL DETAILS

RANCHO VIEJO DE SANTA FE AQUIFER STORAGE & RECOVERY PROJECT		NO.	DATE	REV. BY	DESCRIPTION
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QUANTITIES—WELLHEAD PIPING SYSTEM AND CONSTRUCTION		
A. Civil Work – 3–inch transmission line		
	Unit	QUANTITIES
3–inch Pipe, plain end, including all fittings, trench, and backfill	Linear Feet	7400
Bore and jack steel casing for roadway crossings, including carrier pipe spacers	Linear Feet	190
Excavation, Backfill and Compaction for Insertion and Receiving Pits	CY	250
Trail removal and replacement	SY	15
Remove and Replace existing fencing	Linear Feet	160
B. Well Head and Piping Installation		
Submersible Well Pump	Lump Sum	1
Aboveground Piping, Valve and Appurtenances	Lump Sum	1
2.5–inch Galvanized Steel Pipe, schedule 40	Linear Foot	400
2.5–inch Black Iron weld neck flange, class 150#	Each	12
3–inch Galvanized Steel Pipe, schedule 40	Linear Foot	360
3–inch Black Iron weld neck flange, class 150#	Each	20
Heat Tracer Wire	Linear Foot	105
Pipe wrap and insulation	Linear Foot	60
Pipe Supports, stanchions	Lump Sum	9
Security Fence – 6–foot high chain link, embedded in ground	Lump Sum	1

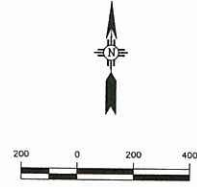
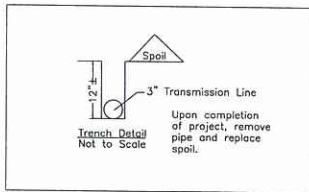
RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT

QUANTITY SHEET

MAB/PCF APRIL 2006	TA/JDL APRIL 2006	NO. DATE	REV. BY REVISIONS (OR CHANGE NOTICES)
DESIGN DATE APRIL 2006	DRAWN DATE APRIL 2006	APPROVAL DATE APRIL 2006	OWNER DATE APRIL 2006
MSH APRIL 2006	PCF APRIL 2006		

URS

SHEET NO. 2 OF 9
DRAWING NO. G-2

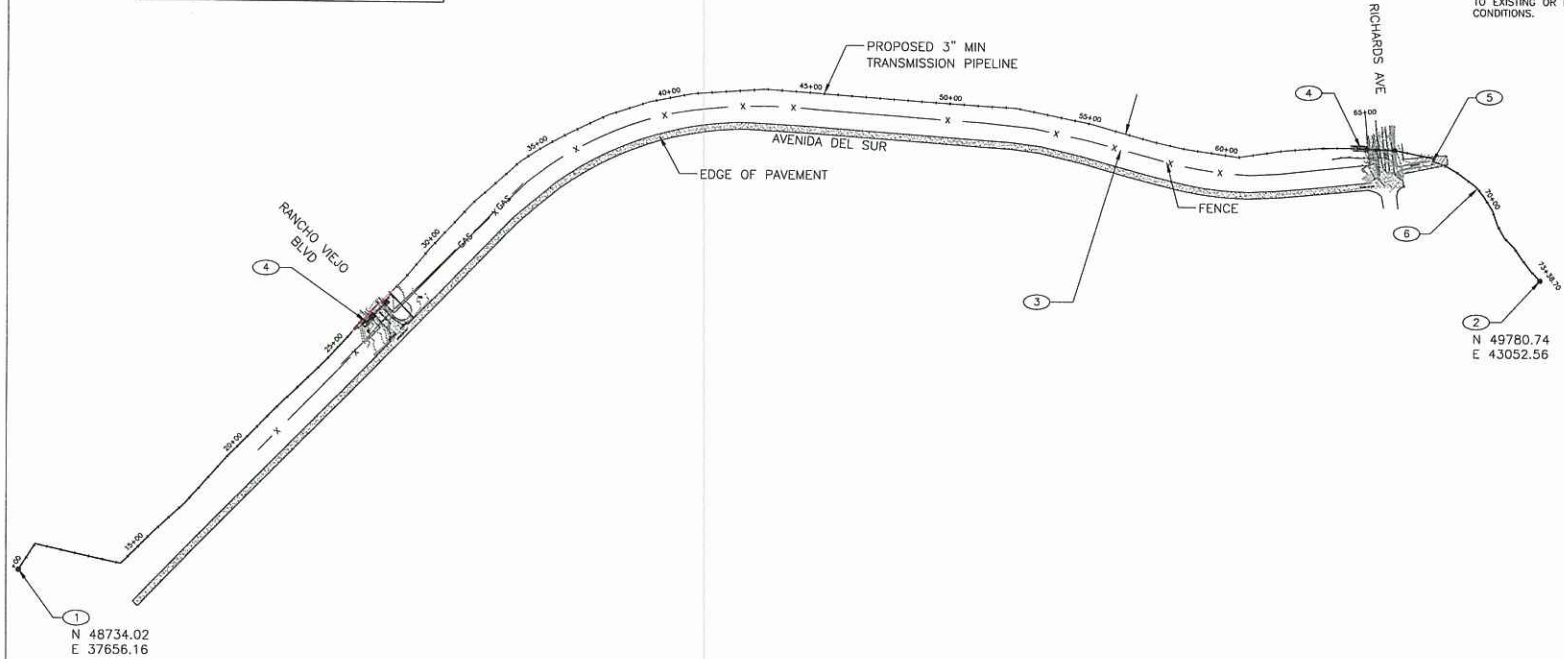


GENERAL NOTES

1. PROJECT COORDINATES ARE MODIFIED NM STATE PLANE, CENTRAL ZONE, NAD 83, NAVD 88.
2. PIPELINE SHALL BE HYDROSTATICALLY TESTED AND DISINFECTED AS PER THE SPECIFICATIONS.
3. IF THIS IS NOT 24"x36", THEN IT IS A REDUCED PLOT. USE GRAPHIC SCALE ACCORDINGLY.

KEY NOTES

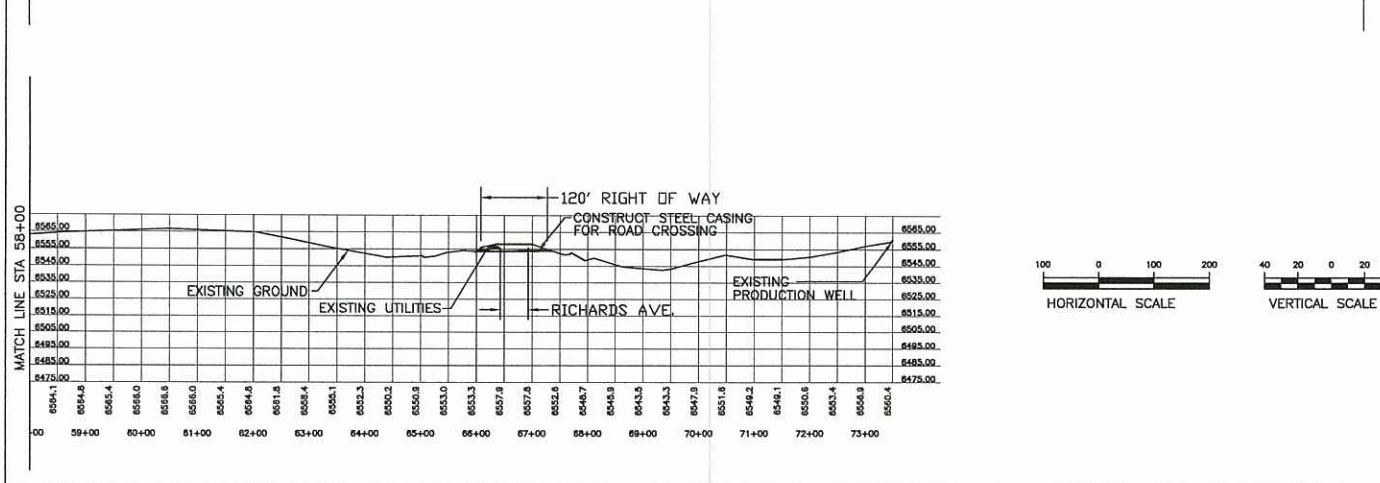
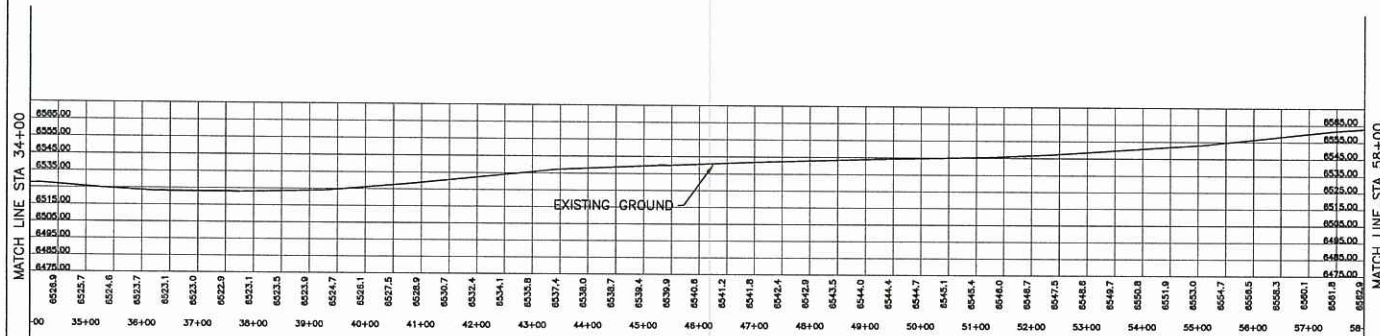
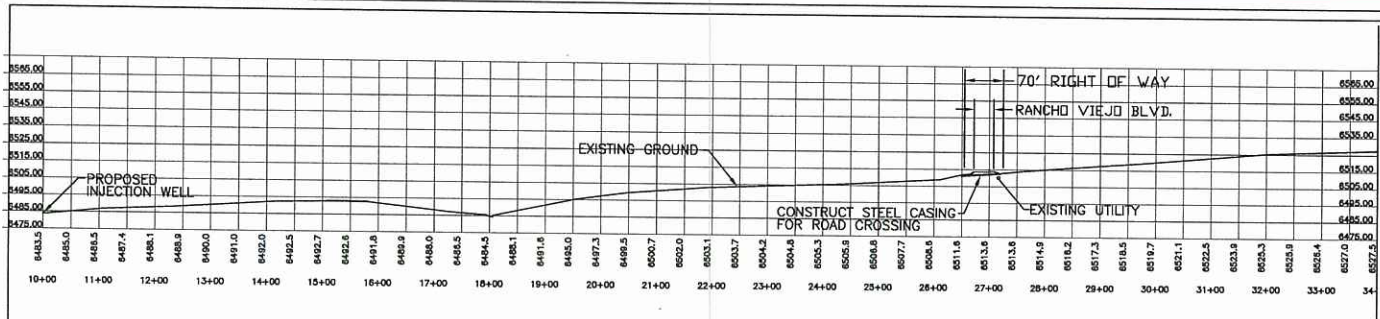
- ① PROPOSED INJECTION WELL.
- ② EXISTING PRODUCTION WELL.
- ③ 60' OFFSET TYPICAL. MAY VARY FOR PRESERVATION OF VEGETATION AND EXISTING SURFACE FEATURES.
- ④ CONSTRUCT STEEL CASING REQUIRED FOR CROSSING. SEE PIPELINE ROAD CROSSING SHEETS.
- ⑤ SANTA FE COUNTY TRAIL. CONSTRUCT BURIED CROSSING. REPLACE TRAIL TO EXISTING OR BETTER CONDITIONS. SEE PIPELINE ROAD CROSSING SHEETS.
- ⑥ DIRT ROAD. CONSTRUCT BURIED CROSSING. REPLACE ROAD SURFACE TO EXISTING OR BETTER CONDITIONS.



①
N 48734.02
E 37656.16

②
N 49780.74
E 43052.56

DESIGN		MAB/PCF		DESIGNER	
APPROVAL		DATE		REVISION (OR CHANGE NOTES)	
DESIGN	DATE	DATE	DATE	NO.	DATE
PCF	APRIL 2006	TA/JDL	APRIL 2006		
DRAWN	DATE	DATE	DATE		
PCF	APRIL 2006				
RANCHO VIEJO DE SANTA FE AQUIFER STORAGE & RECOVERY PROJECT TEMPORARY TRANSMISSION PIPELINE PLAN VIEW					
SHEET NO.	3 OF 9				
DRAWING NO.	C-1				



GENERAL NOTES

- UTILITY LOCATIONS SHOWN HERE ARE APPROXIMATE AND SHALL BE VERIFIED PRIOR TO ANY EARTHWORK, EXCAVATION OR BORING. CONTRACTOR SHALL POTHOLE ALL UTILITIES TO VERIFY HORIZONTAL AND VERTICAL LOCATION WITH SUFFICIENT DETAIL TO AVOID CONTACT DURING EARTHWORK, EXCAVATION OR BORING OPERATIONS. ANY UTILITIES EXPOSED DURING CONSTRUCTION SHALL BE SUPPORTED AND PROTECTED TO THE SATISFACTION OF THE UTILITY OWNER.
- IF THIS IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.



**RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT**

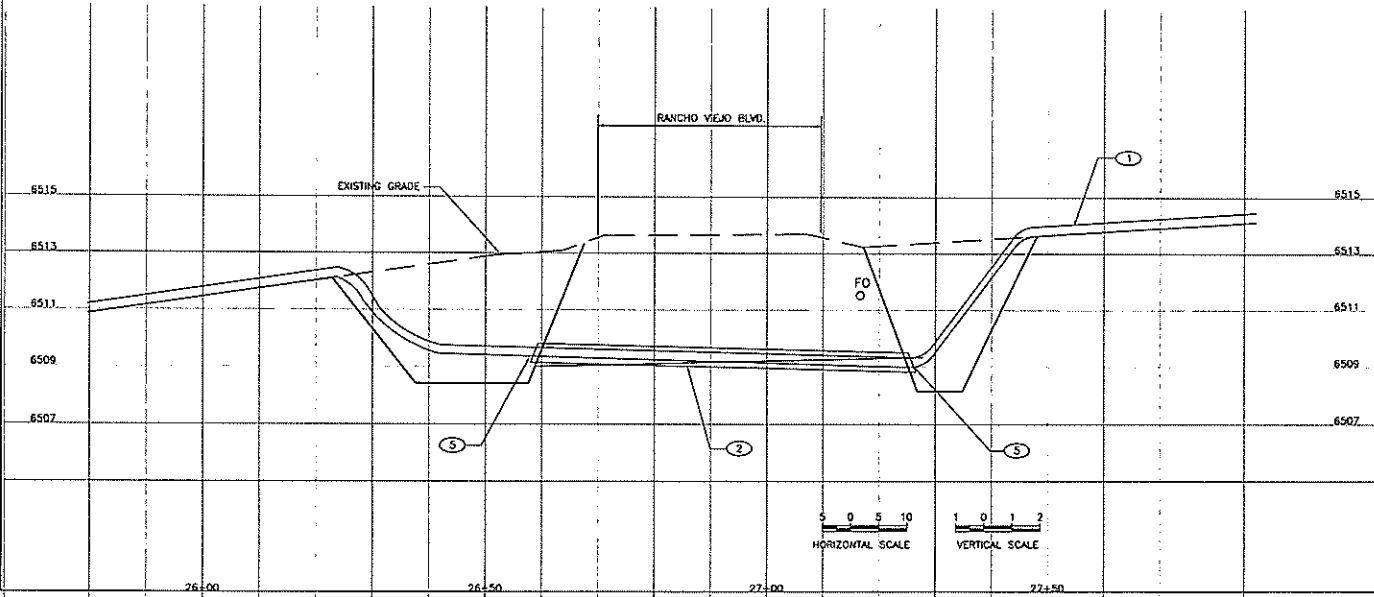
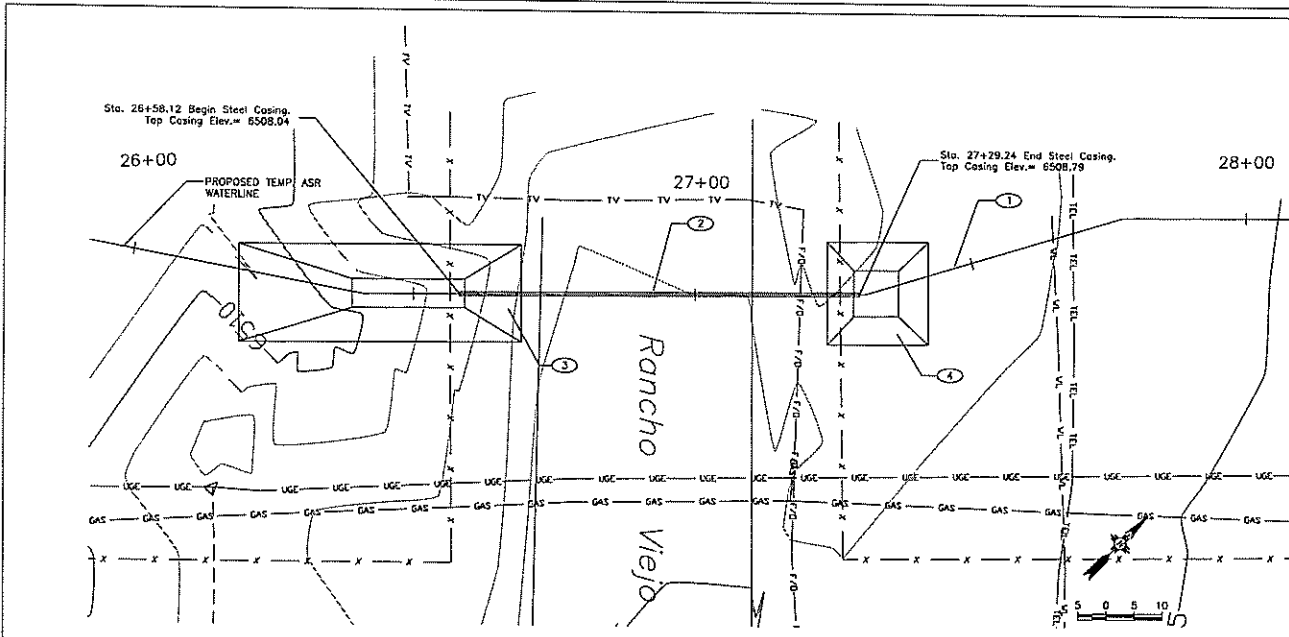
TEMPORARY TRANSMISSION PIPELINE PROFILE

	DESIGN DATE MAY/08	CHECK DATE APRIL 2008	CONSTRUCTION DATE APRIL 2008
	DESIGN DATE APRIL 2008	CHECK DATE APRIL 2008	CONSTRUCTION DATE APRIL 2008

	DESIGN DATE MAY/08	CHECK DATE APRIL 2008	CONSTRUCTION DATE APRIL 2008
	DESIGN DATE APRIL 2008	CHECK DATE APRIL 2008	CONSTRUCTION DATE APRIL 2008

URS

SHEET NO. 4 OF 9
DRAWING NO. C-2



GENERAL NOTES

1. UTILITY LOCATIONS SHOWN HERE ARE APPROXIMATE AND SHALL BE VERIFIED PRIOR TO ANY EARTHWORK, EXCAVATION OR BORING. CONTRACTOR SHALL POthOLE ALL UTILITIES TO VERIFY HORIZONTAL AND VERTICAL LOCATION WITH SUFFICIENT DETAIL TO AVOID CONTACT DURING EARTHWORK, EXCAVATION OR BORING OPERATIONS. ANY UTILITIES EXPOSED DURING CONSTRUCTION SHALL BE SUPPORTED AND PROTECTED TO THE SATISFACTION OF THE UTILITY OWNER.
2. IF ANY CONFLICT IS ENCOUNTERED OR FORESEEN, NOTIFY THE ENGINEER FOR ADJUSTMENT TO THE BORING LOCATION.
3. INSERTION AND RECEIVING PITS SHALL BE EXCAVATED AND SHORED ACCORDING TO OSHA STANDARDS TO PROVIDE A SAFE WORKING ENVIRONMENT. EDGE OF PITS SHALL BE NO CLOSER THEN 2' FROM ANY PAVED SURFACE.
4. A MINIMUM 4' BURRY TO TOP OF STEEL CASING SHALL BE MAINTAINED.
5. REMOVE AND REPLACE FENCING AS NECESSARY FOR BORING AND PIPE INSTALLATION, AS GOOD OR BETTER AS EXISTING.
6. IF THIS IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.

KEY NOTES

- ① 3" CARRIER PIPE
- ② STEEL CASING, BORED AND JACKED INTO PLACE
- ③ INSERTION PIT
- ④ RECEIVING PIT
- ⑤ SUPPORT CARRIER PIPE THROUGH CASING WITH MANUFACTURED SPACERS. FOR INSTALLATION AND SPACING FOLLOW MANUFACTURER'S RECOMMENDATIONS. SEAL END OF CASING WITH EXPANDABLE ANNULAR SPACE SEAL, FLEXIBLE RUBBER SEAL, OR APPROVED EQUAL.

LEGEND

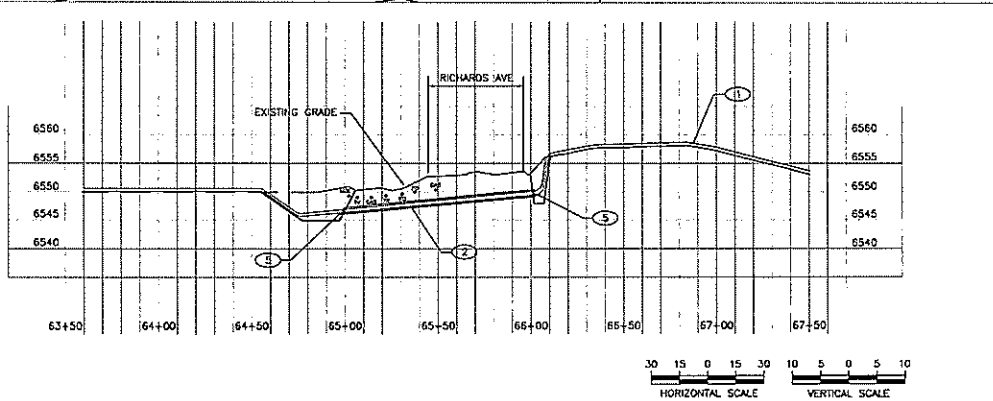
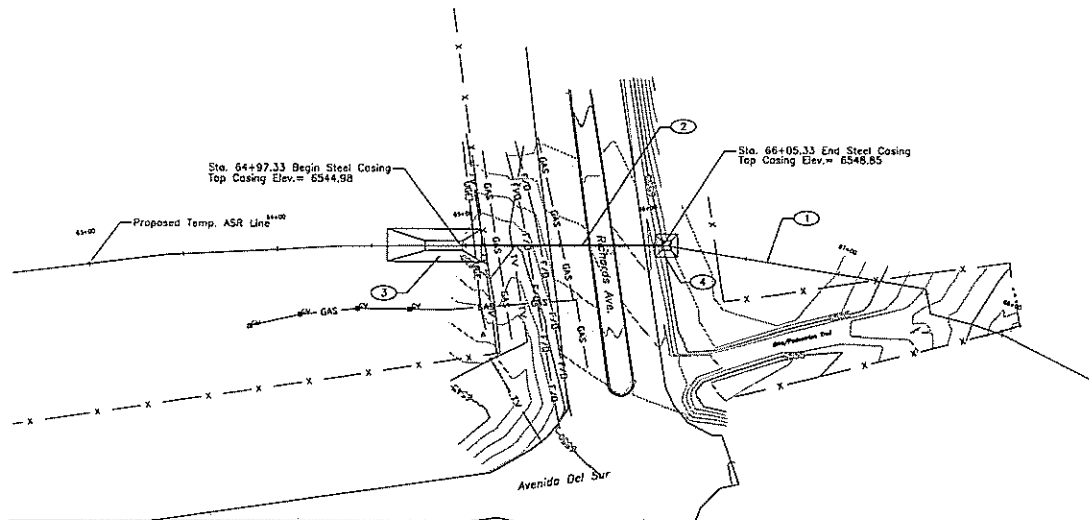
- ELECTRIC
- NATURAL GAS
- CABLE
- WATER LINE
- TELEPHONE
- ▭ EXISTING ROADWAY
- △ TRANSFORMER

RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT
PIPELINE ROAD CROSSING RANCHO VIEJO BLVD
AT AVENIDA DEL SUR

DESIGN	DATE	APPROVAL	DATE
MAJ/PCF	APRIL 2006	MSR	APRIL 2006
DRAWN	DATE	OWNER	DATE
PCF	APRIL 2006	OWNER	DATE
REV. BY	DATE	DESCRIPTION	REV. BY

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SHEET NO. 5 OF 9
DRAWING NO. C-3



GENERAL NOTES

1. UTILITY LOCATIONS SHOWN HERE ARE APPROXIMATE AND SHALL BE VERIFIED PRIOR TO ANY EARTHWORK, EXCAVATION OR BORING. CONTRACTOR SHALL POT-HOLE ALL UTILITIES TO VERIFY HORIZONTAL AND VERTICAL LOCATION WITH SUFFICIENT DETAIL TO AVOID CONTACT DURING EARTHWORK, EXCAVATION OR BORING OPERATIONS. ANY UTILITIES EXPOSED DURING CONSTRUCTION SHALL BE SUPPORTED AND PROTECTED TO THE SATISFACTION OF THE UTILITY OWNER.
2. IF ANY CONFLICT IS ENCOUNTERED OR FORESEEN, NOTIFY THE ENGINEER FOR ADJUSTMENT TO THE BORING LOCATION.
3. INSERTION AND RECEIVING PITS SHALL BE EXCAVATED AND SHORED ACCORDING TO OSHA STANDARDS TO PROVIDE A SAFE WORKING ENVIRONMENT. EDGE OF PITS SHALL BE NO CLOSER THEN 2' FROM ANY PAVED SURFACE.
4. A MINIMUM OF A 4' BURY TO TOP OF CASING SHALL BE MAINTAINED.
5. REMOVE AND REPLACE FENCING AS NECESSARY FOR BORING AND PIPE INSTALLATION, AS GOOD OR BETTER AS EXISTING.
6. IF THIS IS NOT 24"x36", THEN IT IS A REDUCED SIZE PLOT. USE GRAPHIC SCALE ACCORDINGLY.

KEY NOTES

- 1 3" MIN CARRIER PIPE
- 2 STEEL CASING, BORED AND JACKED INTO PLACE
- 3 INSERTION PIT
- 4 RECEIVING PIT
- 5 SUPPORT CARRIER PIPE THROUGH CASING WITH MANUFACTURED SPACERS. FOR INSTALLATION AND SPACING FOLLOW MANUFACTURER'S RECOMMENDATIONS. SEAL END OF CASING WITH EXPANDABLE ANNULAR SPACE SEAL, FLEXIBLE RUBBER SEAL, OR APPROVED EQUAL

LEGEND

- USE — ELECTRIC
- GAS — NATURAL GAS
- TV — CABLE
- WL — WATER LINE
- F/D — TELEPHONE
- ▭ EXISTING ROADWAY
- △ TRANSFORMER

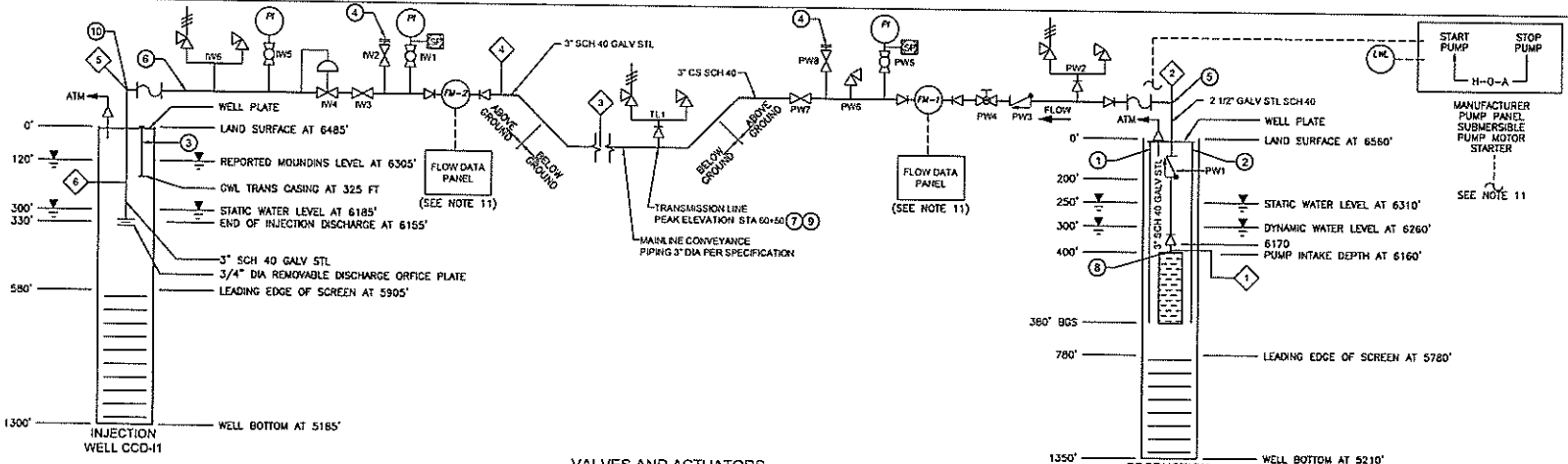
**RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT**

**PIPELINE ROAD CROSSING RICHARDS AVE
AT AVENIDA DEL SUR**

DESIGN	DATE	MAY/06	DATE	APRIL 2006	DESCRIPTION
DESIGN	DATE	APRIL 2006	DATE	APRIL 2006	REVISION (OR CHANGE NOTES)
APPROVAL	DATE	APRIL 2006	DATE	APRIL 2006	
ENGINEER	DATE	APRIL 2006	DATE	APRIL 2006	

URS

SHEET NO. 6 OF 9
DRAWING NO. C-4



FLOW STREAM	SURVEY STATION LOCATION *	OPERATING	
		FLOW RATE (GPM)	LINE PRESSURE (PSI) **
1	STA 73 + 50	50	245
2	STA 73 + 50	50	65
3	STA 60 + 50	50	55
4	STA 10 + 00	50	57
5	STA 10 + 00	50	25
8	STA 10 + 00	50	19

* STATIONING BASED ON PIPELINE ALIGNMENT. STATIONS ARE APPROXIMATE.
 ** OPERATIONS PRESSURES SHOWN ARE APPROXIMATE AND MAY VARY BASED ON ACTUAL SYSTEM OPERATION.

VALVE IDENTIFICATION	VALVE TYPE	FLOW STREAM	DIAMETER (INCHES)	OPERATING PRESSURE (PSI) *
PW1	SPRING LOADED CHECK VALVE	1	2 1/2	245
PW2	AIR VACUUM VALVE	2	1/2	65
PW3	GLOBE CHECK VALVE	2	3	65
PW4	FLOW CONTROL VALVE	2	3	65
PW5	BALL VALVE	2	1/2	65
PW6	SURGE / PRESSURE RELIEF VALVE	2	3	65
PW7	GATE VALVE	2	3	65
PW8	GATE VALVE	2	3	65
TL1	COMBINATION AIR VALVE	3	1	57
FW1	BALL VALVE	4	1/2	57
FW2	GATE VALVE	4	3	57
FW3	GATE VALVE	4	3	57
FW4	PRESSURE REDUCING VALVE	4	3	25
FW5	BALL VALVE	4	1/2	25
FW6	AIR VACUUM VALVE	5	1/2	25

* OPERATING PRESSURES SHOWN ARE APPROXIMATE AND MAY VARY BASED ON ACTUAL SYSTEM OPERATION.

METER IDENTIFICATION	TYPE	SIZE (IN)	MINIMUM FLOW (GPM)	TOTALIZER
FM-1	MCGROMETER ML-08-D PROPELLER TYPE	2"	35	US GALLONS
FM-2	MCGROMETER ML-08-D PROPELLER TYPE	2"	35	US GALLONS

PUMP IDENTIFICATION	PUMP FUNCTION/PERFORMANCE	PUMP TYPE	PUMP (HP)	PERFORMANCE DATA
P-1	PRODUCTION WELL COPP1 PUMP DEDICATED WELL PUMP	SUBMERSIBLE	15	GOLDS MODEL 70L15 50 GPM @ 575 FT HEAD

VALVES AND ACTUATORS

NORMALLY OPEN	VALVE TYPE	NORMALLY CLOSED
	GATE VALVE	
	GLOBE VALVE	
	BALL VALVE	
	CHECK VALVE	N/A
	FLEX COUPLING	N/A
	COMBINATION AIR VENT / VACUUM RELIEF VALVE	N/A
	SURGE RELIEF / PRESSURE RELIEF VALVE	N/A
	PRESSURE REDUCING VALVE	N/A

PIPE SPECIALTIES

SYMBOL	TYPE
	FLOW METER
	FLOW DIRECTION
	FLOW STREAM INDICATOR
	REDUCER
	PRESSURE INDICATOR
	SAMPLE PORT

KEY NOTES:

- PRODUCTION WELL LOW WATER LEVEL TRANSDUCER CASING SHALL BE 1 1/2 INCH SCH 80 PVC AND INSTALLED BELOW GROUND SURFACE TO ELEV 6185.
- PRODUCTION WELL - GROUNDWATER LEVEL TRANSDUCER CASING (SOUNDING TUBE) CASING SHALL BE 1 1/2 INCH SCH 80 PVC AND INSTALLED BELOW GROUND SURFACE TO ELEVATION 6180.
- INJECTION WELL - GROUNDWATER LEVEL TRANSDUCER CASING (SOUNDING TUBE) 1 1/2 INCH SCH 80 PVC SET AT 325 FEET BGS.
- PUMP TO WASTE BYPASS LINE.
- ABOVE GROUND ALIGNMENT FOR THE PRODUCTION WELL WELLHEAD PIPING SHALL BE INSTALLED TO PIPE CENTERLINE ELEV 6562.5 FT.
- ABOVE GROUND ALIGNMENT FOR THE INJECTION WELL WELLHEAD PIPING SHALL BE INSTALLED TO PIPE CENTERLINE ELEV 6487.5 FT.
- MANLINE TRANSMISSION SHOWN AS REFERENCE TO THE CONVEYANCE SYSTEM ONLY. THE MANLINE TRANSMISSION INCREASES IN ELEV FROM THE LOCATION OF THE PRODUCTION WELL AT PIPE ALIGNMENT ELEV 6562.6 FT TO A PIPE ALIGNMENT ELEV OF 6570 AT STATION 60+50. LINE DECREASES IN ELEV TOWARDS THE INJECTION WELL LOCATED AT A PIPE ALIGNMENT ELEVATION OF APPROXIMATELY 6187.5 FT.
- PROVIDE DIELECTRIC FITTING AT PUMP DISCHARGE TRANSITION TO GALV STEEL.
- CONTRACTOR SHALL INSTALL A COMBINATION AIR RELIEF VALVE AT TRANSMISSION LINE STATION 65+50 ELEVATION 6570.1 FT AS APPROVED BY THE ENGINEER. VALVE SHALL BE SIMILAR OR APPROVED TO APCO WILLIAMSITE MODEL NO. 143C, CL 250 CI WITH NSF APPROVED EPOXY COATING.
- MODIFIED WELL SEAL RISER FOR DOWN PIPE ACCESSIBILITY.

PROCESS FLOW DIAGRAM ABBREVIATIONS

ATM	ATMOSPHERIC	HP	HORSE POWER
AW	AIR VENT/VACUUM	LWL	LOW WATER LEVEL
	RELIEF VALVE	NC	NORMALLY CLOSED
BA	BALL VALVE	PI	PRESSURE INDICATOR
BS	BELOW GROUND SURFACE	PRV	PRESSURE REDUCING VALVE
CB	CONCENTRIC REDUCER	PVC	POLYVINYL CHLORIDE
CC	COMBINATION	Q	FLOW DIRECTION
CS	CARBON STEEL	R	REDUCER
CV	CHECK VALVE	S	SAMPLE PORT
ECC	ECCENTRIC REDUCER	SCH	SCHEDULE
ESS	ECCENTRIC REDUCER	SS	STAINLESS STEEL
ELEV	ELEVATION	SR	STANDARD DIMENSION RATIO
FM	FLOW METER	SRV	SURGE-PRESSURE RELIEF VALVE
FT	FEET	STL	STEEL
GALV	GALVANIZED	TDH	TOTAL DYNAMIC HEAD
GPM	GALLONS PER MINUTE	TR	TRANS DUCER
GV	GLOBE VALVE	TYP	TYPICAL
GR	GRADE		
GV	GATE VALVE		
GWL	GROUNDWATER LEVEL		

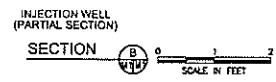
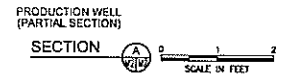
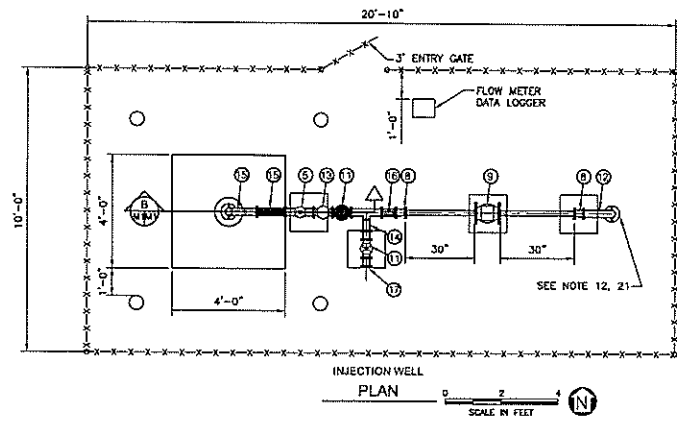
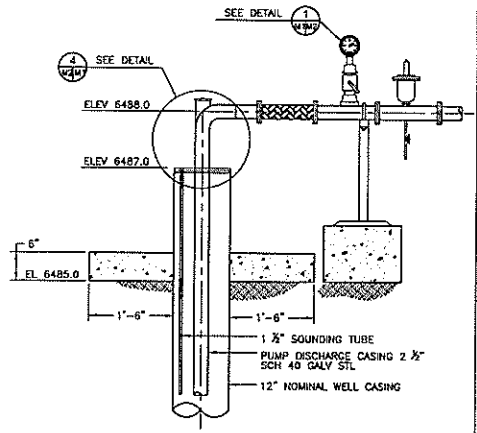
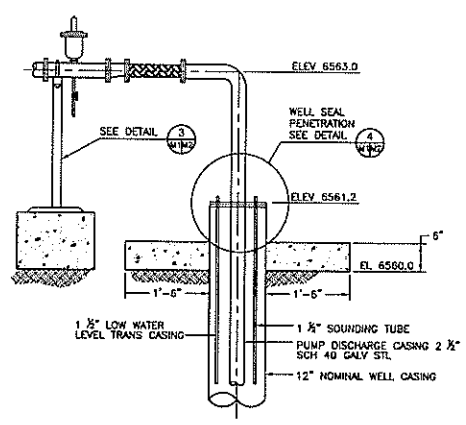
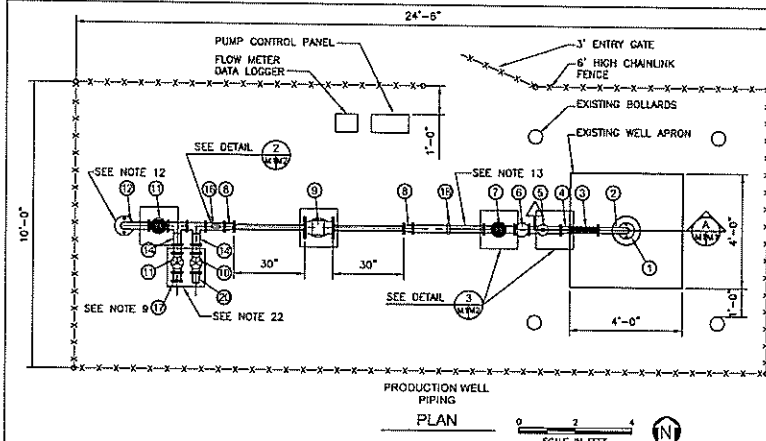
PROCESS FLOW NOTES:

- PROCESS FLOW IS NOT TO SCALE, AND MAY NOT SHOW ALL FITTINGS, AND INFRASTRUCTURE FOR A COMPLETE INSTALLATION.
- WELL DETAILS AND WATER LEVEL DATA PROVIDED BY BALLEAU GROUNDWATER INC.
- STATIC WATER LEVEL AND DYNAMIC WATER LEVEL SHOWN FOR THE PRODUCTION WELL IS BASED ON A WELL DRAWDOWN OF 50 FEET AT A DISCHARGE FLOWRATE OF 50 GPM.
- STATIC WATER LEVEL AND DYNAMIC WATER LEVEL SHOWN FOR THE INJECTION WELL BASED ON AN ANTICIPATED WELL INJECTION FLOW RATE OF 50 GPM AT 12 PSI.
- ALL BELOW GRADE PIPING SHALL BE 3-INCH DIAMETER PLAIN END SCHEDULE 80 PVC TYPE 1.
- ALL ABOVE GROUND PIPING SHALL BE SCH 40 HOT DIPPED GALV ASTM A53 B TO THE DIAMETERS SPECIFIED.
- PRODUCTION WELL COPP1 AND THE INJECTION WELL ARE EXISTING. CONTRACTOR TO FURNISH AND INSTALL PUMP, COLUMN PIPE, INJECTION WELL DISCHARGE PIPE, WELL HEAD PIPING/APERTURANCES/FITTINGS, AND MAIN LINE CONVEYANCE PIPING.
- THE CONTRACTOR IS NOTIFIED THAT THE WORK INVOLVES INSTALLATION OF A GROUNDWATER PUMP SUPPLY AND INJECTION SYSTEM. GROUNDWATER ASSOCIATED WITH THE AQUIFER SHALL BE CONSIDERED DRINKING WATER QUALITY AND ALL MATERIALS, PIPING AND COMPONENTS FURNISHED AND INSTALLED BY THE CONTRACTOR SHALL CONFORM TO NATIONAL SANITATION FOUNDATION STANDARDS 80 AND 61 AS ADOPTED BY THE STATE OF NEW MEXICO.
- ALL ABOVE GROUND REDUCERS SHALL BE ECCENTRIC.
- ALL FITTINGS SHALL BE FLANGED AS SHOWN ON DWG M-1.
- ELECTRICAL DESIGN SHALL BE PROVIDED BY OTHERS. PROCESS FLOW SHOWS MANUFACTURER PUMP PANEL AND LOW WATER CONDITION INTERFACE FOR PROCESS CLARIFICATION ONLY.

RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT

REVISION	DATE	BY	CHKD	APP'D	DESCRIPTION
1	MAR 2006	JML	JML		ISSUE FOR PERMITTING
2	APRIL 2006	JML	JML		REVISED PER PERMITTING COMMENTS
3	APRIL 2006	JML	JML		REVISED PER PERMITTING COMMENTS
4	APRIL 2006	JML	JML		REVISED PER PERMITTING COMMENTS

URS
 SHEET NO. 7 OF 9
 DRAWING NO. P-1



- NOTES:**
1. ALL FLANGES SHALL BE COMPATIBLE.
 2. DIELECTRIC FLANGE KITS SHALL BE INSTALLED WHERE FITTINGS FABRICATED OF DISIMILAR METALS ARE INSTALLED.
 3. DIMENSIONS SHOWN ON EACH PLAN ARE APPROXIMATE AND MAY NOT REFLECT THE EXACT SIZE AND DIMENSIONS OF COMPONENTS.
 4. ORIFICE PLATE FOR THE FLOW CONTROL VALVE SHALL BE PLACED AT LEAST 5 PIPE DIAMETERS DOWNSTREAM OF THE CONTROL VALVE.
 5. SPRING LOADED CHECK VALVE SHALL BE INSTALLED ON THE PUMP DISCHARGE PIPE AT A VERTICAL LOCATION 200 FEET ALONG THE DISCHARGE.
 6. UNLESS OTHERWISE SPECIFIED, CONTRACTOR SHALL MAINTAIN ALL SPACING REQUIREMENTS FOR VALVES AND FITTINGS AS RECOMMENDED BY THE MANUFACTURER.
 7. ALL COMPONENTS, VALVES, FITTINGS, PIPING, APPURTENANCES, SEALANTS AND FLANGES SHALL BE IN CONFORMANCE WITH NSF 60 AND 61 AS REQUIRED BY THE STATE OF NEW MEXICO.
 8. FENCING SHALL BE INSTALLED PER SPECIFICATION 02830.
 9. BLIND FLANGES SHALL BE INSTALLED ON EACH PUMP TO WASTE VALVE DISCHARGE AS SHOWN.
 10. ALL CONTROL TYPE VALVES SHALL BE HYDRAULICALLY OPERATED.
 11. PUMP CONTROL AND FLOW METER DATA LOGGER PANEL SHALL BE INSTALLED AND SUPPORTED WITH GALVANIZED STEEL UNISTRUT FRAMING. FRAMING SHALL BE INSTALLED WITH EMBEDDED POSTS AND SHALL BE CAPABLE OF SUPPORTING THE DEAD WEIGHT AND DYNAMIC LOADING OF THE PANEL, UNLESS SPECIFIED OTHERWISE. TOP OF PANEL HEIGHT SHALL NOT EXCEED 5 FEET ABOVE GROUND SURFACE.
 12. UNDERGROUND TRANSITION SHALL BE INSTALLED WITH 45 DEGREE ELBOWS AND STRAIGHT PIPE AS REQUIRED TO ACHIEVE A TOP OF PIPE CROWN DEPTH OF 36-INCHES. PIPING SHALL BE WRAPPED WITH 20-MIL PVC TAPE, DOUBLE WRAPPED AROUND CIRCUMFERENCE OF PIPE AND FITTINGS. WRAP SHALL BEGIN AT 6-INCHES ABOVE GROUND SURFACE. CONNECTION TO THE MANLINE CONVEYANCE PIPE SHALL BE MADE WITH RESTRAINED JOINTS AS DIRECTED BY THE ENGINEER.
 13. ABOVEGROUND PIPING SHALL BE DRESSED WITH HEAT TRACE AND COVERED WITH MANUFACTURER APPROVED PIPE INSULATION PER THE PROJECT SPECIFICATIONS.
 14. PIPE SUPPORTS AND STANCHIONS SHALL BE FIELD FIT AS REQUIRED TO ADEQUATELY SUPPORT PIPING AND VALVES IN CONFORMANCE WITH THE PROJECT SPECIFICATIONS.
 15. CONCRETE WELLHEAD APRONS, BOLLARDS AND WELLS IS EXISTING.
 16. CONTRACTOR SHALL INSTALL PIPING ALIGNMENT TO THE SECTION ELEVATIONS AS SHOWN.
 17. PRIOR TO EXCAVATION OR CONDUCTING SITE WORK THE CONTRACTOR SHALL CONTACT NEW MEXICO ONE CALL AND MAINTAIN A VALID UTILITY LOCATE CASE FILE AT THE SITE FOR THE PROJECT AT ALL TIMES. CONTRACTOR SHALL COMPLY WITH NEW MEXICO ONE CALL AS PER CHAPTER 82, ARTICLE 14, NMSA 1978.
 18. CONTRACTOR IS NOTIFIED THAT ALL COMPONENTS AND MATERIALS INSTALLED AND/OR USED IN THE WATER DISTRIBUTION SYSTEM SHALL COMPLY WITH NSF 60 AND 61.
 19. ELECTRICAL DESIGN SHALL BE PROVIDED BY OTHERS.
 20. PIPING, VALVES, PUMP AND APPURTENANCES SHALL BE INSTALLED IN CONFORMANCE WITH THE PROJECT SPECIFICATIONS.

MECHANICAL SCHEDULE				
COMPONENT ID	DESCRIPTION	DIA	CONNECTION	MATERIAL / MODEL NO.
1	SILENT CHECK VALVE - GLOBE TYPE	2.5	SC	CAST IRON ASTM A126 GR. B-250 LB CLAPCO
2	MODIFIED LONG RADIUS ELBOW	2.5	W X FL	GALVANIZED SCH. 40 STEEL - MORILL INDUSTRIES 16555 MODIFIED
3	FLEXIBLE COUPLING	2.5 X 12	FL X FL	STAINLESS STEEL TYPE 304 SCH. 40
4	ECCENTRIC RED.	2.5 X 3	FL X W	GALVANIZED SCH. 40 STEEL ASTM A53 GR. B
5	AIR VACUUM VALVE	1/2	SC	CAST IRON ASTM A126 GR. B-250 LB CLAPCO
6	SILENT CHECK VALVE - GLOBE TYPE	3	FL X FL	WILLAMETTE MODEL 141
7	FLOW CONTROL VALVE	3	FL X FL	CAST IRON ASTM A126 GR. B-250 LB CL
8	ECCENTRIC RED.	2.5 X 3	W X W	GALV. STEEL - SCH. 40 ASTM A53 GR. B
9	FLOW METER	2	FL X FL	MICROMETER M1000
10	PRESSURE RELIEF VALVE/SURGE ANTICIPATOR	2 1/2	FL X FL	CL VALVE MODEL 520-G1KC, 150 LB CL DI
11	GATE VALVE	3	FL X FL	BAUKER A-2390, CL 125 CI
12	45 DEGREE ELBOW	3	FL X FL	SS TYPE 304 SCH 40
13	PRESSURE REDUCING VALVE	3	FL X FL	CL VALVE MODEL 506-D1ASK, CL 150 LB DI
14	TEE	3	FL X FL	SS TYPE 304 SCH 40
15	FLEXIBLE COUPLING	3 X 11	FL X FL	SS TYPE 304 SCH 40
16	PRESSURE GAGE/SAMPLE PORT ASSEMBLY	SEE DETAIL 2	SC, FL	SS TYPE 304
17	BLIND FLANGE	3	FL	GALV. STEEL, CL 150 LB SCH 40 ASTM A53 GR. B
18	FLOW CONTROL VALVE ORIFICE	3	FL	SS - CLASS 150 LB (MANUFACTURER PROVIDED)
19	SPRING LOADED CHECK VALVE	3	SC	ORIFICE FOR FLOW CONTROL VALVE
20	90 DEG. ELBOW	3	FL	GALV. STEEL SCH 40 ASTM A53 GR. B

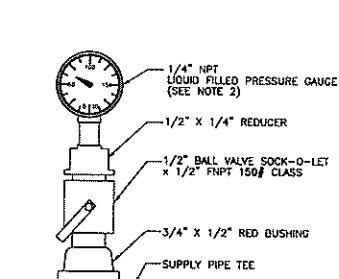
**RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT**

PRODUCTION AND INJECTION WELL PIPING PLANS

DESIGNER	DATE	CHECKED	DATE
MSH	APRIL 2005	MSH	APRIL 2005
DESIGNER	DATE	CHECKED	DATE
MSH	APRIL 2005	MSH	APRIL 2005
DESIGNER	DATE	CHECKED	DATE
MSH	APRIL 2005	MSH	APRIL 2005

SHEET NO. 8 OF 9
DRAWING NO. M-1

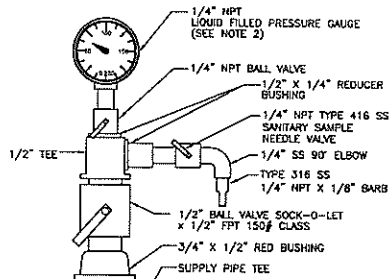
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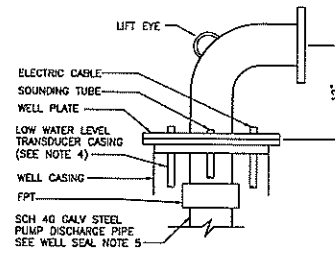
TYPICAL PRESSURE GAUGE ASSEMBLY
DETAIL 1
NOT TO SCALE

GAUGE/SAMPLE PORT NOTES:

1. SEE DIVISION 15 FOR PIPING SPECIALTIES.
2. ALL FITTINGS USED SHALL BE INTERNALLY COATED WITH AN NSF 61 APPROVED COATING.



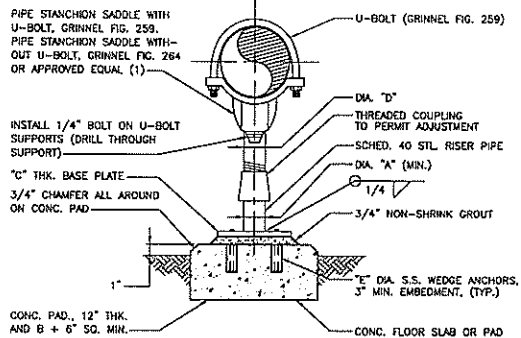
TYPICAL PRESSURE GAUGE/SAMPLE PORT ASSEMBLY
DETAIL 2
NOT TO SCALE



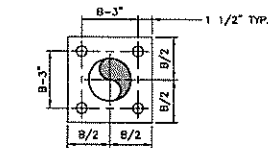
GALVANIZED STEEL WELL SEAL
DETAIL 4
NOT TO SCALE

WELL SEAL NOTES:

1. WELL SEAL SHALL BE COMPRESSION TYPE EQUIVALENT OR APPROVED EQUAL TO MORRILL INDUSTRIES MODEL NG 1595--GALVANIZED STEEL.
2. LIFT EYE SHALL BE CAPABLE OF SUPPORTING WELL PLATE AND FITTINGS ALL LOADS, INCLUDING PIPING, WATER, PUMP, MOTOR AND ASSOCIATED SAFETY AND ELECTRIC CABLES.
3. CASING PROVIDED ONLY FOR PRODUCTION WELL ONLY.
4. PRODUCTION WELL WELL HEAD PLATE SHALL BE EQUIPPED TO RECEIVE A 2 1/2\"/>



TYPICAL PIPE SUPPORT
DETAIL 3
NOT TO SCALE



BASE PLATE						
TYPE	PIPE SIZE	A	B	C	D(2)	E
PS-1	2 1/2", 3", 3 1/2"	2 1/2"	9"	3/8"	1 1/2"	3/8"
OR	4", 6"	3"	10"	3/8"	2 1/2"	3/8"
PS-2	8", 10", 12"	3"	10"	1/2"	2 1/2"	1/2"
	14", 16"	4"	12"	5/8"	3"	1/2"
PS-2	18", 20"	6"	14"	3/4"	3 1/2"	1/2"
	24", 30", 36"	6"	14"	3/4"	4"	1/2"

PIPE SUPPORT NOTES:

1. WHERE LOCATED UNDER FLANGE OR VALVE USE PS2 SUPPORT WITH SADDLE RADIUS TO MATCH FLANGE OR VALVE BODY.
2. FOR PS1 U-BOLT SUPPORTS USE DIMENSION "A" IN LIEU OF "D".

**RANCHO VIEJO DE SANTA FE
AQUIFER STORAGE & RECOVERY PROJECT**

REVISION	DATE	BY	DESCRIPTION

APPROVAL	DATE	OWNER	DATE	REVISION	DATE

MECHANICAL DETAILS

URS

SHEET NO. 9 OF 9
DRAWING NO. M-2

APPENDIX E

PHOTOGRAPHS

RANCHO VIEJO DE SANTA FE

WATER PLAN

PHOTO	DESCRIPTION
DSC02341.JPG	Pumping Well
DSC02344.JPG	Flow Control Valve
DSC02345.JPG	Pumping Well Flow Meter
DSC02346.JPG	Surge Relief Valve
DSC02349.JPG	Injection Well
DSC02350.JPG	Pressure Reducing Valve
DSC02498.JPG	Inject Wellhead with Insulation
DSC02499.JPG	Insulation Close-up
DSC02501.JPG	Insulation Close-up
DSC02502.JPG	CCD-OWA
DSC02504.JPG	CCD-OWB
DSC02506.JPG	CCD-OWC
DSC02517.JPG	Santa Fe Community College Well
DSC02520.JPG	Rancho Viejo Observation Well
DSC02337.JPG	El Rancho Well
DSC02338.JPG	La Cienega Well



DSC02341.JPG
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DSC02344.JPG
8/28/2006 10:57:43 AM



DSC02345.JPG
8/28/2006 10:58:05 AM



DSC02346.JPG
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DSC02349.JPG
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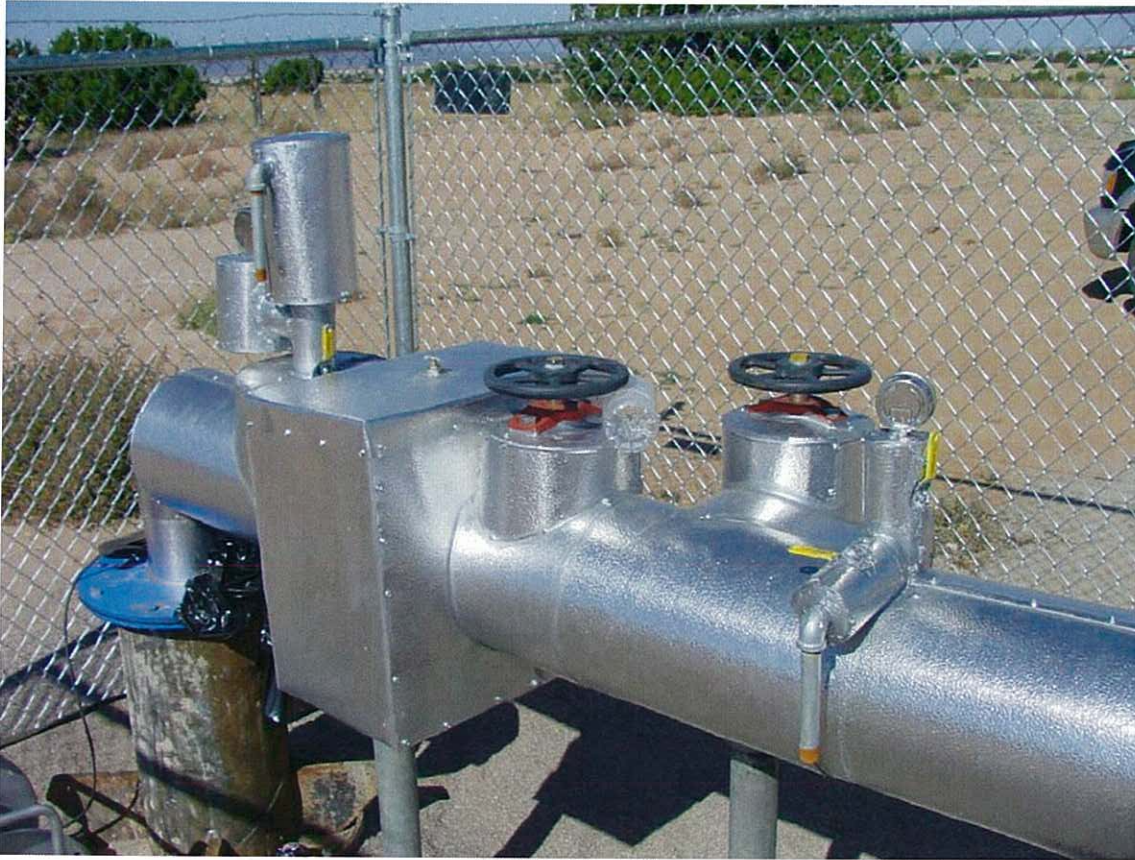
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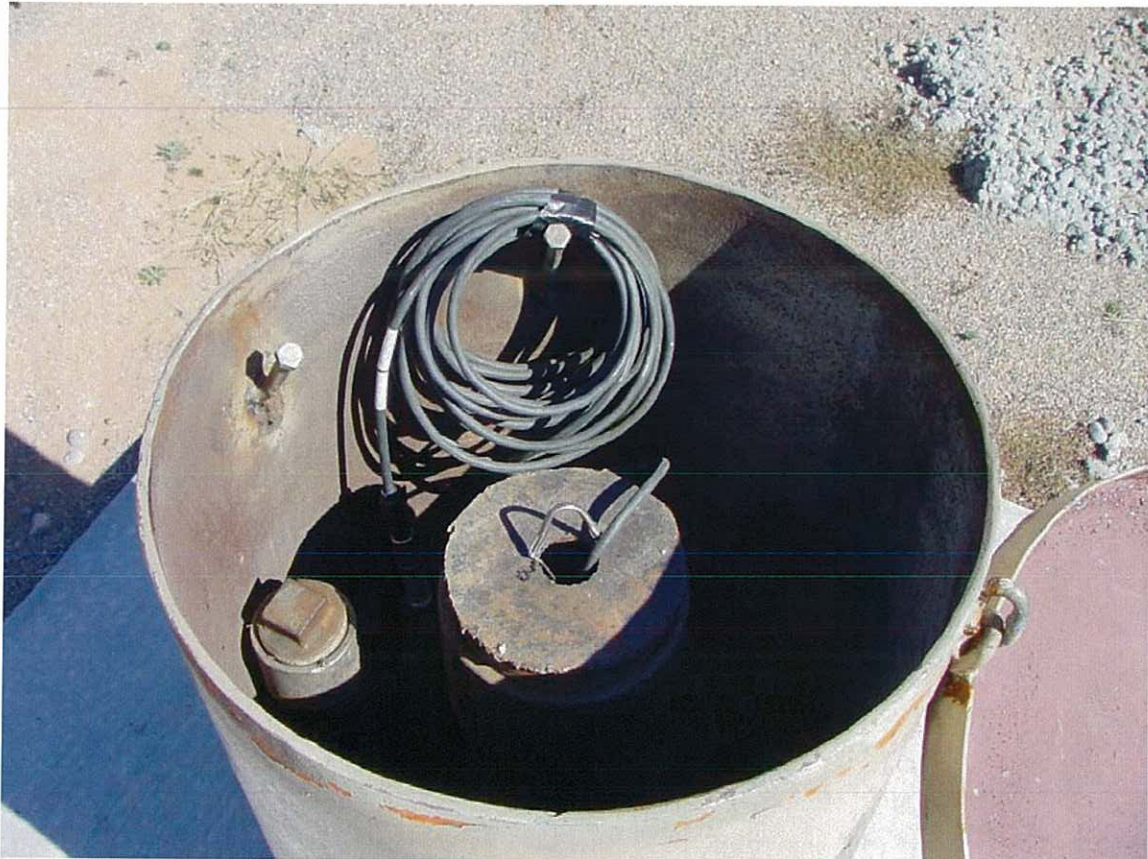
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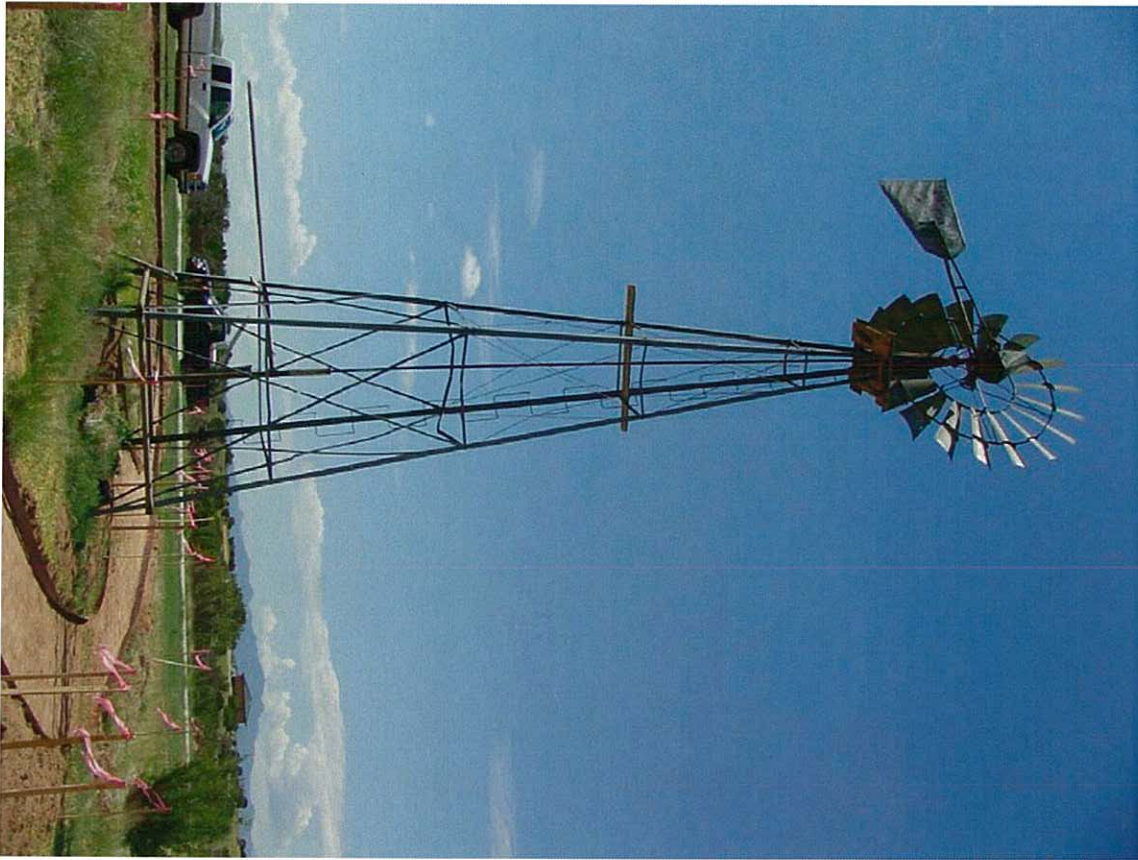
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APPENDIX F

FIELD NOTES AND SHEETS

Rancho Viejo

Apr May 2006 - Aug
2006

Peninsular

FIELD BOOK

50% RAG

64 PAGE

FB 3N2

5/26/06

CWC onsite 0745

inj. wellfield

Download recovery data

Check water levels

ohsite 0855

6/1/06 mtg w/ Comm

Sullivan

Sullivan's well Nija - Driller

4/3/98

~~400~~ Ft deep R6 69393

425 serves 4 houses

300-400 screen

4 1/2 inch csg

DTW 335 (well record)

10-12 gpm

on trib. to Araya Hondo

old truck dam

air in water
pump "shots" off
started when inj well
drilling began

1200 gal tank
↳ pressure tanks

DTW 382.5 ft dtw, just below
top of screen.
pressure → 56 psi
pump came on for ~ 1 min.

6/1/06 CWC onsite
Lij wellfield
Downloading data; measuring
water levels

6/6/06 CWC onsite 14:15
Lij wellfield
Downloading data
Delivered package to Jon Paul.
Set Xducer in CCDPI
offsite 1500

6/19/06 CW and Mick B.

Onsite 11:00

pulling transducers for loggers
to complete wellheads

Solinst 7000 lbs	tape	to (cont.)
0 - 100	100.20	.2
100 - 200	100.15	.35
200 - 300	100.15	.50
300 - 400	100.60	1.00

Offsite 13:15

6/21/06 measured w/ Jeff Watson.

New data on (n) wellfield

OWA shall 2.58' above top Surf csy
Deep (south) 2.62' " "
INT (north) 2.55' " "

OWB 2.92 ft top surf csy to
top protective hsg
5 inch — 0.36 = 2.56
piez — 0.39 = 2.51

OWC 2.50 above top Surf csy
piez 2.21 above " "

73

(n) well not cut down yet

6/28/06 CWC onsite 1400
CED Injection Wellfield

Re-installing transducers.

Can't remove cap from ow-C
~~too~~ shallow piez - let
Self know

offsite 1625

8/10/06 CWC onsite 0830

Setting transducers in
inj well, ow-A shallow,
CED-XI and RV Obs Well.
Checking access to La Granga
and El Rancho wells.
Inspecting pipeline and
valving installation.

□ Arrange for wellhead elev.
survey

Injection well - educator pipe
installed. Piezometers cut to
final height.

CCD-I

M.P. height above surf 15g
inj well sounding tube 2.06 Ft
shallow piez 1.04 Ft
deep ~~shallow~~ piez 0.68 Ft

✗ tape ~~shallow~~ ow-A shallow well
✗ tarp over inj well xducer reel
✗ tape over inj well sounding hole
□ Remind J Watson → Obs C
lid & piez cap

El Rancho Well

213.85 11:38 am Summer 300
access for transducer and
mscope available (need pliers
and wrench to remove plug)
brake on windmill not set,
breeze or wind can activate
pump

□ set brake on windmill

Transducer S/N 316 failed

RV obs well

nearby windmill operating
205.10 ft 15:20 to C
w/ Powers 1000'

Getting to RV obs well

S. on Richards from Rodeo Rd.

wind through ~~Rancho~~ Rancho Viejo

~~231-37~~ SR houses. Just before

AIAT entrance turn left off

Amer Indian
Arch Inst.

rough dirt road. At fence,

turn left. At RR grade

turn right. Go to windmill.

RV obs well is NW of windmill

~ 150 ft

La Cienega well

227-37 toC 16:45 solar 300

well operating

no transducer access

Conner McKinley - when

shutdown wells?

offsite 1700

8/17/06

CWC onsite 10:10

CCD-Pi

213-90

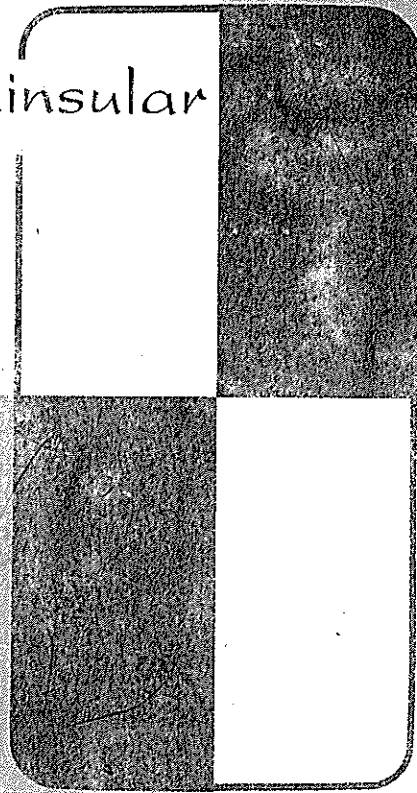
1440

offsite 1630

Rancho Viejo

Aug 2006 -

Peninsular



FIELD BOOK

50% RAG

64 PAGE

FB 3N2

8/23/06 CWC onsite 13:45

CCO-PI
pump has power
All ~~met~~ valves installed
No pressure switch yet
pipe supports not yet
in place.
Transducer set to 1min
Pump started ~ 14:52

CW less flow } FCV
CW more flow }

before FCV
PSI Q
35 11.3
1870 70

off site 16 KC (mi 110)

8/24/06 CWC onsite 10:10

Flushing pipeline
Testing flowmeter.

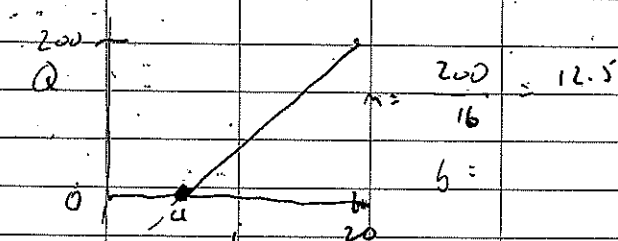
Kerr, Jason and _____
Sam Rodgers assisting

Flow meter

0 gpm @ 4 m

200 gpm @ 20 m

$$Q = 12.5 i - 50$$



Time

Time for water to
travel from CCD-01
to CCD-E1 16 min

Inj flowmeter was stuck -
opened up body and cleared
blockage, works ok

Data loggers reading and storing
flowmeter data.

Using 2 12V batteries to
power flow meter; need 110 VAC
power and transformer to 24 VDC
for 6-mo test.

During pipeline purge
CCDPI flow 100 gpm
CCDFC flow 99 gpm
70 psi upstream
25 psi downstream
of FKV
0 psi (gate
valves open)

Power pipeline purged from
~ 12:15 to 2:45,
chlorine added to CCD-01
about 2:45 pm
CCDPI shut-off @ ~~2:30~~ 3:30

offsite 17:15

mi → 120

Kenny (Rodgers) 280-3733
Jason (Rodgers Plumbing)
203-6122

SFCC Ann Probst 428-1340

Henry McKinley 471-4321

SFCC Frank Joy 428-1225

Jeth Watson 280-0867

Jon Paul Romero 780-0376

Frank Joy cell 690-6509

Rancho Viejo 987, 6921

Sean @ McInerney (451) 652-6811

7/3/07 { Tech Support
office (505) 428-1670

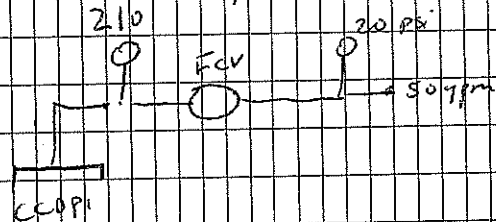
8/25 phone call Jeth w.

- concrete pads/pipe stands are in
- pressure switch is in office
- → will be installed Mon a.m.
- Fencing → 2 car 3 weeks away?
- on temp. fencing up next week
- 110VAC power for both wellheads
- ok for CSD-PI
- issue for CSD-II

8/28/06 CWC onsite 0820
CSD-PI

Starting 6 - no test today

FCV - set to 51 gpm w/
~~no~~ 20 psi downstream,
upstream pressure is 210 psi



Surge relief valve needs inflow
line from system + not installed
at CSD-PI

290 + 70 = 360 ft

Orifice at inj well

300 ft head → ~ 48 gpm

~~200 ft~~

277 ft head ~ 46 gpm

323 ft ~ 50 gpm

expectations

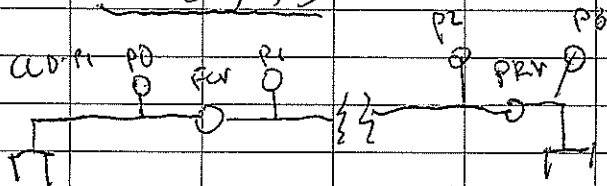
startup → 23 ft head ~ 60 psi
at inj wellhead

CCD-PI wellhead:

downstream pressure gage
wrong - replaced. Now
indicating ~ 50 psi
during pipeline purge
(8 psi @ CCD-11)

Starting head @ inj well
18.25 ft

Pressure gauges



6 mo inj start 15:25

15:28 51 gpm → 12 psi P2

15:29 49 gpm

15:38 45 gpm 16 psi P2

15:55 stopped flow to
inj well w/
gate valves

30 min @ ~ 45-50 gpm
= 1500 gal injected

pressure testing line
overnight

Onsite 1705
110 mi

6/29/06 CW @ onsite 0930
Jett W and
Greg B here

Pipeline passed pressure
check - remained pressurized
@ 100 psi overnight

Draining pipeline @ inj well
(started ~ 9:15)

water is clear during
drainage from pipeline

Elevations

6 ft	CCD PI	6560	83 ft = 56 psi
	Inj	6483	
	air valve	6566	

pipeline drained out ~ 0950
pump on 100 gpm ~ 0955

NOTE: PRESSURE GAGES.
STICK → TAP BEFORE
READING

water arrived ~ 10:05 clear, air
10:10 clear, air
10:12: air out
Steady 100 gpm
water cloudy

10:30 water cloudy

Drop pipe dia 2.5 inch

$$r = 0.104 \text{ ft}$$

$$A = 0.034 \text{ ft}^2$$

$$300 \text{ ft} \times 0.36 = 10 \text{ ft}^3 \times 7.48 \frac{\text{gal}}{\text{ft}^3}$$

$$V = 76 \text{ gal}$$

$$\text{at } \phi = 3 \text{ inch} \rightarrow V = 110 \text{ gal}$$

PRV @ CCD-11

Turn CW to increase
downstream pressure

Turn CCW to increase

range 2-30 psi ~ 3 psi/min

Pre-set @ 10 psi C.S. pressure

speed adj - CW to make
valve close
slower

Start @ 11:00

	PO	PI	P2	P3	F1	F2
10:50	80	55	0	0	100	100

10:52 M1 = 66000
M2 = 37700 } 100 gpm
*estimate @ 11:00

Time	PO	PI	P2	P3	F1	F2
11:02		100	84	8	92	43
11:05	adjust	Flow @	CCD PI	pump	start	
11:10	220	70	42	18	50	17

water clear

Adjust PRV to read 30 psi.
~~do~~ @ P3 @ ~ 11:15

	P0	P1	F1	P2	P3	F2
1117	220	52	55 gpm	47	31	49

FCV was stuck, Kerry
 fixed @ ~ 11:30

1132	220	38	50	74	31	49
------	-----	----	----	----	----	----

→ TR lead rise
 water clear

1145	220	38	51	74	30	49
------	-----	----	----	----	----	----

1210 shutting down → FCV
 failing,
 m1 = 71500
 m2 = 42400

1405 opened valve
 @. m1 well

Pump on
 purging well / line for inject
 startup

— START G-MO TEST —

1500 Initiating injection
 vacuum on air relief
 10 psi on P2
 2 min for
 prep pipe to A11

	P0	P1	F1	P2	P3	F2
1505 ~	220	20	50	26	20	50

FCV & CCD-11 opened

1514	215	70	54	50	29	51
------	-----	----	----	----	----	----

Backed adj of PRV to P3 = 25
 NO Δ in flow

1520	220	85	51	75	25	51
------	-----	----	----	----	----	----

✓ Rodgers → replace P2
 drill hole for air relief
 in CCD-11

1544	215	65	51	70	25	51
------	-----	----	----	----	----	----

Need:

- hole in CCD-11 assy
- locks for gate / gate ✓
- 24V DC power (loggers)

off site 1600

m1 120

8/30/06

CWC Onsite 10:45

6-mo Inj test
underway

10:50 Inj well

F2 50 gpm

P2 56 psi

P3 24 psi

water → clear - bubbles?

11:05 Prod well

P0 215 psi

P1 36 psi

F1 51-52 gpm

water clear, few bubbles

NO evidence of surge

valve release

CCDP1 Drawdown = ~40 ft

CCDX1 " = ~22 ft

Use to calculate

back

pretest

totalizer

11:30 F1 totalizer = 140900

11:50 F2 totalizer = 110900

Set CCDP1 CCDX1 transducers to

log 1 hr

Set F1 datalogger to log half hour

Note - fence builders on site -
using some water from sample
port to mix concrete -

El Rancho valves OK

Did not check Air obs well

Inj well mounding = 25 ft

12:05 F2 = 50

P2 = 63

P3 = 24

Set F2 logger to 1/2 hour

Set CCD-F1 & obs well

transducers to 1 hr

offsite 1245

Jason 14:30 8/31/06

P0 215 psi

P1 62 psi

F1 flow 49-50 gpm

P2 71 psi

P3 22 psi

F2 49 gpm

9/1/06

Henry McKinley
will shut down La Cienega
well in early Oct

9/1/06 CWC on site 11:30

CCD-P1

PO 215 psi

P1 64 psi

F1 48 ~~gpm~~ -49 gpm (P1 ^{fluctuating} briefly to

water clear, bubble free 50 gpm)

no evidence of surge valve
discharge

F1 totalizer 287200

CCD-P1 drawdown ~ 45 ft

Flow Datalogger battery 25.92 V

CCD-II

F2 49 GPM

P2 74 psi

P3 24 psi

Buildup in CCD-II 39 ft

water clear, no bubbles

Flow logger battery 25.87 V

□ measure all WL

□ Call Frank Fox SFCL → check well

□ fix Solinst SDP

office □ Plot inj well temp

□ RV obs well

□ El Rancho well

~~□~~ RV obs well

Cow knocked over
transducer cable reel.

Transducer & cable ok

El Rancho well

transducer and cable ok

14:50 CCD-P1

PO 215 psi

F1 48 -49 gpm

P1 53 psi

1500 Air relief near Richards/

Avenida del Sur is wet,

wet soil below ~~area~~

Get into "manhole"

15:05 CCD-E1

F2 ^{48 gm} 49 gpm

P2 60 psi

P3 24 psi

15:07 Increased P3 to 28 psi

w/ PRV.

F2 stable @ 49 gpm

P2 dropped to 54 psi

15:15 CCD-P1

F1 49 gpm

P1 36 psi

P0 215 psi

~~50~~ 48-50
fluctuating

16:05 CCD-P1

F1 49-51 gpm

P1 40 psi

P0 215 psi

water "fizzy" but clear

16:12 CCD-21

P2 47 psi

P3 28 psi

F2 49 gpm

Water fizzy, but clear

Offsite 1620

7/5/06
Wed

CWC onsite 09:30

CCD-I1

P2 15 psi

P3 28 psi

F2 48 gpm Tor = 529600

Water clear - no bubbles,

no color

CCD-E1 buildup 50 ft

CCD-P1 09:50

P0 210-215

P1 65-66

F1 50 gpm (fluct. to 49)

Surge relief has discharged

water "fizzy".

CCD-P1 drawdown ~ 50 ft

10:05 second sample - water clear,

no "fizz"

10:05 analyzer 572400

Flow logger bat 25.5V

Rodgers i Co observations

Saturday 9/2/06 11:00

PD 210

P1 100

F1 51 gpm 356800 gal

Surge valve discharging (trickle)

P2 100+

P3 30

F2 49 323000 gal

~~Monday 9/4/06~~

Tues 9/5/06 06:30

PD 210

P1 100

P2 100+

P3 29-30 psi

surge valve trickling

CCD-P1 13:00

PD 210-215 psi

P1 65 psi

F1 48-49 gpm

230.87 ft 13:15

SFCC well

"SFCC Grounds Supervisor"

Manuel Gomez

→ 670-3218

Gilbert

920-6777 cell

I left Solimer 300 in

SFCC cell for future

measurements

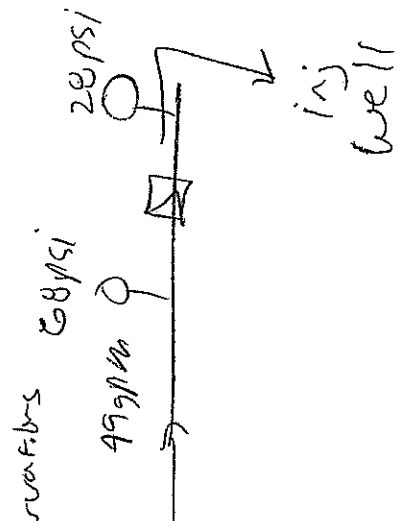
CCD-II 13:25

F2 48-49 gpm

P2 72 psi

P3 28 psi

offsite 13:30



Sunday 5pm
Sept 3 2006

9/8/06

CWC Onsite 0935

CCD-21

F2 48 LPM 740500 gal

P2 > 100 psi

P3 28 psi

Water clear, no fizz

~~no~~ roll sol meter STD

meas. all water levels

STCC - contact, measure

dry check sheet

lower CCD 11 reduce to > 330

~~no~~ PRV spring

CCD-P1 09:55

P0 210 psi

P1 100 psi

F1 53 gpm 791900 gal

Surge valve dumping

~ 3 gpm

CCD-1

W.D. changed PRV getting to 32 psi

(one full turn CW)

F2 → 49 gpm

PZ still > 100 psi

10:06 1 turn CW PRV

PZ to 35 psi

FZ to 49 gpm

1 more turn

PZ to 38 psi

FZ to 50 gpm

P1 still > 100 psi

CCD-I1 buildup ~ 54 ft

mtg w/ SP Romero

□ enclosures?

□ solar panel ← Phil → solar

□ JLF - 1:00

□ PRV spring

□ Frost

→ Thermostat + solar

→ SP ok pressure reducer

□ Check budget; redo

□ Send charts

Jason and Marcus

on site ~ 12:45

Adjusted FZ to 1/4 turn CCW

to reduce flow

(was flowing near 55 gpm

when Jason got on site)

3:00

PD 210 Fluctuating

P1 56

F1 52-53 gpm

13:02 3/4 turn CCW on FZ

F1 to 50-49 gpm

PD - 210

P1 - 36 psi, dropped

to ~ 20 psi in couple
of minutes

13:15 CCD-I1

PZ 29

P3 22

FZ 47

Jason swapping spring in PRV
to red (15-25 psi)

No problems

1330

PO 210-212 psi

PI 19 psi

FI 51 gpm

14:45

PO 210 psi

PI 8 psi

FI 45 gpm

increase flow e FCV to 48-49 gpm
(turned about 1/2 turn)

1500 Pressure building
FI jumped to 53 gpm
with no adjustment
PI up to 20

CCD-PI

303.82 sol 500

127.11 reduce

230.93

1510 - 1/2 turn CCW

at FCV, FI → 50 gpm

PI → 22 psi

15:30 PO = 210

PI = 20 psi

FI = 50-51 gpm

15:50 same as above

16:10 FZ 48 gpm

PZ 30 psi

PB 24 psi

CCD-PI

water clear, no hicc

16:50 CCD-PI

PZ 30 psi

PB 24 psi

FZ 47 gpm

16:57 CCD-PI

PO 210

PI 20 psi

FI 51 gpm

conclusion:

FCV is operating wrong
and/or flow meter FI
is operating wrong

off site 17:15

9/11/06

Jason had to shut down
this morning to troubleshoot.

F1 - 51 steady

F2 - 50 steady

~~re-located~~ ~~and~~ ~~re-located~~
re-oriented orifice so sensing part
is on side instead of on
bottom

Flushed system as before
now operating at 450 gpm

F1 - 51 gpm steady

F2 - 50 gpm steady

9/12/06 CWC i Mink B
Onsite 10:20

F1 51 gpm 1072300 gal

P0 210 psi

P1 43 psi

water hazy

Flow ~~logger~~ battery 25.01V

11:30

F2 51 gpm 1016200 gal

P2 51 psi

P3 44 psi

water slightly hazy

air in sight gage of
FRV - cleared out w/
valve. Did not affect
settings

Flow logger battery 25.02V

(open collector 228.40
SFLL) 13:15

13:50 CCD-F1

F2 50-51 gpm

P2 48 psi

P3 45 psi

Onsite 14:00

SF
LL | 13:07 229.50

9/12 phancon of Seth W.

- Insulating sleeves should be done mid-next week
- B Electric - 110V power @ CCD-P1 end of week
- CCD-P2 - 12V system for hear tape is better for solar power.

R.V. in

8am 9-13-06

F2 = 51 gpm P2 = 51 psi US
1080,000 P3 = 46 " ds

9/26

R.V. SFCC: 230
1558 = 175
2023,25

10/4/06 CWC Onsite 1620

CCD P1 wellfield

- Prod well flowmeter batteries
- meas Prod well WL
- Check CCD-X1 xducer
- " RV OW "

P0 209 psi

P1 46-47 psi

F1 = ~~51~~ gpm 2737700

DTH 514.20 ft CCDP1

a 16:40

CCD-X1 Transducer ok -

communicated w/ newer cable

(note - could not engage connector cable fully on Xducer cable side)

RV obs well

transducer ok

• ~~needs new dominant Cap~~

• ~~CCD-X1 Xducer needs new batteries~~

10/10/06 RU.

SFC

15 28. 228.54

10/24 230.30

1455- 2.91

10/26/06 CWC - onsite 10:30

CCD - P1 site

w/ Kerry from Rodgers

PO - ~~4379800~~ 4379800

PI - 72 psi

F1 - 53 gpm 4379800

Kerry adjusting rate w/
FCV $\frac{1}{2}$ turn

~ 10:45

PI 48 psi

F1 ~~49~~ 49-50 gpm

La Cienega well

Kerry rotated well to improve access

DTW 225.50 to P Plate

Power 500

hangs up a little e ~ 100 ft

Kerry can jack well, move
over a little to eliminate
the catching point need
to get Rancher's
permission first.

11:20 F1 = 50-51 gpm

PI = 46 psi

PD = 105 psi

CCD - P1

F2 = 50 gpm

P2 54 psi

P3 47 psi

offsite 11:40

10/27/06

Mike - Dwan Plumbing -

F1 - 50 gpm

F2 - 49 gpm

10/31

SFC well

1327 227.30

11/14/06

RVS FCC well

226.81 @ 1253

12/27/06 CWC Onsite 0930

Rancho Viejo

measuring water levels, downloading
transducers. Injection test
going ~ 4 1/2 months.

No field visit last week
due to weather.

E/Rancho 214.03 ft

SFCC 226.59

off site 15:45

226.69 - CFCC @ 1412

1/10/07

CWC Onsite 0730

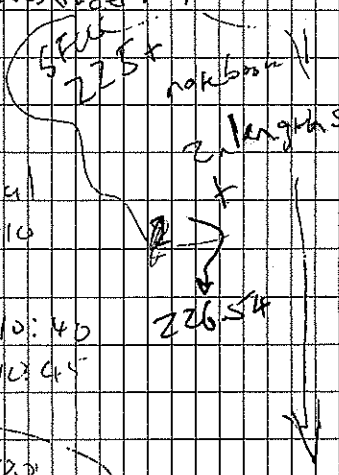
Rancho Viejo pumping/
injection well fields

- measuring water levels
- downloading transducers &
loggers

CWPAI 2411 ✓
9906200 gal
318.12 @ 8:10

DWB 282.74 10:40
piez 290.19 10:45

Offsite 12:00
m. 110



2/26/07 CWC and MB
Onsite 11:30
Prepping for shutdown tomorrow

1350 RV obs 204⁺ -
= _____
on Powers 500 kPa
windmill brake
engaged

samples pulled @
COP1 @ ~1330

COP1
conductivity 19° 225 μ mhos/cm

Offsite 1500

2/27/07
CWC & MB
Onsite 0830
Injection 6-m
rest shutdown
today

10:00 inject flowmeter
2684600

CWB sk pier
288.71 @ 10:21

Ran ~~to~~ Detamore
690-5247

Final flowmeter (pumping)
13361600

RV obs 203.97 kPa (Powers)
@ 11:29
windmill ~~brake~~ brake engaged

CWB sk pier
288.66 @ 1154

Offsite 15:30

2/29/07

el Rancho 213.97 @ 11:49

CC 12:25 226.47

3/2/07

CWC onsite 0740

offsite measuring well's
downloading xducers

offsite 0850

115 mi

3/6/07 rwc onsite 13:30
CCD wells

offsite 1645
100 mi

3/13/07

CWC onsite 1400

CCD wellfield

meas well's

reset xducers to 4 hrs

move deep OW to RW obs

offsite 1645

120 mi

3/30/07

CWC onsite 0900

Dawson Survey (Dennis)

surveying wellhead KY and
elevation.

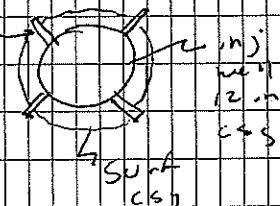
mj well head not

complete - surveying

~~offsite top of each CCS~~

top of Am on NW side

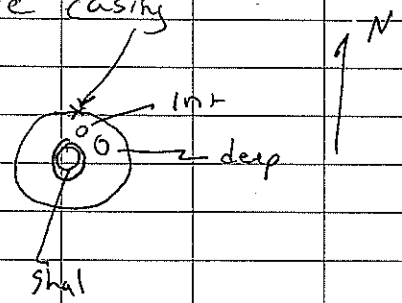
side



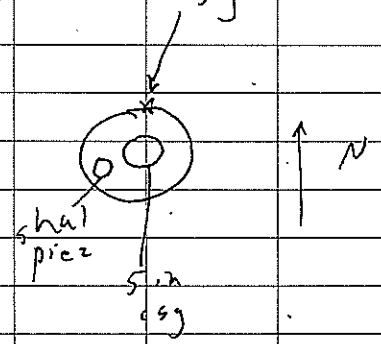
NOTE: Transducer
time is NOT
adjusted for DST
(1 hr earlier than
actual time)

CCD-06

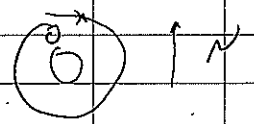
~~066~~ A Survey pt
N. side top of
protective casing



CCD-06B - Survey pt
N. side top of
protective casing

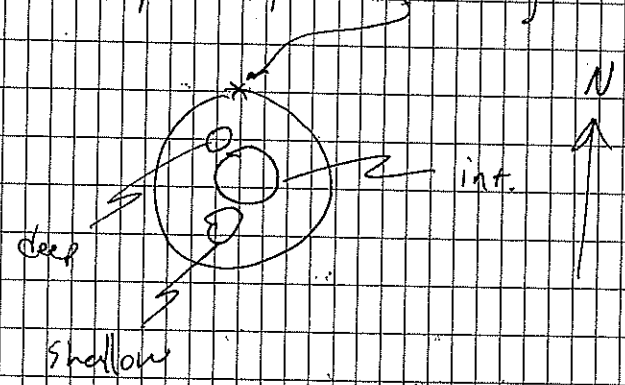


CCD-06C Survey pt
N side top of
protective casing



CCD-X1

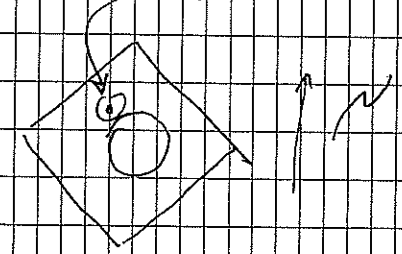
Survey pt. top N side
top of protective casing



X1 S 237.80 10.56
X1 D 234.17

CCD-P1

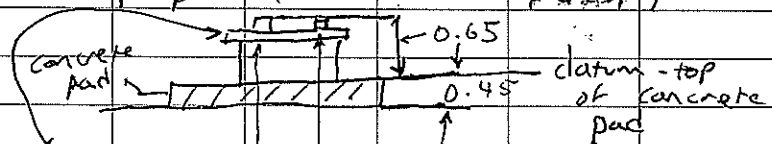
NW side of
well casing on
concrete pad



SPCC 226.41 11:06

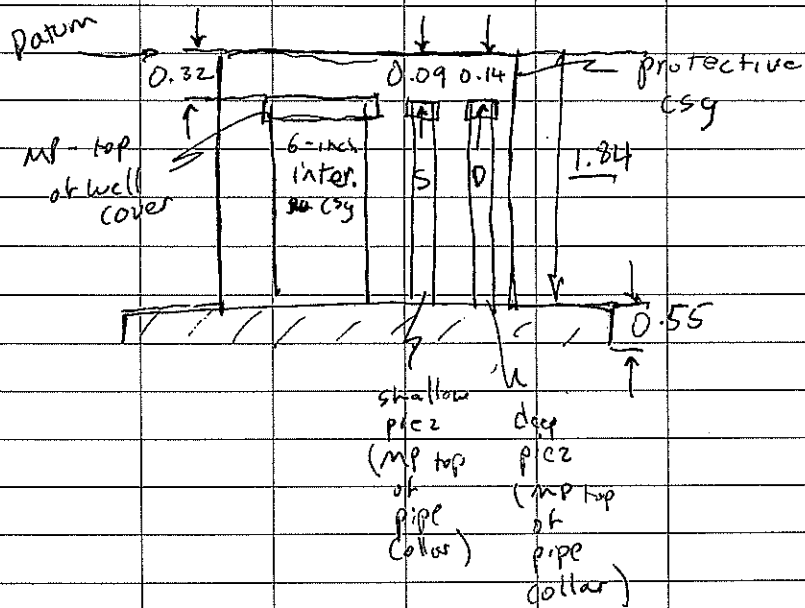
3/30/07
 M.P. Offset from Datum (all units = ft)

CCD-P1 (Temporary configuration w/
 pump installation for 6-mo test)

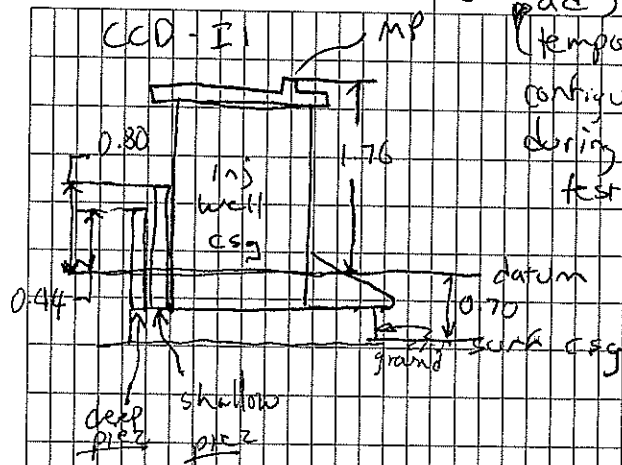


temporary
 cover for
 pump
 instal.
 microscope
 port
 Xducer
 port

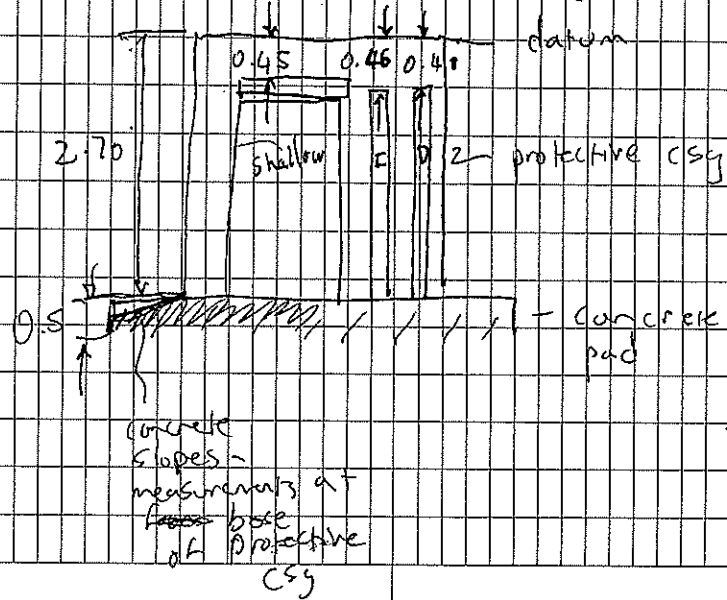
CCD-X1 (permanent configuration)

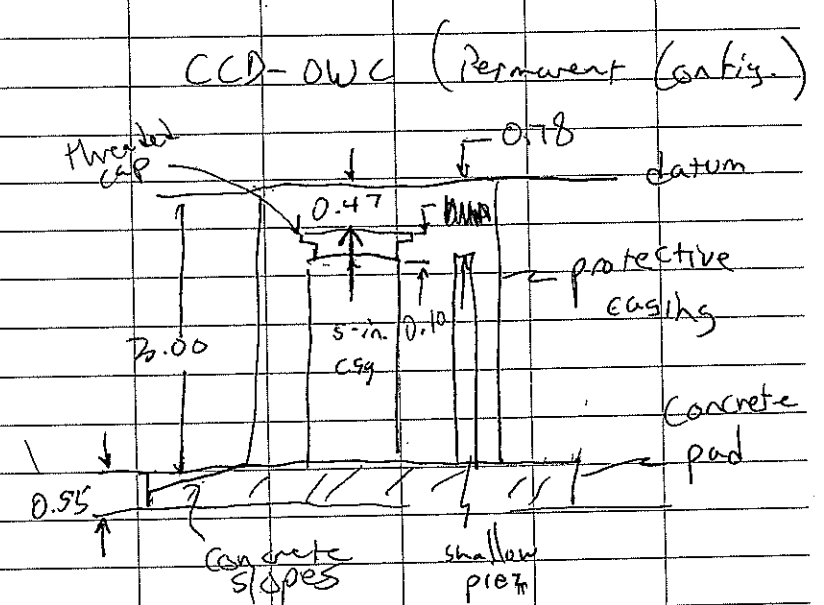
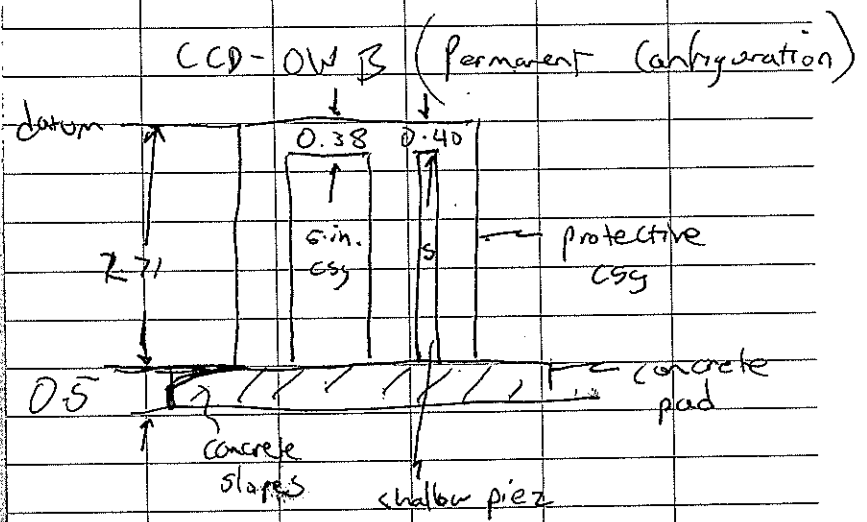


(no concrete pad)
 (temporary configuration during 6-mo test)



CCD-OWA (permanent configuration)





Offsite
3:30

4/18/07 CWC onsite 1550
inj tes + recovery
measurements / down loads

SFCe well _____ ft
could not open lock - Cambio
change?
Cross locks watered, soil damage
well probably in use.
Solinst 500

CCD-7II
shallow 315.73 ft 1600
deep 288.02 ft 1605

Changed all clocks
to daylight savings
(1 hr forward)

OWA shal 289.03 ft 16:10

OWB shallow piez 292.35 16:20

OWC sh piez 236.36 16:30

CCDX1 sh piez 236.65 16:50

CCDX1 deep piez 234.15 16:55

offsite 17:00

Vresjo

- All WL's
- pull RW obs reducer ✓
set in CCD-PI ✓
- pull BGW reducers, return ✓
to office
- Get 300' solinst SFCC ✓

5/25/07

CWC onsite 0900

checking water levels, downloading
transducers.

~~OWA~~ CWC

CCD-PI 236.41 ft @ 10:00

pulling BGW reducer

El Rancho well - brake off,

pumping - No more observations.

offsite 13:30

mi 120

7/3/07

- 1115 - BGW on-site (Mick & Bill) at injection well
- 1330 - Downloaded all reducers and measured water levels. Never could get hold of Frank Joy, left 2nd message.
- 1345 - Called Manuel Gomez (SECC Grounds Sup.) left message. No answer on the number for Gilbert.
- 1350 - BGW off-site

Jyl

* Frank Joy returned call @ 1425. He said that Manuel Gomez should be the contact for access, and we can always call the office for help ---

505-428-1670

670-3218

9/19/07

- 1350 - BJ on-site to download reducers and measure fluid levels. Called Manuel Gomez (SECC), he will come to unlock SECC well.
- 1410 - Retrieved 300' Solinst
- 1600 - Measured fluid levels and collected reducer data BGW off-site
- ~~Replaced dessicant at injection well~~

COPY^{06/0888}

FILE

FAX FROM

RICH DURAN PLUMBING AND HEATING , INC.

17 B PASEO DEL ORO

SANTA FE , NM 87506

505-992-0308

505-992-0283 FAX

DATE 9-28-06

NUMBER OF PAGES 2/4

TO Durham Valleau Ground water

FROM Rich Duran P&H 412-1284-

RE ~~Wells~~ Rancho Viedo Wells

MESSAGE _____

OCT-1

Rancho Viejo Pump and Inject System Daily Check List													Comments	Initials
Date	Time	Pumping Well					Injection Well							
		P0	P1	F1 (gpm)	F1 (gal)	Water Quality	P2	P3	F2 (gpm)	F2 (gal)	Water Quality			
10-21-06	7:47	210	75	53	3981700	F:22y	80	71	54	3878600	Clear			
10-21-06	5:15	210	75	53	4015200	F:22y	80	71	54	3928500	Clear			
10-22-06	8:30	200	76	53	4064900	F:22y	80	70	54	3978400	F:22y			
10-22-06	4:00	210	74	53	4088400	F:22y	79	72	54	4002700	Clear			
10-23-06	4:30	200	75	53	4116700	F:22y	79	71	54	4034200	Clear			
10-24-06														
10-25-06	4:00	200	72	53	424200	F:22y	71	71	54	4159800	Clear			
10-25-06	7:30	200	72	53	4297800	F:22y	79	71	54	4212400	Clear			
10-25-06	4:00	200	72	53	4319800	F:22y	79	71	54	4238300	F:22y to clear			
10-26-06	7:30	200	72	53	4370500	F:22y	79	70	54	4290200	Clear			
10-26	4:30	210	49	50	4396100	F:22y to clear	54	49	50	4314600	Clear			
10-27-06	7:30	210	40	50	44444500	F:22y to clear	49	40	49	4363800	Clear			

Normal Ranges:

- F1 and F2 - 49 to 51 gpm
- P0 - 200 to 215 psi
- P1 and P2 - 30 to 90 psi
- P3 - 30 to 70 psi

Emergency Contacts:

- Jon Paul Romera work (505) 983-6821 cell (505) 780-0376
- Jeff Watson work (505) 677-1030 cell (505) 280-0867
- Casoy/Cooli work (505) 247-2000 cell (505) 252-0150

Rancho Viejo Pump and Inject System Daily Check List

Date	Time	Pumping Well					Injection Well					Comments	Initials
		P0	P1	F1 (gpm)	F1 (psi)	Water Quality	P2	P3	F2 (gpm)	F2 (psi)	Water Quality		
10-6-06	8:15	218	50	52	2861900	FIZZY TO CLEAR	56	50	51	2781400	CLEAR		
10-6-06	7:26	210	51	52	2896700	CLEAR	60	51	51	2816100	CLEAR	NO (P0) GAUGE RECAL	HL
10-7-06	8:30	210	51	52	2939100	FIZZY TO CLEAR	60	52	51	2857600	CLEAR		
10-7-06	4:00	210	43	51	2959600	FIZZY TO CLEAR	51	45	50	2877900	CLEAR	P1 GPM CHANGES FROM 50 TO 51 GPM	
10-8-06	8:30	208	44	51	3012900	" "	52	46	50	2929300	CLEAR		
10-8-06	4:15	209	52	51	3075800	" "	58	52	51	2952100	CLEAR		
10-9-06	7:00	210	50	51	3088500	" "	56	50	51	3005100	CLEAR	F2 GPM CHANGES FROM 50 TO 51 GPM	
10-9-06	5:00	210	53	51	3113800	" "	60	54	51	3029500	FIZZY TO CLEAR		
10-10-06	7:40	210	53	51	3159400	" "	61	54	51	3075200	CLEAR		
10-10-06	5:20	210	43	50	3189800	" "	59	41	50	3105300	CLEAR		
10-11-06	7:30	210	43	50	3232800	" "	51	41	50	3140600	FIZZY TO CLEAR		
10-11-06	6:45	210	50	51	3267900	" "	58	50	51	3182000	CLEAR		
10-12-06	8:15	210	48	51	3309000	" "	53	49	50	3223500	CLEAR		
10-12-06	6:30	210	48	50	3340900	" "	53	49	50	3254900	CLEAR		
10-13-06	10:00	210	51	51	3393000	" "	59	51	51	3306900	CLEAR		
10-13-06	6:30	210	51	51	3415100	" "	60	52	51	3328000	CLEAR		
10-14-06	7:00	210	51	51	3454100	" "	60	51	51	3366600	CLEAR		
10-14-06	4:00	210	51	51	3482600	" "	59	50	51	3394800	CLEAR		
10-15-06	8:30	209	48	51	3513800	" "	48	50	50	3445700	CLEAR		
10-15-06	4:30	208	50	51	3536700	" "	56	48	50	3445700	FIZZY TO CLEAR		BG
10-16-06	7:30	209	48	51	3610300	" "	54	49	51	3522200	" "		BG
10-16-06	5:20	210	48	51	3637800	" "	54	47	51	3550400	" "		
10-17-06	8:30	210	47	51	3680000	" "	55	49	50	3591900	" "		
10-17-06	5:30	210	50	52	3710700	" "	62	42	50	3720900	" "		
10-18-06	8:00	210	50	52	3764500	" "	58	50	50	3669700	CLEAR	(SPIKE TO B2 PSE) CALLED BOB	
10-18-06	6:16	209	75	53	3787200	FIZZY	80	71	54	3696300	FIZZY	TALK WITH JEFF.	
10-19-06	7:30	209	75	53	3826600	FIZZY	80	71	54	3740700	FIZZY	SPIKE P2 & P3 GPM AT 54 SPIKE ON P1	
10-19-06	6:21	209	75	53	3862000	FIZZY	79	71	54	3773500	FIZZY		
10-20-06	9:15	209	75	53	3912900	FIZZY	80	71	54	3825100	FIZZY		
10-20-06	5:15	209	75	53	3963800	FIZZY	80	71	54	3877100	FIZZY		

FAX

Normal Ranges
 F1 and F2 - 48 to 51 gpm
 P0 - 200 to 215 psi
 P1 and P2 - 30 to 50 psi
 P3 - 30 to 70 psi

Emergency Contacts
 Jon Paul Romero work (505) 883-8921 cell (505) 790-0376
 Jeff Watson work (505) 877-1000 cell (505) 280-0867
 Casey Cook work (505) 247-2000 cell (505) 252-0150

Date	Time	Pumping Well					Injection Well					Comments	Initials
		P0	P1	F1 (gpm)	F1 (psi)	Water Quality	P2	P3	F2 (gpm)	F2 (psi)	Water Quality		
9-21-06	8:40	209	54	53	170600	FIZZY TO CLEAR	60	54	52	176400	CLEAR		
9-21-06	8:28	210	45	51	1768700	FIZZY TO CLEAR	54	49	50	1700800	FIZZY		RD
9-22-06	8:04	210	48	52	1806100	FIZZY	54	49	51	1738500	FIZZY		RD
9-22-06	6:38	210	50	52	1837000	FIZZY TO CLEAR	58	50	51	1770700	FIZZY TO CLEAR		ML
9-23-06	7:45	210	50	52	1886900	FIZZY	55	50	51	1811200	FIZZY TO CLEAR		ML
9-24-06	4:15	210	49	52	1904400	FIZZY	55	50	51	1835100	FIZZY TO CLEAR		ML
9-24-06	1:55	209	48	51	1975400	CLEAR	55	50	51	190500	FIZZY TO CLEAR		ML
9-24-06	7:20	209	50	52	1992400	CLEAR	56	50	51	1921600	FIZZY TO CLEAR		ML
9-25-06	7:37	209	50	52	2031100	FIZZY TO CLEAR	56	50	51	1957700	CLEAR		ML
9-25-06	7:54	209	49	52	2070100	CLEAR	56	50	51	1997200	CLEAR		ML
9-26-06	7:43	209	50	52	2106700	FIZZY TO CLEAR	56	51	51	2034300	CLEAR		ML
9-26-06	6:23	209	51	52	2140500	FIZZY	54	52	51	2067300	CLEAR	Meter Changes From 52 To 53 GPM	ML
9-27-06	7:29	210	51	52	2182000	FIZZY TO CLEAR	60	51	51	2117800	CLEAR	" " " " 51 TO 52 GPM	ML
9-27-06	7:45	210	51	52	2221500	FIZZY	58	49	51	2146900	CLEAR		ML
9-28-06	8:34	210	51	52	2261500	FIZZY TO CLEAR	59	51	51	2180800	CLEAR		ML
9-28-06	6:38	209	51	52	2292900	FIZZY TO CLEAR	59	51	51	2217500	CLEAR		ML
9-28-06	8:00	210	51	52	2335100	FIZZY TO CLEAR	59	51	51	2259200	CLEAR		ML
9-29-06	7:21	209	51	52	2377400	FIZZY TO CLEAR	59	51	51	2294100	CLEAR		ML
9-30-06	8:47	210	50	52	2412900	FIZZY TO CLEAR	56	50	51	2335800	CLEAR		ML
9-30-06	4:13	209	49	51	2437700	FIZZY TO CLEAR	52	49	51	2360200	CLEAR		ML
10-1-06	7:22	209	49	52	2484200	FIZZY TO CLEAR	55	50	51	2409300	CLEAR		ML
10-1-06		207	48	52	2516800	FIZZY TO CLEAR	55	50	51	2381600	CLEAR		ML
10-2-06	7:54	209	67	53	2560700	FIZZY TO CLEAR	70	62	53	2491600	CLEAR		ML
10-2-06	6:40	208	65	53	2594800	FIZZY TO CLEAR	66	60	55	2515500	CLEAR	GPM Spike To 55 GPM	ML
10-3-06	7:39	209	51	52	2635700	FIZZY	59	51	51	2556900	CLEAR		ML
10-3-06	4:45	209	42	51	2663700	FIZZY TO CLEAR	51	49	50	2584400	CLEAR		ML
10-4-06	7:43	210	50	52	2711000	CLEAR	58	50	51	2631200	CLEAR		ML
10-4-06	6:28	210	48	51	2744600	FIZZY TO CLEAR	55	50	51	2663700	CLEAR		ML
10-5-06	8:02	210	48	51	2786300	FIZZY TO CLEAR	57	49	50	2705600	CLEAR		ML
10-5-06	7	210	46	51	2815100	FIZZY TO CLEAR	52	49	50	2734200	CLEAR		ML

Normal Ranges
 F1 and F2 - 40 to 51 gpm
 P0 - 200 to 215 psi
 P1 and P2 - 30 to 80 psi
 P3 - 30 to 70 psi

Emergency Contacts
 John Peter Romero work (505) 983-6921 cell (505) 780-0376
 Jeff Watson work (505) 877-1030 cell (505) 280-0867
 Casey Cook work (505) 247-2000 cell (505) 252-0150

Field Checklists

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date:	Observed	by:	Observation
9/19/06		MICK	
Production Well	CCD-Prod 1:	Time	
	Flow-1 GPM:	10:56	fluctuation bet 51 & 52 every 3-4 secs
	Flow-1 Total:	10:56	1599500 gal
	Pressure-0	10:57	209 psi
	Pressure-1	10:59	44 psi
	Battery VDC		24.40
	Seal Batt. Box		✓
	Water Quality		fizzy / clear
	Laptop ELOG		✓
	Download to handheld (old cable)		✓
	CCD-Expl 1:	12:35	243.49 Shallow
	Piezometer water levels (2)	12:39	233.45 Deep
	Download to handheld (old cable)		✓
Injection Well	Air purged	11:37	✓
	Flow-2 GPM:	11:40	51 gpm
	Flow-2 Total:	"	1537300 gal
	Pressure-2		51 psi
	Pressure-3		46 psi
	Battery VDC		24.46
	Seal Batt. Box		✓
	Water Quality		fizzy / clear
	Laptop ELOG		✓
	Downloads to handheld (P5)		✓
	Piezometer water levels (2) Shallow	11:52	230.00 Deep
	Deep	11:55	315.98 Shallow
Observation Well	OW-A:		
	Download to handheld (P5) (3)		✓
	OW-B:		
	Download		✓
	Piezometer water level	14:07	290.3
	OW-C:		
	Download ✓	14:18	236.59 ↗
	Piezometer water level		↘
El Rancho Well	Piezometer water level	12:54	214.03
SFCC Well	Piezometer water level	13:27	229.50
La Cienega Well	(Future)		

purge on prod. well?

↳ unable to connect handheld.

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 9/26/06	Observed by: M.L.K.	Time	Observation
Production Well			
CCD-Prod 1:			
Flow-1 GPM:		1354	52 gpm
Flow-1 Total:		"	2126400 gal
Pressure-0		1355	206 psi
Pressure-1		"	49 psi
Battery VDC		1353	23.90
Seal Batt. Box		✓	
Water Quality			slightly fizzy
Laptop ELOG		1351	
Download to handheld (old cable, P4)		✓	
CCD-Expl 1:			
Piezometer water levels (2) Shallow:		1409	243.96
Deep:		1407	233.45
Download to handheld (old cable, P4)		✓	
Injection Well			
Air purged		✓	
Flow-2 GPM:		1250	51 gpm
Flow-2 Total:		1250	2049800 gal
Pressure-2		1249	56 psi
Pressure-3		1249	51 psi
Battery VDC		1246	22.89
Seal Batt. Box		✓	
Water Quality			tiny bubbles / fizzy
Laptop ELOG		1242	
Downloads to handheld (P5)		✓	
Piezometer water levels (2) Shallow:		1301	315.96
Deep:		1257	226.50
Observation Wells			
OBS Well:			
Download to handheld (P5)		✓	265.51 @ 1449 w/ sounder
OW-A:		✓	↳ changed x-ducer
Download to handheld (P5) (3)		✓	
OW-B:			
Download		✓	
Piezometer water level		1319	290.38
OW-C:			
Download		✓	
Piezometer water level		1327	236.59
El Rancho Well			
Piezometer water level		1425	213.95
SFCC Well			
Piezometer water level		1558	212.50

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 10/3/06	Observed by: MLK	Time	Observation
Production Well	CCD-Prod 1:		
	Flow-1 GPM:		52 gpm
	Flow-1 Total:		26562.00
	Pressure-0	14:10	205 psi
	Pressure-1		49-50 psi
	Battery VDC	14:13	23.16
	Seal Batt. Box	✓	
	Water Quality	✓	fizzy / lots of bubbles.
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	changed batt on X-ducer ↳ pulled x-ducer
CCD-Expl 1: 1555 295.80	15:30	313.90	
Piezometer water levels (2) Shallow:	15:39	244.76	
Deep:	15:41	233.61	
Download to handheld (old cable, P4)			
Injection Well	Air purged	✓	
	Flow-2 GPM:		51 gpm
	Flow-2 Total:		25744.00
	Pressure-2	13:24	57 psi
	Pressure-3	"	52 psi
	Battery VDC	✓	changed batt.
	Seal Batt. Box	✓	
	Water Quality	✓	slightly fizzy
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
Piezometer water levels (2) Shallow:	13:30	215.81	
Deep:	13:35	233.63	
Observation Wells	OBS Well:		
	Download to handheld (P5)	16:34	205.49
	OW-A:		
	Download to handheld (P5) (3)	✓✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	13:52	290.21
OW-C:			
Download	✓		
Piezometer water level	13:59	236.92	
El Rancho Well	Piezometer water level	16:12	214.0
SFCC Well	Piezometer water level	17:02	228.25 needs tape measure

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 10/10/06		Observed by: Mick	
		Time	Observation
Production Well	CCD-Prod 1:		
	Flow-1 GPM:	11:42	51-52, mostly 52, slight fluctuation
	Flow-1 Total:		3171800
	Pressure-0		20.6
	Pressure-1		53 psi
	Battery VDC		25.43
	Seal Batt. Box	✓	
	Water Quality		set, repaired r-reducer, few bubbles / ear
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
CCD-Expl 1:	Piezometer water levels (2) Shallow:	12:03	245.05
	Deep:	12:59	233.54
	Download to handheld (old cable, P4)	✓	changed batts to r-reducer, reset.
Injection Well	Air purged		
	Flow-2 GPM:	13:36	50 gpm
	Flow-2 Total:		3093100
	Pressure-2		54 psi
	Pressure-3		48 psi
	Battery VDC		24.76
	Seal Batt. Box	✓	
	Water Quality		fizzy
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
Piezometer water levels (2)	Shallow:	14:01	315.70
	Deep:	13:52	222.14
Observation Wells	OBS Well:		
	Download to handheld (P5)	✓	
	OW-A:		
	Download to handheld (P5) (3)	✓	
	OW-B:		
	Download	✓	
	Piezometer water level	14:02	289.91
	OW-C:		
	Download	✓	
	Piezometer water level	14:32	236.57
El Rancho Well	Piezometer water level	15:16	214.16
SFCC Well	Piezometer water level	15:28	228.55

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 10/17/06		Observed by: Mick	
		Time	Observation
Production Well	CCD-Prod 1:		
	Flow-1 GPM:	1343	50-51 gpm
	Flow-1 Total:	"	3696800
	Pressure-0		206
	Pressure-1		49
	Battery VDC	1346	24.91
	Seal Batt. Box	✓	
	Water Quality	✓	
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	X	started new test @ 1400
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:		
	Deep:		
	Download to handheld (old cable, P4)		
Injection Well	Air purged		
	Flow-2 GPM:	12:32	50
	Flow-2 Total:	"	3603800
	Pressure-2	"	55 psi
	Pressure-3	"	49 psi
	Battery VDC	12:34	24.19
	Seal Batt. Box	✓	
	Water Quality	✓	fizzy, tiny bubbles
	Laptop ELOG	✓	
	Downloads to handheld (P5) Deep ←	✓	222.66 @ 12:43 sol 500
Piezometer water levels (2) Shallow	12:47	230.81	
	Shallow Deep	12:50	315.57
Observation Wells	OBS Well:		
	Download to handheld (P5)	✓	
	OW-A:		
	Download to handheld (P5) (3)	✓✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	✓	
	OW-C:		
Download	✓		
Piezometer water level	✓		
El Rancho Well	Piezometer water level		
SFCC Well	Piezometer water level		

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 10/24	Observed by: MICK	Time	Observation
Production Well	CCD-Prod 1:		
	Flow-1 GPM:		55
	Flow-1 Total:		423.5900
	Pressure-0		199
	Pressure-1		22
	Battery VDC		24.32
	Seal Batt. Box	✓	
	Water Quality	✓	clear, few tiny bubbles
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:	1357	246.02
	Deep:	1401	233.60
	Download to handheld (old cable, P4)	✓	
Injection Well	Air purged		✓
	Flow-2 GPM:		54
	Flow-2 Total:		4150300
	Pressure-2		77 psi
	Pressure-3		70 "
	Battery VDC		22.47 25.55 re-read
	Seal Batt. Box	✓	
	Water Quality	✓	Clear, No Bubbles
	Laptop ELOG	✓	
	Downloads to handheld (P5)		
	Piezometer water levels (2) Shallow:	1244	215.90
	Deep:	1239	215.81
Observation Wells	OBS Well: hand meas v/c	14:35	205.05
	Download to handheld (P5)	✓	
	OW-A:		
	Download to handheld (P5) (3)	✓	
	OW-B:		
	Download	✓	
	Piezometer water level	1331	289.90
	OW-C:		
	Download	✓	
	Piezometer water level	1339	236.64
El Rancho Well	Piezometer water level	1419	213.99
SFCC Well	Piezometer water level		

PEH
SOL 2973

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 10/31	Observed by: MICK	Time	Observation	
Production Well	CCD-Prod 1:			
	Flow-1 GPM:		51 gpm	
	Flow-1 Total:		46.28 4748600	
	Pressure-0		206 psi	
	Pressure-1		47 psi	
	Battery VDC		23.78	
	Seal Batt. Box	✓	changed batt.	
	Water Quality	✓	fizzy, lots of bubbles	
	Laptop ELOG	✓		
	Download to handheld (old cable, P4)	✓		
	CCD-Expl 1:			
	Piezometer water levels (2) Shallow:	12:21	245.78	
	Deep:	12:17	233.61	
	Download to handheld (old cable, P4)	✓		
Injection Well	Air purged			
	Flow-2 GPM:		51 gpm	
	Flow-2 Total:		4662800	
	Pressure-2		54 psi	
	Pressure-3		48 psi	
	Battery VDC	11:02	24.92	
	Seal Batt. Box	✓		
	Water Quality	✓	fizzy, lots of tiny bubbles	
	Laptop ELOG	✓		
	Downloads to handheld (P5)	✓		
	Piezometer water levels (2) Shallow:	11:14	315.76	
	Deep:	11:18	218.32	
	Observation Wells	OBS Well: PEH	13:56	205.67
		Download to handheld (P5)	✓	
OW-A:				
Download to handheld (P5) (3)	✓✓			
OW-B:				
Download	✓			
Piezometer water level	11:36	249.83		
OW-C:				
Download	✓			
Piezometer water level	11:43	236.70		
El Rancho Well				
	Piezometer water level	13:37	214.18	
SFCC Well				
	Piezometer water level	13:27	227.30	

La Cienega Piezometer level 13:09 224.29

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 11/7	Observed by: M. Ck	Time	Observation
Production Well	CCD-Prod 1:		
	Flow-1 GPM:		50
	Flow-1 Total:		5264700
	Pressure-0		206
	Pressure-1		48
	Battery VDC	1255	24.88
	Seal Batt. Box	✓	
	Water Quality		clear, low few tiny particles.
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:	1302	245.88
	Deep:	1305	238.63
	Download to handheld (old cable, P4)	✓	
Injection Well			
	Flow-2 GPM:		50
	Flow-2 Total:		5175200
	Pressure-2		55
	Pressure-3		48
	Battery VDC	1100	24.32
	Seal Batt. Box	✓	
	Water Quality		fizzy, tiny bubbles
	Laptop ELOG		
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:	1121	315.84
	Deep:	1118	217.12
Observation Wells			
	Rancho Viejo OBS Well:	1202	205.82 pulled & ducer
	Download to handheld (P5)	✓	
	OW-A:		
	Download to handheld (P5) (3)	✓✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	1136	289.88
	OW-C:		
	Download	✓	
	Piezometer water level	1142	236.83
El Rancho Well			
	Piezometer water level	1225	214.15
SFCC Well			
	Piezometer water level	1235	227.0
La Cienega Well			
	Piezometer water level	1328	225.41

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 11/14/06	Observed by: MICK	Time	Observation
Production Well	CCD-Prod 1:		Inside MAX: 82.5
	Flow-1 GPM:	50	MW: 55.5
	Flow-1 Total:	57742	OUT MAX: 76.8
	Pressure-0	206	MW: LL.2
	Pressure-1	47	
	Battery VDC	no meter	
	Seal Batt. Box	✓	
	Water Quality	✓	Fizzy, lots of tiny bubbles
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:	1244	245.73
	Deep:	1242	233.67
	Download to handheld (old cable, P4)	✓	
Injection Well			Inside: MAX: 76.4
			MW: 46.7
	Flow-2 GPM:	50 gpm	
	Flow-2 Total:	5685200	
	Pressure-2	54 psi	
	Pressure-3	47 psi	
	Battery VDC	no meter	
	Seal Batt. Box	✓	
	Water Quality	✓	Fizzy, lots of tiny bubbles
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:	1117	315.49
	Deep:	1121	216.37
Observation Wells	Rancho Viejo OBS Well:		
	Download to handheld (P5) Piezometer W.L.	1202	205.71
	OW-A:		
	Download to handheld (P5) (3)	✓✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	1136	289.68
	OW-C:		
	Download	✓	
	Piezometer water level	1144	236.56
El Rancho Well			
Piezometer water level	1218	214.06	
SFCC Well			
Piezometer water level	1253	226.81	
La Cienega Well			
Piezometer water level	14:14	225.16	Powers 1000'

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 11/21/06	Observed by: MICK		
		Time	Observation
Production Well	CCD-Prod 1:		
	Flow-1 GPM:		51 gpm
	Flow-1 Total:		629,4600 gal
	Pressure-0		206 psi
	Pressure-1		49 psi
	Battery VDC		22.27
	Seal Batt. Box		✓
	Water Quality		fizzy, bubbles
	Laptop ELOG		✓
	Download to handheld (old cable, P4)		✓
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:	1544	245.91
	Deep:	1542	233.69
	Download to handheld (old cable, P4)		✓
Injection Well			
	Flow-2 GPM:		50 gpm
	Flow-2 Total:		6202700 gal
Temp	Pressure-2		56 psi
inside MAX: 71.4	Pressure-3		49-50 psi
min: 47.8	Battery VDC		23.04, changed, 25.52
	Seal Batt. Box		✓
out MAX: 85.2	Water Quality		fizzy, bubbles
MW: —	Laptop ELOG		✓
	Downloads to handheld (P5)		✓
	Piezometer water levels (2) Shallow:	1344	315.93
	Deep:	1342	215.34
Observation Wells			
	Rancho Viejo OBS Well:		
	Download to handheld (P5) W.L.	1500	205.49
	OW-A:		
	Download to handheld (P5) (3)		✓✓✓
	OW-B:		
	Download		✓
	Piezometer water level	1404	289.99
	OW-C:		
	Download		✓
	Piezometer water level	1411	236.81
EI Rancho Well			
	Piezometer water level	1516	214.06
SFCC Well			
	Piezometer water level	1610	233.10 227.10
La Cienega Well			
	Piezometer water level	1557	225.39

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 11/28/06	Observed by: MICK	Time	Observation
Production Well			
CCD-Prod 1:			
Inside MW: 70.8	Flow-1 GPM:		51
MW: 51.6	Flow-1 Total:		6809900
	Pressure-0		206
	Pressure-1		48
	Battery VDC		20.15 - replaced to 25.31
	Seal Batt. Box		✓
	Water Quality		fizzy, tiny bubbles
	Laptop ELOG		✓
	Download to handheld (old cable, P4)		✓
CCD-Exp1 1:			
	Piezometer water levels (2) Shallow:	1521	245.98
	Deep:	1524	233.74
	Download to handheld (old cable, P4)		✓
Injection Well			
Inside MW: 76.2	Flow-2 GPM:		50
MW: 49.6	Flow-2 Total:		6714300
	Pressure-2		56 psi
	Pressure-3		48 psi
	Battery VDC		25.50 ⊖ cable unplugged - re-attached
	Seal Batt. Box		✓
	Water Quality		fizzy, lots of bubbles
	Laptop ELOG		✓
	Downloads to handheld (P5)		✓
	Piezometer water levels (2) Shallow:	1400	315.47
	Deep:	1358	214.30
Observation Wells			
Rancho Viejo OBS Well:			
	Download to handheld (P5) w.L.:	14:34	205.66
	OW-A:		
	Download to handheld (P5) (3)		✓✓
	OW-B:		
	Download		✓
	Piezometer water level	1413	289.71
	OW-C:		
	Download		✓
	Piezometer water level	1420	236.67
El Rancho Well			
	Piezometer water level	1452	214.14
SFCC Well			
	Piezometer water level	1547	226.78
La Cienega Well			
	Piezometer water level	1536	225.17

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 12/5/06	Observed by: MCLK	Time	Observation
Production Well			
CCD-Prod 1:			
Inside Max: 67.8	Flow-1 GPM:	9	51
Inside Min: 45.1	Flow-1 Total:		732.80
Outside Max: 80.2	Pressure-0		206
Outside Min: 45.3	Pressure-1		49
	Battery VDC		24.39
	Seal Batt. Box	✓	24.39
	Water Quality		fizzy, lots of tiny bubbles
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
CCD-Expl 1:			
	Piezometer water levels (2) Shallow:	1401	246.14
	Deep:	1404	233.89
	Download to handheld (old cable, P4)	✓	
Injection Well			
Inside Max: 63.5	Flow-2 GPM:		50
Inside Min: 31.9	Flow-2 Total:		7223200
Outside Max: 74.3	Pressure-2		58
Outside Min: 2	Pressure-3		50
	Battery VDC		24.67
	Seal Batt. Box	✓	
	Water Quality		
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:		315.88 @ 12:42 PM
	Deep:		213.69 @ 12:40 PM
Observation Wells			
	Rancho Viejo OBS Well: Windmill?		vane is closed
	Piezometer water level	1623	205.12
	OW-A:		
	Download to handheld (P5) (3)	✓✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	1257	290.06
	OW-C:		
	Download	✓	
	Piezometer water level	1303	236.85
El Rancho Well			
	Piezometer water level	1636	214.04
SFCC Well			
	Piezometer water level	1706	226.71
La Cienega Well			
	Piezometer water level	1654	225.67

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 12/12/06	Observed by: Mick	Time	Observation
Production Well			
CCD-Prod 1:			
Inside Max: 70.1	Flow-1 GPM:		49
Inside Min: 60.1	Flow-1 Total:		7833300
Outside Max:	Pressure-0		206
Outside Min:	Pressure-1		41
	Battery VDC		23.76
	Seal Batt. Box	✓	
	Water Quality		
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
CCD-Expl 1:			
	Piezometer water levels (2) Shallow:		
	Deep:		
	Download to handheld (old cable, P4)		
Injection Well			
Inside Max: 72.5	Flow-2 GPM:		49
Inside Min: 53.4	Flow-2 Total:		7720800
Outside Max:	Pressure-2		49
Outside Min:	Pressure-3		42
	Battery VDC		24.09 24.09
	Seal Batt. Box	✓	
	Water Quality		
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:	1128	315.10
	Deep:	1124	214.55
Observation Wells			
Rancho Viejo OBS Well:			
	Piezometer water level	1228	205.13
	OW-A:	✓	
	Download to handheld (P5) (3)	✓✓	
	OW-B:	✓	
	Download	✓	
	Piezometer water level	✓	
	OW-C:	✓	
	Download	✓	
	Piezometer water level	✓	
El Rancho Well			
	Piezometer water level	1243	214.31
SFCC Well			
	Piezometer water level		
La Cienega Well			
	Piezometer water level		

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FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 12/27/06		Observed by: CWC	
		Time	Observation
Production Well	CCD-Prod 1:		
Inside Max:	Flow-1 GPM:		49-50 gpm
Inside Min:	Flow-1 Total:		8919300
Outside Max:	Pressure-0	15:26	210 ps
Outside Min:	Pressure-1		46 ps
	Battery VDC		22.12 changed → 25.43
	Seal Batt. Box		✓
	Water Quality		clear
	Laptop ELOG		✓
	Download to handheld (old cable, P4)		✓
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:	15:18	246.10
	Deep:	15:22	235.18
	Download to handheld (old cable, P4)		✓
Injection-Well			
Inside Max: 20	Flow-2 GPM: 50		50
Inside Min: screw	Flow-2 Total: 88073		8807300
Outside Max: driver	Pressure-2: 53 psi		53
Outside Min:	Pressure-3		47
	Battery VDC		22.85 (meds change)
	Seal Batt. Box		✓
	Water Quality		✓
	Laptop ELOG		✓
	Downloads to handheld (P5)		✓
	Piezometer water levels (2) Shallow:	14:34	315.51
	Deep:	14:32	212.30 e
Observation Wells			
	Rancho Viejo OBS Well:		
	Piezometer water level		✓
	OW-A:		
	Download to handheld (P5) (3)		✓✓✓
	OW-B:		
	Download		✓
	Piezometer water level	14:55	289.90
	OW-C:		
	Download		
	Piezometer water level	15:04	236.70
El Rancho Well			
	Piezometer water level		✓
SFCC Well			
	Piezometer water level		✓
La Cienega Well			
	Piezometer water level		✓

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Note: Logger times
are 1 hr off →
daylight saving time

Date:	Observed by:	Time	Observation
1/10/07	CWC		
Production Well	CCD-Prod 1:	8:10	9906200
Inside Max:	Flow-1 GPM:	50	
Inside Min:	Flow-1 Total:		9906200 gal 8:00
Outside Max:	Pressure-0	220	
Outside Min:	Pressure-1	146	
	Battery VDC	24.11	
	Seal Batt. Box		
	Water Quality		
	Laptop ELOG		✓
	Download to handheld (old cable, P4)		✓
	CCD-Expl 1:	7:40	300.29
	Piezometer water levels (2) Shallow:	7:35	246.04
	Deep:	7:37	234.00
	Download to handheld (old cable, P4)	7:30	✓
Injection Well		09:56	213.52
Inside Max:	Flow-2 GPM:		49-50 49-50
Inside Min: 50	Flow-2 Total:	11:30	9240000
Outside Max:	Pressure-2		54 psi
Outside Min: 2.5	Pressure-3	09:30	47 psi
	Battery VDC		26.01V
	Seal Batt. Box		replaced (batteries were dead)
	Water Quality		✓
	Laptop ELOG		✓
	Downloads to handheld (P5)		✓
	Piezometer water levels (2) Shallow:	09:42	315.89
	Deep:	09:46	211.59
Observation Wells			
	Rancho Viejo QBS Well:		shl 222.87 10:22
	Piezometer water level		Int 222.76 10:30
	OW-A:		Deep 222.63 10:25
	Download to handheld (P5) (3)		✓
	OW-B:	10:40	282.74
	Download		✓
	Piezometer water level	10:45	290.19
	OW-C:		
	Download		
	Piezometer water level		
EI Rancho Well		11:00	214.05
	Piezometer water level		
SFCC Well		9:00	226.54
	Piezometer water level		
La Cienega Well			
	Piezometer water level		too much snow to drive to site

957 652 6811

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date:	Observed by:	Time	Observation
Production Well			
CCD-Prod 1:			
Inside Max: 71.9	Flow-1 GPM:		50
Inside Min: 57.5	Flow-1 Total:		11013000
Outside Max:	Pressure-0		206
Outside Min:	Pressure-1		50
	Battery VDC	✓	
	Seal Batt. Box	✓	changed batt
	Water Quality		
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
CCD-Expl 1:			
	Piezometer water levels (2) Shallow:	13:56	234.02 Deep
	Deep:	14:00	246.65 shallow
	Download to handheld (old cable, P4)	✓	solchst reel broken
Injection Well			
Inside Max: 77.3	Flow-2 GPM: 51		
Inside Min: 44	Flow-2 Total: 10335100		
Outside Max:	Pressure-2 53		
Outside Min:	Pressure-3 51		
	Battery VDC		24.80
	Seal Batt. Box	✓	
	Water Quality	✓	
	Laptop ELOG	✓	
	Downloads to handheld (P5)	13:49	211.42
	Piezometer water levels (2) Shallow:	13:51	316.00
	Deep:	13:54	209.63
Observation Wells			
Rancho Viejo OBS Well:			
	Piezometer water level		Too much snow
OW-A:			
	Download to handheld (P5) (3)	✓✓	
OW-B:			
	Download	✓	
	Piezometer water level	13:14	290.36
OW-C:			
	Download		Too much snow
	Piezometer water level		
El Rancho Well			
	Piezometer water level	13:24	214.12
SFCC Well			
	Piezometer water level	14:12	226.69
La Cienega Well			
	Piezometer water level	Too	much snow

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

- 1 /

Date: 1/30/07		Observed by: MICK		Time	Observation
Production Well	CCD-Prod 1:			49	
Inside Max: 69.9	Flow-1 GPM:			11372700	349
Inside Min: 59.5	Flow-1 Total:				
Outside Max:	Pressure-0			209	
Outside Min:	Pressure-1			40	
	Battery VDC			24.94	
	Seal Batt. Box		✓		
	Water Quality				
	Laptop ELOG		✓		
	Download to handheld (old cable, P4)		✓		
	CCD-Expl 1:				
	Piezometer water levels (2)	Shallow: 1305		245.65	Powers 500"
		Deep: 1309		233.16	"
	Download to handheld (old cable, P4)		✓		
Injection Well					
Inside Max: 70.5	Flow-2 GPM:			49	
Inside Min: 48.2	Flow-2 Total:			10704300	32.8 AF
Outside Max:	Pressure-2			49	
Outside Min:	Pressure-3			42	
	Battery VDC			24.35	
	Seal Batt. Box		✓		
	Water Quality				
	Laptop ELOG		✓		
	Downloads to handheld (P5)		✓		
	Piezometer water levels (2)	Shallow: 1358		313.98	Powers 500'
		Deep: 1349		207.93	"
					+0.6 = 208.53 correction
Observation Wells					
	Rancho Viejo OBS Well:				
	Piezometer water level				
	OW-A:				
	Download to handheld (P5) (3)		✓✓		
	OW-B:				
	Download		✓		
	Piezometer water level		1420	298.70	
	OW-C:				
	Download		✓		
	Piezometer water level		1430	235.55	
El Rancho Well					
	Piezometer water level		1330	213.37	
SFCC Well					
	Piezometer water level		1320	226.55	
La Cienega Well					
	Piezometer water level				

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

1437:57.98

Date: 2/09	Observed by: Mick	Time	Observation
Production Well	CCD-Prod 1:		
Inside Max: 73.4	Flow-1 GPM:	Flow 1	49
Inside Min: 56.6	Flow-1 Total:	Flow 1 Tot.	12025500
Outside Max:	Pressure-0	1609	218.36
Outside Min:	Pressure-1		206
	Battery VDC		48
	Seal Batt. Box	✓	24.46
	Water Quality	✓	
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	changed x-duces batt, reset test
	CCD-Expl 1:		
	Piezometer water levels (2) Shallow:	1416	246.51
	Deep:	1415	234.11
	Download to handheld (old cable, P4)	✓	
Injection Well			
Inside Max: 81.3	Flow-2 GPM:		50
Inside Min: 46.7	Flow-2 Total:		11348700
Outside Max:	Pressure-2		55
Outside Min:	Pressure-3		49
	Battery VDC		23.74, changed batt
	Seal Batt. Box	✓	
	Water Quality	✓	
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:	1321	315.83
	Deep:	1319	209.20
Observation Wells			
	Rancho Viejo OBS Well:		
	Piezometer water level	1516	204.94
	OW-A:		
	Download to handheld (P5) (3)	✓✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	1345	290.27
	OW-C:		
	Download	✓	
	Piezometer water level	1336	236.64
El Rancho Well			
	Piezometer water level	1437	214.08
SFCC Well			
	Piezometer water level	1648	226.55
La Cienega Well			
	Piezometer water level	1635	225.48

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 2/20	Observed by: Mick	Time	Observation
Production Well			
CCD-Prod 1:			50
Inside Max: 72.6	Flow-1 GPM:		50
Inside Min: 56.8	Flow-1 Total:		12869000
Outside Max:	Pressure-0		209
Outside Min:	Pressure-1		46
	Battery VDC		23.76
	Seal Batt. Box	✓	
	Water Quality	—	
	Laptop ELOG	✓	
	Download to handheld (old cable, P4)	✓	
CCD-Expl 1:			
	Piezometer water levels (2) Shallow:	12 18	245.81
	Deep:	12 21	234.22
	Download to handheld (old cable, P4)	✓	
Injection Well			
Inside Max: 76.4	Flow-2 GPM:		50
Inside Min: 48.6	Flow-2 Total:		12193800
Outside Max:	Pressure-2		54
Outside Min:	Pressure-3		48
	Battery VDC		24.46
	Seal Batt. Box	✓	
	Water Quality	—	
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:	1333	315.83
	Deep:	1336	208.99
Observation Wells			
Rancho Viejo OBS Well:			
	Piezometer water level	1422	204.84
	OW-A:		
	Download to handheld (P5) (3)	✓✓	
	OW-B:		
	Download	✓	
	Piezometer water level	1351	289.70
	OW-C:		
	Download	1401	236.76
	Piezometer water level	✓	
El Rancho Well			
	Piezometer water level	1449	213.94
SFCC Well			
	Piezometer water level	1521	226.54
La Cienega Well			
	Piezometer water level	1500	225.54

FIELD CHECKLIST:
RANCHO VIEJO WELLFIELD

Date: 2/26/07	Observed by: MICK	Time	Observation
Production Well			
CCD-Prod 1:			
Inside Max:	Flow-1 GPM:		48-49
Inside Min:	Flow-1 Total:		13302000
Outside Max:	Pressure-0		210
Outside Min:	Pressure-1		40
	Battery VDC		
	Seal Batt. Box	✓	22.94
	Water Quality	✓	
	Laptop ELOG		
	Download to handheld (old cable, P4)		
CCD-Expl 1:			
	Piezometer water levels (2) Shallow:		
	Deep:		
	Download to handheld (old cable, P4)		
Injection Well			
Inside Max:	Flow-2 GPM:		49
Inside Min:	Flow-2 Total:		12617800
Outside Max:	Pressure-2		49
Outside Min:	Pressure-3		44
	Battery VDC		22.72
	Seal Batt. Box	✓	
	Water Quality	✓	
	Laptop ELOG	✓	
	Downloads to handheld (P5)	✓	
	Piezometer water levels (2) Shallow:	1129	315.68
	Deep:	1126	209.67
Observation Wells			
	Rancho Viejo OBS Well:		
	Piezometer water level		
	OW-A:		
	Download to handheld (P5) (3)		
	OW-B:		
	Download		
	Piezometer water level		
	OW-C:		
	Download		
	Piezometer water level		
El Rancho Well			
	Piezometer water level		
SFCC Well			
	Piezometer water level		
La Cienega Well			
	Piezometer water level		

3/2/07

CWL onsite CCD wells using Solinst 500 sounder 0740

	DTW	Time
CCD-I1 sh piez	315.80	0749
deep piez	258.21	0745
CCD OUB ch piez	290.67	0802
Ow c sh piez	236.95	0809
CCD-X1 sh piez	243.80	08 27 27
deep piez	243.18	0830
SFCC	226.62	0838
El rancho	214.27	0845

13-782 500 SHEETS, FULLER, 8 SQUARE
 42-301 50 SHEETS, EYE-EASE, 8 SQUARE
 42-302 100 SHEETS, EYE-EASE, 8 SQUARE
 42-303 100 SHEETS, EYE-EASE, 8 SQUARE
 42-304 100 SHEETS, EYE-EASE, 8 SQUARE
 42-305 200 RECYCLED, WHITE, 8 SQUARE
 Made in U.S.A.



Injection / Observation
Well Test Records

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. inj well 12 inch csg Rate Control _____
 Location _____ Measuring Point top meas tube,
 Collected By _____ Pump Intake (ft.) 2.01 ft above
surf csg

Clock Time (24hrs)			Hold Unit	+ - DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec				t	t'	t/t'	
8	10	06							well csg cut down, inj. eqpt installed
09	08			296.55	+0.5 =	297.05			powers 1000
8	24	06							set transducer 4N 103747
14	05			296.08	powers 1000	296.58			(300 psi) to 635.00 ft 315.00
9	8								
10	51			241.75	sol 500				sol 500
13	30								lowered transducer ~ 20 ft to
									get below drop pipe for
9	8								better temperature sensing.
14	00			242.10	sol 500				
10	17	06							
	12	43		222	66	sol 500			
12	12	06							
12	10			216	51				
11	10	07							
09	50			213	52				
1	25	07							
12	49			211	42				
2	26	07							
11	34			211	37				Final meter 12684600

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. Inj Well shallow piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point +00
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δrate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
6	28	06								
15	20		317	44	+0.5	= 317.94				w/ power 1000' casing not covered
8	10	06								csg cut down - 1.046ft above surf csg
9	12		315	27	+0.5	315.77				
8	24	06								
16	14		315	08	+0.5	315.58				power loss transducer S/N 103826
9	18									(rental) set to 351.78 ft
10	55		315	62						sol 500
9	12	06								Pulled Xducer
11	00									
11	13	51	315	81						sol 500
9	19	06								
11	55		315	88						"
9	26	06								
13	01		315	96						"
10	3	06								
13	30		315	81						"
10	10	06								
14	01		315	70						"
10	17	06								
12	50		315	87						
10	24	06								
12	44		315	90						
10	31	06								
11	14		315	76						
11	07	06								
11	25	21	315	84						
	11	14	06							
11	17		315	49						

AQUIFER WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline 50' inst 560
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. Faj Well Shallow Piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point TC
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
11	21	06								
13	44		315	93						
11	28	06								
14	00		315	47						
12	5	06								
12	42		315	88						
12	12	06								
11	28		315	98						
12	27	06								
14	34		315	51						
11	10	07								
09	42		315	89						
1	24	07								
12	51		316	00						
1	30	07								
13	58		314	04						
2	8	07								
13	21		315	83						
2	20	07								
13	33		315	83						
2	26	07								
11	29		315	68						
2	27	07								
8	37		315	75						
10	03		315	74						
11	51		315	71						
13	30		315	66						
2	28	07	1164	79						
			315	93						

16/67 14:06
 3/13/07 14:06
 315.73
~~273.35~~

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Deep Piez

Well ID. Injection Well
 Location ZV
 Collected By CWC

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	-	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.	
Hr	Min	Sec						t	t'	t/t'		
6/28/06												Set transducer s/n 103797 (300 psi)
14	15											to 531.72 ft
15	14		301	22		→ 301.72						w/ power loss ducer 230.0
												Casing not cut yet
8/10/06												csg cut to 0.68' above next csg
09	18		295	22	+ 0.5	295.72						transducer pulled by
8/24												Rodgers; csg ~ 8/1
16	09		294	78	+ 0.5	295.28						Installed rental transducer
9/8/06												s/n 103186 to 300.44 ft
13	28		240	22		sol 500						
9/12/06												
2	11:00											pulled x-ducer
13	46		235	90								
9/19/06												
11	52		230	00								sol 500
9/26/06												
12	57		226	50								"
10/3/06			2									
13	35		213	63								"
10/10/06												
13	52		222	14								"
10/17/06												
12	47		220	87								"
10/24/06												
12	39		215	81								
10/31/06												
11	18		219	32								
11/07/06			217									
11	18		217	12								

Deep Piez

Well ID. Injector Well
 Location RY
 Collected By MR

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery Step 1-2-3-4
 Tape, M-scope, airline
 Start Time _____
 Starting Rate _____
 Static at Start _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
11	14	06								
11	21		216	37						Sol. hst 500'
11	21	06								
11	42		215	34						"
11	28	06								
11	58		214	30						
12	5	06								
12	40		213	69						
12	12	06								
11	24		214	55						
12	27	06								
12	32		212	30						
1	16	07								
11	59	46	211	59						
11	25	07								
12	54		209	63						
1	30	07								
13	49		208	53						
2	8	07								
13	19		209	20						
2	20	07								
13	36		208	98						
2	26	07								
11	26		209	67						
2	27	07								
8	34		209	40						Shutdown @ 10:00
10	04	30	219	19						
11	49		227	06						
3	28		229	27						
2	21	07								
11	16		243	78						

3/6/07 C:\admin (SL)\forms\tech\AWTR.DOC
 16:13 272.05

3/13/07 16:12 273.35

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4 _____

Tape, M-scope, airline _____

Start Time _____

Starting Rate _____

Static at Start _____

 Well ID. OW A shallow
 Location RV
 Collected By _____

 Rate Control _____
 Measuring Point to C → 2.58 ft
 Pump Intake (ft.) above surface

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
	6/28/06									
15	35		300	51	+0.5 =	301.0'				Powers 1000
	8/10/06									
10	30		296	98	+0.5 =	297.48				Get transducer s/n 107472 (100 psi) to 350 psi = 16 ft
8	24									
14	52		296	45	→	296.95				Powers
	9/10/06									
13	40		249	29	sol	520				
	10/17/06									
13	02		230	39						
	12/12/06									
	1/4/07		225	07						
	1/16/07									
16	22		222	87						
	2/7/07									
11	42		221	71						
	3/13/07									
14	42		279	26						pulling reducer to put in RV obs well

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. OW-A (Interim)
 Location RV
 Collected By _____

Rate Control _____
 Measuring Point hdc → 2.55 ft above top surf
 Pump Intake (ft.) top surf
CSG

Clock Time (24hrs)			Hold Unit	+ - DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec				t	t'	t/t'	
6	28	06							set transducer S/N 104002 100
6	30								to 350.86 FE hdc
13	38		300	17 = 300.67					w/ powers 1000
									educer 50.19
8	24	06							348.31 above top sur
15	00		295	92 = 296.42					powers 1000
9	18								
13	43		249	30 Sol 500					
10	17	06							
13	06		230	35 "					
12	12	06							
	11	46	225	00					
1	00	07							
10	30		222	76					
2	20	07							
11	46		221	53					

AQUIFER/WELL TEST RECORD

BGW Sheet of
 Test Date
 Drawdown/Recovery
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time
 Starting Rate
 Static at Start

Well ID. Obs A deep
 Location
 Collected By

Rate Control
 Measuring Point TOC → 2.62 ft
 Pump Intake (ft.) Above surf csg

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
6	28	06								
14	35									
15	42		296	20		296.70				corrected set xducer #/N 104001 to 485.75 ft (100 psi) w/1000' static power's xducer 189.05
8	24									
14	56		291	78		292.28				below
9	18									483.13 at
13	46		254	22	sol	568				moved transducer up about 10 ft @ 13:55 surf csg
10	17	06								
	13	08	231	12						
12	12	06	224	91						
11	44									
1	10	07								
10	25		222	63						
2	26	07								
11	45		221	19						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. OW-13
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point to C - 2.56 ft
 Pump Intake (ft.) above surf csg

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
6	28	06								
14	45									Xducer 104000 set (100 psi) rd 345.29 ft Xducer 42.77 ft w/ powers 1000'
15	52		302	02	302.52					542.73 ft - below surf csg
8/24/06	15	15	298	60	299.10					powers 1000
9/8	16	40	290	77						sd 500
10/17/06	13	17	295	30						sd 500
12/12/06	11	51	283	41						
12/27/06	14	55	289	90						
1/10/07	10	40	282	74						
2/2/07	12	41	282	04						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. OWB shallow #2 Rate Control _____
 Location _____ Measuring Point fdc → 2.51
 Collected By _____ Pump Intake (ft.) to above surf csg

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
6	28	06								
15	55		297	98	→ 293.48					power 1000'
8	10	06								
10	58		291	97	292.47					" "
8	24									
15	19		291	97	292.47					" "
8	28									
14	18		292	09	292.59					" "
8	24									
11	29		292	19	292.64					" "
14	49		292	13	292.63					
15	58		292	10	292.60					" "
	8	30								
12	27		292	00	292.50					" "
	9	1/06								
13	44		291	74						"
9	15	06								
11	48		291	46						"
9	18	06								
16	38		290	95	→ 291.45					291.38 / Sol/s
9	12									
13	40		291	28						Sol, not 500
9	19	06								
14	07		290	30						"
9	26	06								
13	19		290	38						"
10	3	06								
13	52		290	21						"
10	10	06								
14	22		289	91						"
	10	17	1321	289	81					"

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. OW-B shallow piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point TOC + 2.51
 Pump Intake (ft.) above surf 65g

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
10/24/06										
13	31		289	90						
10/31/06										
11	36		289	83						
11/07/06										
11	36		289	88						
11/14/06										
11	36		289	68						
11/21/06										
14	04		289	99						
11/28/06										
14	13		289	71						
12/5/06										
12	57		290	06						
12/12/06										
11	55		290	14						
12/27/06										
14	55		289	90						
1/10/07										
10	45		290	19						
1/28/07										
13	14		290	36						
1/30/07										
14	20		288	70						
2/8/07										
13	45		290	27						
2/20/07										
13	51		289	70						
2/26/07										
12	41		290	22						
2/27										
13/45			290	26						S3/MSH 500

13/48 288.72 Powers 500

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery_ _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. OW 3 shallow piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point to 251
 Pump Intake (ft.) 664 concrete pump

Clock Time (24hrs)			Hold Unit	+	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
2	27	07								
10	03		288	73						Power Saw
11	56		288	68						
10	21		288	71						
13	38		288	70						
14	10		288	67						
15	06		288	65						
2	29	07								
11	05		290	15						solinst 500
3	2	07								
8	02		290	67						"
3	6	07								
16	20		291	18						
3	13	07								
14	30		291	50						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. OW-C
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point FOC = 2.50 above
 Pump Intake (ft.) top surf csg

Clock Time (24hrs)			Hold Unit	+	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec		-			t	t'	t/t'	
6	28	06								
15	00									set reducer S/N 103998 (30 ft) to 325.47 for FOC reducer 67.75 powers 1000
16	08		257	30	+0.42	257.72				
8	24									= 323
15	38		252	12	+0.42	252.54				powers 1000
9	8	06								
10	27		248	70						50/500
10	17	00								
13	36		244	39						v
12	12	00								
12	04		242	96						
2	26	07								
12	52		241	34						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. 06C Shallow piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
6	25	06								Can't measure - cap not accessible to wrench
8	24	06								
15	40		236	57	+ 16	237.07				press 600
8	28				0.5	237.20				"
14	32		236	70	16.5	236.88				"
8	30									
12	12		236	85	.18	237.03				solinst 300
9	11									
13	33		236	74						"
9	5									
11	42		236	60						"
	9	18								
16	30		236	58						sol 500
9	12									
13	26		236	64						sol 500
9	19	06								
14	18		236	59						"
9	26	06								
13	27		236	59						"
10	3	06								
13	59		236	92						"
10	10	06								
14	32		236	57						"
10	17	06								
13	33		236	57						"
10	24	06								
13	39		236	64						
10	31	06								
11	43		236	70						
	11	7								
	11	42	236	83						

AQUIFER WELL TEST RECORD

BGW Sheet of
 Test Date
 Drawdown/Recovery
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time
 Starting Rate
 Static at Start

Well ID. OW-C Shallow Piez
 Location
 Collected By

Rate Control
 Measuring Point
 Pump Intake (ft.)

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
11	14	06								
11	44		236	56						
11	21	06								
14	11		236	81						
11	28	06								
14	20		236	67						
12	5	06								
13	03		236	85						
12	12	06	236	93						
12	02									
12	27	06								
15	04		236	70						
1	30	07								
14	30		235	55						
4	8	07								
6	36		236	64						
2	26	07								
14	01		236	76						
2	26	07								
12	50		236	59						
2	27									
08	56		236	77						
10	12		236	77						
11	56		236	77						
13	36		236	80						
2	28	07								
11	30		236	63						
3	6	07								
16	35		236	63						
14	21		236	56						

Production / Exploratory
Well Test Records

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

257.31

Well ID. CCD-PI
 Location RV
 Collected By _____

Rate Control _____
 Measuring Point east near tube
 Pump Intake (ft.) = 0.71 ft above concrete pad

Clock Time (24hrs)			Hold Unit	+	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
8	17	06								
10	35		250	-1.36	248.64	+0.28				solinst 300 (needs correction)
8	23	06								
14	08				248.68	+ 28 = 248.96				set transducer s/n 7137 (100 psi) to 430.22 ft 181.28 + 248.96
8	28	06								
08	55				257.31	+ .28 =				sol 300
9	1	06								
12	10				294.85					"
9	18	06								
15	05				303	82	sol	500		
10	3	06								
16	30				313	90	sol	500		changed batt on x-ducer, pulled x-ducer
10	14	06								
16	40				314	20	sol	500		
10	5	06								
17	55				314	10	sol	500		installed rental x-ducer, set repaired x-ducer
10	10	06								
10	17	06								started new test
14	06				315	45	sol	500		
12	12	06								
13	18				317	29				
1	10	07								
08	10									
2	8	07								
16	09				328	36				pulled x-ducer, changed batt, reset on 2/9
2	26	07								
14	04				317	54				

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. CCD-X1 (5 inch)
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point to c
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
8	10	06								
	16	00	246	09	28	=	246.37			Solmsr 300
8	23									Set transducer 7303 (100 psi)
14	39		246	07			246.35			10 ~ 300 ft ↙ 338.97
8	28									
08	42		249	46			249.74			col 300
9	1	06								
12	00		275	34						sol 300
9	18									
15	29		285	31						Sol 500
10	3	06								
	15	55	295	80						"
10	10	06								changed batt in x-ducer.
10	17	06								
14	27		297	22						Sol 500
12	12	06								
13	31		297	56						
1	10	07								
07	40		300	29						
2	26	07								
14	10		299	90						
2	27	07								moved transducer up ~ 20 ft

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. CCD-71 Shal Piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	-	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec						t	t'	t/t'	
	8	12					Corrected				
16	15		231	37		0.28	231.65				sol inst 300
8	23										
14	41		231	33			231.61				"
8	23										
8	46		232	40			232.68				"
8	30										
11	13		236	34			236.62				"
9	1	06									
12	06		238	00			238.28				"
9	5	06									
10	41		239	42			240.20				"
	9	8									
15	23		241	20							sol 500
9	12	06									
10	41		241	68							"
9	19	06									
12	35		243	49							"
9	26	06									
14	09		243	96							"
10	2	06									
15	39		244	76							"
10	10	06									
13	03		245	05							"
10	17	06									
14	22		245	48							"
10	24	06									
13	57		246	02							
10	31	06									
12	21		245	78							
11	07	06									
	13	02	245	88							

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. CCD-X1 shall Piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
11/14/06										
12	44		245	73						solinst 500'
11/21/06										
15	44		245	91						"
11/28/06										
15	21		245	98						
12/5/06										
14	01		246	14						
12/12/06										
13	29		246	109						
12/27/06										
15	18		246	10						"
1/16/07										
07	35		246	04						
1/25/07										
14	00		246	65						
1/30/07										
13	05		245	65						
2/9/07										
14	16		246	51						
2/20/07										
12	18		245	81						
2/26/07										
14	11		246	24						
2/27/07										
9	35		246	22						
10	54		245	73						
12	44		245	43						
2/28/07										
12	08		244	21						

3/6/07
 15 43
 3/13/07
 241 60
 239.71

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. CCD-X1 Deep Piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t ¹	t/t ¹	
8	10	06				<u>Corrected</u>				
16	20		233	27	+ 0.28	233.55				sol 300
8	23									
16	44		233	15		233.43				"
8	28									
08	48		233	25		233.53				"
8	30									
16	19		233	26		233.54				"
9	1	06								
12	03		233	27		233.55				"
9	5	06								
10	45		233	26		233.54				"
	9	13								
15	26		233	39						sol 500
9	12	06								
10	43		233	39						"
9	19	06								
12	39		233	45						"
9	26	06								
14	07		233	45						"
10	3	06								
15	41		233	61						"
10	10	06								
12	59		233	54						"
10	17	06								
14	25		233	58						
10	24	06								
14	01		233	60						
10	31	06								
12	17		233	61						
11	7	06								
	13	05	233	63						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4 _____

Tape, M-scope, airline _____

Start Time _____

Starting Rate _____

Static at Start _____

Well ID. CCD-X1 Deep Pier

Location _____

Collected By _____

Rate Control _____

Measuring Point _____

Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
11/14/06										
12	42		233	67						solinst 500'
11/21/06										
15	42		233	69						
11/28/06										
15	24		233	74						
12/5/06										
14	04		233	89						
12/12/06										
13	27		233	91						
12/27										
13:22			233	98						
6/10/07										
07	37		234	00						
1/29/07										
13	56		234	02						
1/30/07										
13	08		233	16						
2/8/07										
14	15		234	11						
2/20/07										
12	21		234	22						
2/26/07										
14	12		234	08						
2/27/07										
9	33		234	09						
2/27/07										
10	51		234	11						
12	47		234	11						
2/28/07										
11	05		234	17						

12/3/07
15:45
3/13/07
11:12

234.15
234.20

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Outlying Observation
Well Test Records

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4 _____

Tape, M-scope, airline _____

Start Time _____

Starting Rate _____

Static at Start _____

 Well ID. E1 Rancho Well
 Location RV
 Collected By _____

 Rate Control _____
 Measuring Point top case plate
 Pump Intake (ft.) ~ flush w/
ground level

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t ¹	t/t ¹	
8	10	06								
11	38		213	85						
8	17	06								
14	10		213	90						sol. nr 300
8	24									
17	00		213	70						"
8	24									set transducer s/n 106606
09	35		213	97						(rental) to 231.84 232.12 ft
9	12									
12	54		214	00						sol 500 pulled transducer
9	19	06								
12	54		214	03						"
9	26	06								
14	25		213	95						"
10	8	06								
16	12		214	00						sol 500
10	10	06								
15	16		214	16						"
10	17	06								
14	38		214	17						"
10	24	06								
14	19		213	99						"
10	31	06								
13	37		214	18						"
11	07	06								
12	25		214	15						"
11	14	06								
12	18		214	06						
11	21	06								
15	16		214	06						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. E1 Rancho Well
 Location R.V.
 Collected By _____

Rate Control _____
 Measuring Point top cover plate
 Pump Intake (ft.) Flush w/ground lvl

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
11	28	06								
14	52		214	14						
12	15	06								
16	36		214	04						
12	12	06								
12	43		214	31						
12	27	06								
10	30		214	00						vane open - I closed it and
1	10	07								wired it down
11	00		214	05						vane closed
11	25	07								
13	24		214	12						
2	8	07								
14	37		214	08						
2	20	07								
14	49		213	94						
2	26	07								
13	25		214	13						
2	27	07								
10	36		214	20						
13	17		214	11						
2	29	07								
11	49		213	97						
3	6	07								
			214	10						
3	13	07								
15	50		214	04						windmill turning - small amount of water coming out

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. S FCC well
 Location S FCC
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
9	15									
13	15				230	87				
9	12									
13	15				228	40				
9	19	06								
13	27				229	50				
9	26	06								
15	58				228	25				
10	3	06								
17	02				229	25				
10	10	06								
15	28				228	55				
10	17	06								
15	38				228	36				
10	24	06								
14	55				227	09				
10	31	06								
13	27				227	30				
11	07	06								
12	35				227	00				
11	14	06								
12	53				226	81				
11	21	06								
16	10				227	10				
11	28	06								
15	47				226	78				
12	5	06								
17	06				226	71				
12	12	06								
14	12				226	82				

12/27/06
11:30

226 59

1/10/07 9:00

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226.54

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4
 Tape, M-scope, airline
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. SFCC Well
 Location SFCC
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
1	25									
14	12		226	69						
1	30									
13	20		226	55						
2	8									
16	48		226	55						
2	20									
15	21		226	54						
2	26									
13	34		226	54						
2	27									
11	00		226	59						
12	55		226	56						
15	23		226	55						
2	28		226	47						
12	25		226	47						
3	2		226	62						
8	38									
3	6									
11	35		226	50						
3	13									
16	26		226	42						

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. Rancho V. Obs Well
 Location KV
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
8	10	06								
8	15	20	205	10						solinst 300 Powers 1000
8	17	06								
8	11	30	205	10						solinst 300
			430	2						set xducer s/n 106615 30psi
8	8	26	235	20						(renul) to 235.30 ft.
8	10	04	205	10						solinst 300
9	1	12								
12	12	10	205	25						sol 500
10	10	3								
10	16	34	205	49						
10	10	17								
		1456	205	08						sol 500
10	10	24								
10	14	35	205	05						"
10	10	31								
10	13	56	205	67						"
11	11	07								
11	12	02	205	82						" pulled x-ducer
11	11	14								
11	12	02	205	71						
11	11	21								
11	15	00	205	49						
11	11	28								
11	14	34	205	66						
12	12	5								
12	16	23	205	20						Vane on windmill is closed
12	12	12								
12	12	28	205	13						
12	12	17								
12	10	00	204	97						Vane closed

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4 _____

Tape, M-scope, airline _____

Start Time _____

Starting Rate _____

Static at Start _____

Well ID. Rancho Viejo Obs Well

Location R.V.

Collected By _____

Rate Control _____

Measuring Point _____

Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	-	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.	
Hr	Min	Sec						t	t'	t/t'		
2/9	10	07										
14	16		204	94								
2/26	07											
14	22		204	84								
2/26	10											
13	50		203	92								
2/27	07											
11	24		203	97			"	"				
3/13	07											
15	16		205	45			solinst					
												Windmill operating setting xducer S/N 107472 (10 psi) to ~350 ft.

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 _____
 Tape, M-scope, airline _____
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. La Cienega
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
10/24/06										
11	30		225	50						Powers 500
10/31/06										
13	09		224	29						"
11/07/06										
13	20		225	41						"
11/14/06										
14	14		225	16						"
11/21/06										
15	57		225	39						"
11/28/06										
15	36		225	17						Powers 1000
12/14/06										
16	54		225	67						pow 500
12/18/06										
13	50		225	33						pow 500
12/27/06										
11	00		225	79						5-line Powers 500 Valve closed
2/8/07										
15	24		225	93						
2/20/07										
15	06		225	54						
2/26/07										
13	47		225	78						
2/27/07										
11	12		225	84						cont get
										3/12/07 cont get lock open - changed combo?

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
Test Date _____
Drawdown/Recovery
Step 1-2-3-4
Tape, M-scope, airline
Start Time _____
Starting Rate _____
Static at Start _____

CCD-P1

Well ID. CCD-P1
Location _____
Collected By _____

Rate Control _____
Measuring Point _____
Pump Intake (ft.) _____

Clock Time	Hold Unit	+ -	Depth to Water	Drawdown or Recovery.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
					t	t ⁱ	t/t ⁱ	
5/25/07								
10 00	256	41						Water level moving up and down with wind gusts (?)
								pulling BGW reducer setting BV reducer S/N ~ 350 ft
7/3/07								
12 35	254	80						
12 38	254	79						piezometer?

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4 _____

Tape, M-scope, airline 50/mis + 500

Start Time _____ unless noted otherwise

Starting Rate _____

Static at Start _____

Well ID. lnjwell Shal Piez
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point toc
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
3	13	07	315	73						
14	06									
3	13	07								
09	25		315	89						
5	25	07								
12	46		315	90						
3/07/11	20		315	81						
15	00		315	80						9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4

Tape, Microscope, airline

Start Time _____

Starting Rate _____

Static at Start _____

*50 inst
500*

Well ID. Inj Well Deep Pier
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point to c
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
hr	Min	Sec					t	t'	t/t'	
1	13	07								
4	12		273	35						
3	20	07								
09	35		285	34						
5	25	07								
12	50		290	48						
7	3	07	29	73						
1	24		291	73						
1	32		293	04						
5	03		292	73						<i>inj well 12" casing 9/19/07</i>

AQUIFER/WELL TEST RECORD

BGW Sheet of

Test Date

Drawdown/Recovery

Step 1-2-3-4

Tape, M-scope, airline

*solinst
500*

Start Time

Starting Rate

Static at Start

OW-A Shallow

Well ID. ~~OW-A~~ *OW-A*

Location

Collected By

Rate Control

Measuring Point ~~past screen tube~~

Pump Intake (ft.)

0.71 ft above screen

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
3	30	07								Note - transducer was tested removed on Mar. 13
8	45		286	00						
5	25	07								
12	56		291	70						
<u>7</u>	<u>3</u>	<u>07</u>								
11	49		292	98						shallow
11	46		288	55						OWA deep piezometer
11	52		292	60						OWA intermediate
15	20		293	97						9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet __ of __

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4

Tape, M-scope airline Solim str
500

Start Time _____

Starting Rate _____

Static at Start _____

15 Well ID. DW-13 Shal Piez
Location _____
Collected By _____

Rate Control _____

Measuring Point _____

Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
5	30	07								
09	55		292	12						
5	25	07								
13	05		292	94						
7	3	07								
12	01		293	14						
12	04		295	60						5" casing
15	50		293	07						9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___

Test Date _____

Drawdown/Recovery _____

Step 1-2-3-4 _____

Tape, M-scope, airline _____

*sol in st
500*

Start Time _____

Starting Rate _____

Static at Start _____

Well ID. DW-C Shal Piez

Location _____

Collected By _____

Rate Control _____

Measuring Point _____

Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	-	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.	
Hr	Min	Sec						t	t'	t/t'		
3	30	07										
10	15		236	62								
5	25	07										
13	12		236	74								
7	3	07										
12	10		236	54								shal piez
12	12		249	89								5" casing
14	40		233	81								9/19/07 By (CCD-X1 Deep level)
15	38		237	02								9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet of

Test Date

Drawdown/Recovery

Step 1-2-3-4

Tape M-scope, airline

Solinst-500

Start Time

Starting Rate

Static at Start



Well ID. CO-41 Shallow piez

Location

Collected By

Rate Control

Measuring Point

Pump Intake (ft.)

Clock Time (24hrs)			Hold Unit	+	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec		-			t	t'	t/t'	
3	30	07								
10	50		237		80					
5	25	07								
10	25		235		90					
7	3	08								
12	46		251		25	B1				5" depth, moved measurement to correct sheet
12	49		235		44					Shallow piez
14	38		235		03					9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
Test Date _____
Drawdown/Recovery _
Step 1-2-3-4
Tape, M-scope, airline
Start Time _____
Starting Rate _____
Static at Start _____

Well ID. CCD-X1 main CSG Rate Control _____
Location _____ Measuring Point _____
Collected By _____ Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time t t' t/t'			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec								
5	25	00	252	61						
7	7	00								
12	46		251	25						
14	35		249	99						9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4
 Tape. M scope, airline 50/mst
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. CD-X1 Deep Pic
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+	-	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec						t	t'	t/t'	
3	30	57									
10	52		234	17							
7	3	07									
12	51		233	99							
14	40		233	81							9/19/07

AQUIFER/WELL TEST RECORD

BGW Sheet of

Test Date

Drawdown/Recovery

Step 1-2-3-4

Tape, ~~M-scope~~ airline

Start Time

Starting Rate

Static at Start

Solinst
300

Well ID. SFCC well
Location
Collected By

Rate Control

Measuring Point

Pump Intake (ft.)

Clock Time (24hrs)			Hold Unit	+ - DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
hr	Min	Sec				t	t'	t/t'	
<i>3</i>	<i>38</i>	<i>07</i>							
	<i>1:06</i>		<i>226</i>	<i>41</i>					
<i>1</i>	<i>18</i>	<i>07</i>							

AQUIFER/WELL TEST RECORD

BGW Sheet __ of __
 Test Date _____
 Drawdown/Recovery _____
 Step 1-2-3-4 50/150
 Tape, M-scope, airline 500
 Start Time _____
 Starting Rate _____
 Static at Start _____

Well ID. E1 Ranch Well
 Location _____
 Collected By _____

Rate Control _____
 Measuring Point _____
 Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ - DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec				t	t'	t/t'	
3	30	07							
11	20		214	22					windmill turning, small amount of water produced
7	3	07							
12	24		224	11					

AQUIFER/WELL TEST RECORD

BGW Sheet ___ of ___
Test Date _____
Drawdown/Recovery _____
Step 1-2-3-4 _____
Tape, M-scope, airline _____
Start Time _____
Starting Rate _____
Static at Start _____

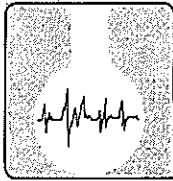
Well ID. RV Obs Well
Location _____
Collected By _____

Rate Control _____
Measuring Point _____
Pump Intake (ft.) _____

Clock Time (24hrs)			Hold Unit	+ -	DTW	DD or Recov.	Elapsed Time			Remarks: static, start, end, Δ rate, sample, etc.
Hr	Min	Sec					t	t'	t/t'	
09	20	51.25/07	205	20						windmill off; pulling xducer setting 205.20 + 146.57 = 351.77 ft

APPENDIX G

WATER ANALYSES



ASSAIGAI ANALYTICAL LABORATORIES, INC.

4301 Masithead NE • Albuquerque, New Mexico 87109 • (505) 345-8964 • FAX (505) 345-7259

3332 Wedgewood, Ste. N • El Paso, Texas 79925 • (915) 593-6000 • FAX (915) 593-7820

127 Eastgate Drive, 212-C • Los Alamos, New Mexico 87544 • (505) 662-2558

Explanation of codes

B	Analyte Detected in Method Blank
E	Result is Estimated
H	Analyzed Out of Hold Time
N	Tentatively Identified Compound
S	Subcontracted
1-9	See Footnote

BALLEAU GROUNDWATER
attn: CASEY COOK
901 RIO GRANDE BLVD NW SUITE F-242
ALBUQUERQUE NM 87104

STANDARD

Assaigai Analytical Laboratories, Inc.

Certificate of Analysis

All samples are reported on an "as received" basis, unless otherwise noted (i.e. - Dry Weight).

Client: **BALLEAU GROUNDWATER**
Project: **RANCHO VIEJO**
Order: **0702694 BAL01** Receipt: **02-26-07**

William P. Biays
William P. Biays, President of Assaigai Analytical Laboratories, Inc.

Sample: **CCDP1** Collected: **02-26-07 14:30:00** By: **CC**
Matrix:

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0702694-0001A EPA 120.1 Specific Conductance By: MJN										
WCOND-07-007	WC.2007.538.4	10-34-4	Conductivity	230	umhos/cm	1	1		03-07-07	03-07-07
0702694-0001A EPA 150.1 pH, Electrometric By: RKA										
WPH07027	WC.2007.488.1	10-29-7	pH	8.20	units	1	0.1		02-27-07	02-27-07
WPH07027	WC.2007.488.1		sample temperature @	12.7	deg C	1	0		02-27-07	02-27-07
0702694-0001A EPA 160.1 Total Dissolved Solids By: MJN										
WTDS-07-018	WC.2007.479.15	10-33-3	Total Dissolved Solids	145	mg/L	1	10		02-28-07	03-01-07
0702694-0001A EPA 300.0 Anions by IC By: JJK										
W07154	WC.2007.494.7	16887-00-6	Chloride	1.52	mg/L	5	0.05		02-27-07	02-27-07
W07154	WC.2007.494.7	16984-48-8	Fluoride	ND	mg/L	5	0.05		02-27-07	02-27-07
W07154	WC.2007.494.7	14797-65-0	Nitrate, as N	0.645	mg/L	5	0.05		02-27-07	02-27-07
W07154	WC.2007.494.7	14797-55-8	Nitrite, as N	ND	mg/L	5	0.05		02-27-07	02-27-07
W07154	WC.2007.494.7	14808-79-8	Sulfate	11.8	mg/L	5	0.05		02-27-07	02-27-07
0702694-0001A EPA 310.1 Alkalinity, Titrimetric By: RKA										
WALK07016	WC.2007.505.10	T-005	Alkalinity, Total	108	mg/L	1	2		03-05-07	03-05-07
0702694-0001A SM 2330B By: JPM										
LANGL	WC.2007.695.1		Langlier Saturation Index	0.11	%	1	0		03-22-07	03-22-07
0702694-0001B EPA 4.1.3/200.7 ICP By: AZC										
M07248	MT.2007.413.39	7440-70-2	Calcium	22.5	mg/L	10	0.5		03-12-07	03-13-07
M07202	MT.2007.348.22	7439-95-4	Magnesium	1.43	mg/L	1	0.5		03-01-07	03-02-07
M07248	MT.2007.447.46	7440-09-7	Potassium	1.44	mg/L	1	0.5	1	03-12-07	03-19-07
M07202	MT.2007.348.27	7440-23-5	Sodium	27.8	mg/L	10	0.5		03-01-07	03-02-07

Assagai Analytical Laboratories, Inc.

Certificate of Analysis

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Client: **BALLEAU GROUNDWATER**
 Project: **RANCHO VIEJO**
 Order: **0702694 BAL01** Receipt: **02-26-07**

Sample: **CCDP1** Collected: **02-26-07 14:30:00** By: **CC**

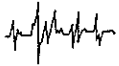
Matrix:

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
EPA 11.2.2/200.8 Metals by ICP-MS By: DPA										
0702694-0001B										
M07198	MT.2007.369.27	7440-38-2	Arsenic	0.0049	mg/L	1	0.001		03-01-07	03-06-07
SM 2340B By: JPM										
0702694-0001B										
HARD	MT.2007.477.1		Hardness, as CaCO3	62	mg/L	1	0		03-23-07	03-23-07
SW846 5030B/8260B Purgeable VOCs by GC/MS By: EJB										
0702694-0001C										
V07120	XG.2007.291.12	67-66-3	Chloroform	ND	ug/L	1	1		02-27-07	02-27-07

Unless otherwise noted, all samples were received in acceptable condition and all sampling was performed by client or client representative. Sample result of ND indicates Not Detected, ie result is less than the sample specific Detection Limit. Sample specific Detection Limit is determined by multiplying the sample Dilution Factor by the listed Reporting Detection Limit. All results relate only to the items tested. Any miscellaneous workorder information or footnotes will appear below.

Analytical results are not corrected for method blank or field blank contamination.

1 The LCS is outside QC criteria at 116.8 percent for K. This should be taken into account when reviewing the data.



ASSAIGAI ANALYTICAL LABORATORIES, INC.

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Explanation of codes

B	Analyte Detected in Method Blank
E	Result is Estimated
H	Analyzed Out of Hold Time
N	Tentatively Identified Compound
S	Subcontracted
1-9	See Footnote

BALLEAU GROUNDWATER
attn: **CASEY COOK**
901 RIO GRANDE BLVD NW SUITE F-242
ALBUQUERQUE NM 87104

STANDA

Assaigai Analytical Laboratories, Inc.

Certificate of Analysis

All samples are reported on an "as received" basis, unless otherwise noted (i.e. - Dry Weight).

Client: **BALLEAU GROUNDWATER**
Project: **INJECTION WELL**
Order: **0605465 BAL01** Receipt: **05-19-06**

William P. Biava, President of Assaigai Analytical Laboratories, Inc.

Sample: **RV CCD-11** Collected: **05-19-06 10:30:00** By: **CC**
Matrix: **DW**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
EPA 150.1 pH, Electrometric By: NJL										
WPH06076	WC.2006.1254.1	10-29-7	pH	8.36	units	1	0.1		05-19-06	05-19
WPH06076	WC.2006.1254.1		sample temperature @	18.8	deg C	1	0		05-19-06	05-19
EPA 160.1 Total Dissolved Solids By: MJN										
WTDS-06-056	WC.2006.1301.11	10-33-3	Total Dissolved Solids	167	mg/L	1	10		05-24-06	05-25
EPA 180.1 Turbidity, Nephelometric By: MJN										
WTURB-06-040	WC.2006.1237.2	10-08-02	Turbidity	0.59	NTU	1	0.3		05-19-06	05-19
EPA 300.0 Anions by IC By: JTK										
W06378	WC.2006.1265.4	16887-00-6	Chloride	1.65	mg/L	5	0.05		05-19-06	05-19
W06378	WC.2006.1265.4	16984-48-8	Fluoride	ND	mg/L	5	0.05		05-19-06	05-19
W06378	WC.2006.1265.4	14797-65-0	Nitrate, as N	0.260	mg/L	5	0.05		05-19-06	05-19
W06378	WC.2006.1265.4	14797-55-8	Nitrite, as N	ND	mg/L	5	0.05		05-19-06	05-19
W06378	WC.2006.1265.4	14808-79-8	Sulfate	13.1	mg/L	5	0.05		05-19-06	05-19
EPA 310.1 Alkalinity, Titrimetric By: NJL										
WALK06023	WC.2006.1328.2	71-52-3	Alkalinity, Bicarbonate	112	mg/L	1	2		05-30-06	05-30
WALK06023	WC.2006.1328.2	3812-32-6	Alkalinity, Carbonate	ND	mg/L	1	2		05-30-06	05-30
WALK06023	WC.2006.1328.2	T-005	Alkalinity, Total	112	mg/L	1	2		05-30-06	05-30
SM 2120B By: MJN										
WCOLOR-06-029	WC.2006.1239.2		Color	ND	APHA	1	5		05-19-06	05-19
SM 2330B By: JPM										
LANGL	WC.2006.1529.1		Langlier Saturation Index	0.14	%	1	0		06-23-06	06-23

Certificate of Analysis

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Client: **BALLEAU GROUNDWATER**
 Project: **INJECTION WELL**
 Order: **0605465 BAL01** Receipt: **05-19-06**

Sample: **RV CCD-11** Collected: **05-19-06 10:30:00** By: **CC**
 Matrix: **DW**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date	
0605465-0001B			EPA 4.1.3/200 series AA-FL					By: DPA			
M06550	MT.2006.1007.19	7440-23-5	Sodium	44.8	mg/L	10	1		05-24-06	06-0	
0605465-0001B			EPA 4.1.3/200.7 ICP					By: TGA			
M06538	MT.2006.952.37	7440-70-2	Calcium	13.4	mg/L	1	0.5		05-23-06	05-2	
M06538	MT.2006.952.37	7439-95-4	Magnesium	1.33	mg/L	1	0.5		05-23-06	05-2	
0605465-0001B			EPA 11.2.2/200.8 Metals by ICP-MS					By: BAS			
M06550	MT.2006.958.24	7429-90-5	Aluminum	0.0160	mg/L	1	0.01		05-24-06	05-2	
M06550	MT.2006.999.11	7440-36-0	Antimony	ND	mg/L	1	0.005		05-24-06	06-0	
M06550	MT.2006.958.24	7440-38-2	Arsenic	0.0101	mg/L	1	0.001		05-24-06	05-2	
M06550	MT.2006.1006.20	7440-39-3	Barium	0.116	mg/L	1	0.0005		05-24-06	06-0	
M06550	MT.2006.1006.20	7440-41-7	Beryllium	ND	mg/L	1	0.0005		05-24-06	06-0	
M06550	MT.2006.958.24	7440-43-9	Cadmium	ND	mg/L	1	0.0005		05-24-06	05-2	
M06550	MT.2006.958.24	7440-47-3	Chromium	0.0042	mg/L	1	0.001		05-24-06	05-2	
M06550	MT.2006.958.24	7440-50-8	Copper	0.0057	mg/L	1	0.001		05-24-06	05-2	
M06550	MT.2006.958.24	7439-89-6	Iron	ND	mg/L	1	0.01		05-24-06	05-2	
M06550	MT.2006.980.23	7439-92-1	Lead	0.0011	mg/L	1	0.0005		05-24-06	05-3	
M06550	MT.2006.958.24	7439-96-5	Manganese	0.0029	mg/L	1	0.0005		05-24-06	05-2	
M06550	MT.2006.958.24	7440-02-0	Nickel	0.0005	mg/L	1	0.0005		05-24-06	05-2	
M06550	MT.2006.958.24	7782-49-2	Selenium	ND	mg/L	1	0.005		05-24-06	05-2	
M06550	MT.2006.958.24	7440-22-4	Silver	ND	mg/L	1	0.0005		05-24-06	05-2	
M06550	MT.2006.995.36	7440-28-0	Thallium	ND	mg/L	1	0.0005		05-24-06	05-3	
M06550	MT.2006.1006.20	7440-61-1	Uranium	0.0027	mg/L	1	0.0005		05-24-06	06-0	
M06550	MT.2006.1006.20	7440-66-6	Zinc	0.0110	mg/L	1	0.005		05-24-06	06-0	
0605465-0001B			EPA 245.1 Mercury by CVAA					By: BAS			
M06569	MT.2006.992.34	7439-97-6	Mercury	ND	ug/L	1	0.2		05-31-06	05-3	
0605465-0001B			SM 2340B					By: JPM			
M06538	MT.2006.1122.1		Hardness, as CaCO3	39	mg/L	1	0		06-22-06	06-2	
0605465-0001C			EPA 100.2					By: JM			
QTM137003	SB.2006.241.1		Amphibole Asbestos	ND	MFL	1	0.123	S	05-24-06	05-2	
QTM137003	SB.2006.241.1		Chrysotile Asbestos	ND	MFL	1	0.123	S	05-24-06	05-2	
0605465-0001D			EPA 900					By: TS			
ARS10600989	SB.2006.217.3		Gross Alpha	2.0619+/- 0.7532	pCi/L	1	0	S	06-04-06	06-0	
ARS10600989	SB.2006.217.3		Gross Beta	2.1625+/- 0.6321	pCi/L	1	0	S	06-04-06	06-0	
0605465-0001D			EPA 903					By: KP			
ARS010600989	SB.2006.247.2		Radium-226	-0.0003+/- 0.0003	pCi/L	1	0	S	05-30-06	05-3	
0605465-0001D			EPA 904					By: KP			
ARS10600989	SB.2006.246.2		Radium-228	0.2400+/- 0.3600	pCi/L	1	0	S	05-30-06	05-3	

Certificate of Analysis

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Client: **BALLEAU GROUNDWATER**
 Project: **INJECTION WELL**
 Order: **0605465 BAL01** Receipt: **05-19-06**

Sample: **RV CCD-11** Collected: **05-19-06 10:30:00** By: **CC**
 Matrix: **DW**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date	
0605465-0001E			Glyphosate by EPA 547					By: CAS			
CASK0604160	SB.2006.226.1		Glyphosate	ND	ug/L	1	6	S	05-30-06	05-	
0605465-0001F			EPA 140.1 Threshold Odor					By: MJN			
WODOR-06-029	WC.2006.1238.2		Odor	No detectable odor	TON	1	1		05-19-06	05-	
0605465-0001G			Haloacetic Acids by EPA 552.2					By: CAS			
CASK0604160	SB.2006.231.1		Bromoacetic Acid	ND	ug/L	1	1	S	05-30-06	05-	
CASK0604160	SB.2006.231.1		Chloroacetic Acid	ND	ug/L	1	2	S	05-30-06	05-	
CASK0604160	SB.2006.231.1		Dibromoacetic Acid	ND	ug/L	1	1	S	05-30-06	05-	
CASK0604160	SB.2006.231.1		Dichloroacetic Acid	ND	ug/L	1	1	S	05-30-06	05-	
CASK0604160	SB.2006.231.1		Trichloroacetic Acid	ND	ug/L	1	1	S	05-30-06	05-	
0605465-0001H			Chlorinated Acids by EPA 515.4					By: CAS			
CASK0604160	SB.2006.222.1		2,4,5-TP (Silvex)	ND	ug/L	1	0.05	S	05-24-06	05-	
CASK0604160	SB.2006.222.1		2,4-D	ND	ug/L	1	0.1	S	05-24-06	05-	
CASK0604160	SB.2006.222.1		Dalapon	ND	ug/L	1	0.54	S	05-24-06	05-	
CASK0604160	SB.2006.222.1		Dinoseb	ND	ug/L	1	0.2	S	05-24-06	05-	
CASK0604160	SB.2006.222.1		Pentachlorophenol	ND	ug/L	1	0.04	S	05-24-06	05-	
CASK0604160	SB.2006.222.1		Picloram	ND	ug/L	1	0.1	S	05-24-06	05-	
0605465-0001H			EPA 335.4					By: CAS			
CASK0604160	SB.2006.228.1		Cyanide, Total	ND	mg/L	1	0.01	S	05-26-06	05-	
0605465-0001I			Endothall by EPA 548.1					By: CAS			
CASK0604160	SB.2006.227.1		Endothall	ND	ug/L	1	5	S	05-23-06	05-	
0605465-0001J			ASTM D2330-88					By: ECC			
W06397	WC.2006.1314.4		Surfactants	0.14	mg/L	1	0.03		05-26-06	05-	
0605465-0001K			Pesticides/PCBs by EPA 508.1					By: CAS			
CASK0604160	SB.2006.232.1		Aroclor 1016	ND	ug/L	1	0.05	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Aroclor 1221	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Aroclor 1232	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Aroclor 1242	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Aroclor 1248	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Aroclor 1254	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Aroclor 1260	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Chlordane	ND	ug/L	1	0.099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Endrin	ND	ug/L	1	0.0099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		gamma-BHC (Lindane)	ND	ug/L	1	0.0099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Heptachlor	ND	ug/L	1	0.0099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Heptachlor Epoxide	ND	ug/L	1	0.0099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Methoxychlor	ND	ug/L	1	0.0099	S	06-02-06	06-0	
CASK0604160	SB.2006.232.1		Toxaphene	ND	ug/L	1	0.099	S	06-02-06	06-0	
0605465-0001L			EPA Method 525.2					By: CAS			
CASK0604160	SB.2006.224.1		Alachlor	ND	ug/L	1	0.71	S	06-02-06	06-1	

Certificate of Analysis

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Client: **BALLEAU GROUNDWATER**
 Project: **INJECTION WELL**
 Order: **0605465 BAL01** Receipt: **05-19-06**

Sample: **RV CCD-11** Collected: **05-19-06 10:30:00** By: **CC**
 Matrix: **DW**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date	
0605465-0001L		EPA Method 525.2							By: CAS		
CASK0604160	SB.2006.224.1		Atrazine	ND	ug/L	1	0.99	S	06-02-06	06-11	
CASK0604160	SB.2006.224.1		Benzo(a)pyrene	ND	ug/L	1	0.02	S	06-02-06	06-11	
CASK0604160	SB.2006.224.1		Bis(2-ethylhexyl) Adipate	ND	ug/L	1	0.5	S	06-02-06	06-11	
CASK0604160	SB.2006.224.1		Bis(2-ethylhexyl) Phthalate	ND	ug/L	1	0.5	S	06-02-06	06-11	
CASK0604160	SB.2006.224.1		Hexachlorobenzene	ND	ug/L	1	0.5	S	06-02-06	06-11	
CASK0604160	SB.2006.224.1		Hexachlorocyclopentadiene	ND	ug/L	1	0.099	S	06-02-06	06-11	
CASK0604160	SB.2006.224.1		Simazine	ND	ug/L	1	0.5	S	06-02-06	06-11	
0605465-0001M		Method 1613b							By: CAS		
CASK0604160	SB.2006.267.1		2, 3, 7, 8-TCDD	ND	pg/L	1	0.152	S	06-20-06	06-21	
0605465-0001N		Diquat by EPA 549.2							By: CAS		
CASK0604160	SB.2006.229.1		Diquat	ND	ug/L	1	0.4	S	05-23-06	06-01	
0605465-0001O		EPA 531.1							By: CAS		
CASK0604160	SB.2006.225.1		Aldicarb	ND	ug/L	1	0.5	S	05-23-06	05-21	
CASK0604160	SB.2006.225.1		Aldicarb Sulfone	ND	ug/L	1	0.5	S	05-23-06	05-21	
CASK0604160	SB.2006.225.1		Aldicarb Sulfoxide	ND	ug/L	1	0.5	S	05-23-06	05-21	
CASK0604160	SB.2006.225.1		Carbofuran	ND	ug/L	1	0.5	S	05-23-06	05-21	
CASK0604160	SB.2006.225.1		Oxamyl	ND	ug/L	1	0.5	S	05-23-06	05-21	
0605465-0001P		EPA 524 PURGEABLE VOCs by GC/MS							By: CAS		
CASK0604160	XG.2006.818.1		1,1 Dichloroethane (SPCC)	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,1 Dichloroethene (CCC)	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,1,1 Trichloroethane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,1,1,2 Tetrachloroethane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,1,2 Trichloroethane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,1,2,2 Tetrachloroethane (SPCC)	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,1-Dichloropropene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2 Dibromoethane (EDB)	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2 Dichlorobenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2 Dichloroethane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2 Dichloropropane (CCC)	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2,3 Trichloropropane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2,3-Trichlorobenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2,4-Trichlorobenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2,4-Trimethylbenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,2-Dibromo-3-chloropropane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,3 Dichlorobenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,3,5-Trimethylbenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,3-Dichloropropane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		1,4 Dichlorobenzene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		2,2-Dichloropropane	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		2-Chlorotoluene	ND	ug/L	1	0.5		05-26-06	05-21	
CASK0604160	XG.2006.818.1		4-Chlorotoluene	ND	ug/L	1	0.5		05-26-06	05-21	

Certificate of Analysis

All samples are reported on an "as received" basis, unless otherwise noted (i.e. - Dry Weight).

Client: **BALLEAU GROUNDWATER**

Project: **INJECTION WELL**

Order: **0605465 BAL01**

Receipt: **05-19-06**

Sample: **RV CCD-11**

Collected: **05-19-06 10:30:00** By: **CC**

Matrix: **DW**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date	
0605465-0001P			EPA 524 PURGEABLE VOCs by GC/MS					By: CAS			
CASK0604160	XG.2006.818.1		Benzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Bromobenzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Bromochloromethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Bromodichloromethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Bromoform (SPCC)	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Bromomethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Carbon tetrachloride	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Chlorobenzene (SPCC)	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Chlorodibromomethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Chloroethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Chloroform (CCC)	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Chloromethane (SPCC)	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		cis-1,2 Dichloroethene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		cis-1,3 Dichloropropene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Dibromomethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Ethylbenzene (CCC)	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Hexachlorobutadiene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Isopropylbenzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Methyl tert-Butyl Ether	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Methylene chloride	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Naphthalene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		n-Butylbenzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		n-Propylbenzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		O-Xylene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		P/M Xylenes	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		p-Isopropyltoluene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		sec-ButylBenzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Styrene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		T-1,2 Dichloroethene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		t-1,3 Dichloropropene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		tert-Butylbenzene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Tetrachlorethene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Toluene (CCC)	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Trichloroethene	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Trichloro fluoromethane	ND	ug/L	1	0.5		05-26-06	05-	
CASK0604160	XG.2006.818.1		Vinyl chloride (CCC)	ND	ug/L	1	0.5		05-26-06	05-	

0605465-0001Q

EPA 504 EDB/DBCP by GC/ECD

By: **W/RLG**

S06276	XG.2006.626.12	96-12-8	1,2-Dibromo-3-chloropropane	ND	ug/L	1	0.025		05-22-06	05-
S06276	XG.2006.626.12	106-93-4	1,2-Dibromoethane, EDB	ND	ug/L	1	0.025		05-22-06	05-

Certificate of Analysis

All samples are reported on an "as received" basis, unless otherwise noted (i.e. - Dry Weight).

Client: **BALLEAU GROUNDWATER**

Project: **INJECTION WELL**

Order: **0605465 BAL01** Receipt: **05-19-06**

Unless otherwise noted, all samples were received in acceptable condition and all sampling was performed by client or client representative. Sample result of ND indicates Not Detected, ie result is less than the sample specific Detection Limit. Sample specific Detection Limit is determined by multiplying the sample Dilution Factor by the listed Reporting Detection Limit. All results relate only to the items tested. Any miscellaneous workorder information or footnotes will appear below.

Analytical results are not corrected for method blank or field blank contamination.

MEMO: The analysis for gross alpha, gross beta, radium-226 and radium-228 was subcontracted to American Radiation Services.
The analysis for asbestos was subcontracted to Quantem Laboratories.
The analysis for EPA 547, EPA 552.2, EPA 515.4, EPA 335.4, EPA 548.1, EPA 508.1, EPA 552.2, EPA 1613, EPA 549.2, EPA 531.1, EPA 524.2 and EPA 504 was subcontracted to Columbia Analytical Services.



**ASSAIGAI
ANALYTICAL
LABORATORIES, INC.**

7300 Jefferson, NE • Albuquerque, New Mexico 87109 • (505) 345-8964 • FAX (505) 345-7259

3332 Wedgewood Dr., Suite N • El Paso, Texas 79925 • (915) 593-6000 • FAX (915) 593-7820
127 Eastgate Drive, 212-C • Los Alamos, New Mexico 87544 • (505) 662-2550

Explanation of codes

B	analyte detected in Method Blank
E	result is estimated
H	analyzed out of hold time
N	tentatively identified compound
S	subcontracted
1-9	see footnote

BALLEAU GROUNDWATER
attn: **CASEY COOK**
901 RIO GRANDE BLVD NW STE F242
ALBUQUERQUE NM 87104

STANDARD

Assaigai Analytical Laboratories, Inc.

Certificate of Analysis

Client: **BALLEAU GROUNDWATER**
Project: **RANCHO VIEJO**
Order: **0202125 RAN03** Receipt: **01-23-02**

[Signature]
William P. Buva, President of Assaigai Analytical Laboratories, Inc.

Sample: **CDPROD1/ RANCHO VIEJO**
Matrix: **AQ**

Collected: **01-23-02 13:00:00** By: **CWC**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0202125-01A		EPA 900						By: KP		
ARS020183	TT.2002.547.1		Gross Alpha	3.22+/-0.48	pCi/L	1	0.83	S	02-14-02	02-14-02
ARS020183	TT.2002.547.1		Gross Beta	1.43+/-0.53	pCi/L	1	1.44	S	02-14-02	02-14-02

Unless otherwise noted, all samples were received in acceptable condition and all sampling was performed by client or client representative. Sample result of ND indicates Not Detected, is result is less than the sample specific Detection Limit. Sample specific Detection Limit is determined by multiplying the sample Dilution Factor by the listed Reporting Detection Limit. All results relate only to the items tested. Any miscellaneous workorder information or footnotes will appear below.





ASSAIGAI ANALYTICAL LABORATORIES, INC.

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127 Eastgate Drive, 212-C • Los Alamos, New Mexico 87544 • (505) 662-2558

Explanation of codes

B	analyte detected in Method Blank
E	result is estimated
H	analyzed out of hold time
N	tentatively identified compound
S	subcontracted
1-9	see footnote

BALLEAU GROUNDWATER
attn: **CASEY COOK**
901 RIO GRANDE BLVD NW STE F242
ALBUQUERQUE NM 87104

STANDARD

Assaigai Analytical Laboratories, Inc.

Certificate of Analysis

Client: **BALLEAU GROUNDWATER**
Project:
Order: **0201283 RAN03** Receipt: **01-23-02**


William P. Davis, President of Assaigai Analytical Laboratories, Inc.

Sample: **CDPROD1/ RANCHO VIEJO**
Matrix: **AQ**

Collected: **01-23-02 12:12:00** By: **CWC**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-01A		SM-9223B						By: NL		
BT0220	TT.2002.251.3		E. coli, MMO/MUG	Absent	N/A	1	0		01-24-02	01-25-02
BT0220	TT.2002.251.3		Total Coliform, MMO/MUG	Present	N/A	1	0		01-24-02	01-25-02

Sample: **CDPROD1/ RANCHO VIEJO**
Matrix: **AQ**

Collected: **01-23-02 12:14:00** By: **CWC**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-02A		SM-9223B						By: NL		
BT0220	TT.2002.261.4		E. coli, MMO/MUG	Absent	N/A	1	0		01-24-02	01-25-02
BT0220	TT.2002.261.4		Total Coliform, MMO/MUG	Absent	N/A	1	0		01-24-02	01-25-02

Sample: **CDPROD1/ RANCHO VIEJO**
Matrix: **AQ**

Collected: **01-23-02 12:25:00** By: **CWC**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-03A		EPA 824.2						By: EHL		
EHL698255	TT.2002.507.1		Bromodichloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698255	TT.2002.507.1		Bromoform	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698255	TT.2002.507.1		Chloroform	0.8	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698256	TT.2002.507.1		Dibromochloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02



Assaigal Analytical Laboratories, Inc.
Certificate of Analysis

Client: **BALLEAU GROUNDWATER**

Project:

Order: **0201283 RAN03**

Receipt: **01-23-02**

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:50:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-04A		EPA 815.1		By: EHL						
EHL688256	TT.2002.514.1		2,4,5-TP (Silvex)	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL688256	TT.2002.514.1		2,4-D	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL688256	TT.2002.514.1		Dalapon	ND	ug / L	1	1	S	01-28-02	01-30-02
EHL688256	TT.2002.514.1		Dicamba	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL688256	TT.2002.514.1		Dinoseb	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL688256	TT.2002.514.1		Pentachlorophenol	ND	ug / L	1	0.04	S	01-28-02	01-30-02
EHL688256	TT.2002.514.1		Picloram (Tordon)	ND	ug / L	1	0.1	S	01-28-02	01-30-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:20:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-05A		EPA 548.1		By: EHL						
EHL688267	TT.2002.518.1		Endothall	ND	ug / L	1	9	S	01-28-02	01-31-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:30:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-06A		EPA 647		By: EHL						
EHL688258	TT.2002.517.1		Glyphosate (Round-up)	ND	ug / L	1	6	S	01-28-02	01-30-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:15:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-07A		EPA 624.2		By: EHL						
EHL688259	TT.2002.508.1		1,1,1,2-Tetrachloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,1,1-Trichloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,1,2,2-Tetrachloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,1,2-Trichloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,1-Dichloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688250	TT.2002.508.1		1,1-Dichloroethylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,1-Dichloropropylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,2,3-Trichlorobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,2,3-Trichloropropane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688259	TT.2002.508.1		1,2,4-Trichlorobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL688260	TT.2002.508.1		1,2,4-Trimethylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02

Assalgal Analytical Laboratories, Inc.
Certificate of Analysis

Client: **BALLEAU GROUNDWATER**

Project:

Order: **0201283 RAN03**

Receipt: **01-23-02**

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:15:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-07A		EPA 824.2						By: EHL		
EHL698259	TT.2002.508.1		1,2-Dibromo-3-Chloropropane	ND	ug / L	1	0.2	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,2-Dibromoethane(EDB)	ND	ug / L	1	0.2	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,2-Dichlorobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,2-Dichloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,2-Dichloropropane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,3,5-Trimethylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,3-Dichlorobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,3-Dichloropropane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		1,4-Dichlorobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		2,2-Dichloropropane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		2-Chlorotoluene (o-)	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		4-Chlorotoluene (p-)	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		4-Isopropyltoluene (p-)	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Benzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Bromobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Bromochloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Bromodichloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Bromoform	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Bromomethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Carbon tetrachloride	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Chlorobenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Chloroethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Chloroform	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Chloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		cis-1,2-Dichloroethylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		cis-1,3-Dichloropropylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Dibromochloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Dibromomethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Dichlorodifluoromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Dichloromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Ethylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Hexachlorobutadiene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Isopropylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Methyl-t-butyl ether (MTBE)	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Naphthalene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		n-Butylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		n-Propylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		sec-Butylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Styrene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		tert-Butylbenzene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Tetrachloroethylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Toluene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Total Xylenes	ND	ug / L	1	0.5	S	01-28-02	01-28-02

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Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:15:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-07A		EPA 624.2		By: EHL						
EHL698259	TT.2002.508.1		trans-1,2-Dichloroethylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		trans-1,3-Dichloropropylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Trichloroethylene	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Trichlorofluoromethane	ND	ug / L	1	0.5	S	01-28-02	01-28-02
EHL698259	TT.2002.508.1		Vinyl chloride	ND	ug / L	1	0.2	S	01-28-02	01-28-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:49:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-08A		EPA 606		By: EHL						
EHL698260	TT.2002.513.1		Aroclor 1016	ND	ug / L	1	0.08	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Aroclor 1221	ND	ug / L	1	2	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Aroclor 1232	ND	ug / L	1	0.5	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Aroclor 1242	ND	ug / L	1	0.3	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Aroclor 1248	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Aroclor 1254	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Aroclor 1260	ND	ug / L	1	0.2	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Chlordane	ND	ug / L	1	0.1	S	01-28-02	01-30-02
EHL698260	TT.2002.513.1		Toxaphene	ND	ug / L	1	1	S	01-28-02	01-30-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:22:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-09A		EPA 531.1		By: EHL						
EHL698261	TT.2002.511.1		3-Hydroxycarbofuran	ND	ug / L	1	0.5	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Aldicarb	ND	ug / L	1	0.5	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Aldicarb Sulfone	ND	ug / L	1	0.7	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Aldicarb Sulfoxide	ND	ug / L	1	0.5	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Carbaryl	ND	ug / L	1	0.5	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Carbofuran	ND	ug / L	1	0.9	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Methomyl	ND	ug / L	1	0.5	S	01-30-02	02-02-02
EHL698261	TT.2002.511.1		Oxamyl (Vydate)	ND	ug / L	1	1	S	01-30-02	02-02-02

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Order: **0201283 RAN03** Receipt: **01-23-02**

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:00:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-10A		1613B						By: TLI		
TL158481	TT.2002.424.2		2,3,7,8-TCDD	ND	pg / L	1	3	S	01-30-02	02-04-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:00:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-11A		EPA 626.2						By: EHL		
EHL698282	TT.2002.510.1		Alachlor (Lasso)	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Aldrin	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		alpha-Chlordane	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Atrazine	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Benzo(a)pyrene	ND	ug / L	1	0.02	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Butachlor	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Di(2-ethylhexyl)adipate	ND	ug / L	1	0.6	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Di(2-ethylhexyl)phthalate	ND	ug / L	1	0.6	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Dieldrin	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Endrin	ND	ug / L	1	0.01	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		gamma-Chlordane	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Heptachlor	ND	ug / L	1	0.04	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Heptachlor epoxide	ND	ug / L	1	0.02	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Hexachlorobenzene	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Hexachlorocyclopentadiene	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Lindane (gamma-BHC)	ND	ug / L	1	0.02	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Methoxychlor	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Metolachlor (Dual)	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Metribuzin (Sencor)	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Propachlor	ND	ug / L	1	0.1	S	01-28-02	02-04-02
EHL698282	TT.2002.510.1		Simazine	ND	ug / L	1	0.07	S	01-28-02	02-04-02

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:55:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-12A		EPA 336.4						By: EHL		
EHL698283	TT.2002.509.1		Cyanide	ND	mg / L	1	0.02	S	02-01-02	02-01-02

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Sample: **CDPROD1/ RANCHO VIEJO** Collected: **01-23-02 12:55:00** By: **CWC**
 Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-13A		EPA 648.2						By: EHL		
EHL999264	TT.2002.515.1		Diquat	ND	ug / L	1	0.4	S	01-28-02	01-28-02

Sample: **CDPROD1/ RANCHO VIEJO** Collected: **01-23-02 12:56:00** By: **CWC**
 Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-14A		EPA 425.1						By: ROE		
W026	MW.2002.128.3		Surfactants	ND	mg / L	1	0.03		01-29-02	01-29-02

Sample: **CDPROD1/ RANCHO VIEJO** Collected: **01-23-02 12:58:00** By: **CWC**
 Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-16A		EPA 100.2						By: JM		
QL2010TA078617	TT.2002.412.1		Amphibole	ND	MFL	1	0.151	S	01-30-02	01-30-02
QL2010TA078617	TT.2002.412.1		Chrysotile	ND	MFL	1	0.151	S	01-30-02	01-30-02
QL2010TA078617	TT.2002.412.1		Total Asbestos Fibers >= 10 um	ND	MFL	1	0.051	S	01-30-02	01-30-02

Sample: **CDPROD1/ RANCHO VIEJO** Collected: **01-23-02 12:58:00** By: **CWC**
 Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
0201283-16A		EPA 200.8 ICP-MS						By: C.J		
M0287	MW.2002.188.30	7428-80-5	Aluminum	0.014	mg / L	1	0.01		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-38-0	Antimony	ND	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-38-2	Arsenic	0.010	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-39-3	Barium	0.117	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.210.4	7440-41-7	Beryllium	ND	mg / L	1	0.001		01-25-02	02-12-02
M0287	MW.2002.188.30	7440-43-9	Cadmium	ND	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-47-3	Chromium	0.005	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-50-8	Copper	0.004	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7439-89-6	Iron	0.070	mg / L	1	0.01		01-25-02	02-11-02
M0287	MW.2002.188.30	7439-92-1	Lead	ND	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7439-98-5	Manganese	0.005	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-02-0	Nickel	ND	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7782-49-2	Selenium	ND	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-22-4	Silver	ND	mg / L	1	0.001		01-25-02	02-11-02
M0287	MW.2002.188.30	7440-28-0	Thallium	ND	mg / L	1	0.001		01-25-02	02-11-02

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Order: **0201283 RAN03** Receipt: **01-23-02**

Sample: **CDPROD1/RANCHO VIEJO**

Collected: **01-23-02 12:55:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
EPA 200.8 ICP-MS By: CJ										
0201283-16A	MW.2002.188.30	7440-89-8	Zinc	0.011	mg / L	1	0.005	B	01-25-02	02-11-02
EPA 245.1 CVAA By: je										
0201283-16A	MW.2002.138.25	7438-87-8	Mercury	ND	mg / L	1	0.0002		01-30-02	01-30-02
EPA 4.1.3/200.7 ICP By: SKD										
0201283-16A	MW.2002.125.49	7440-70-2	Calcium	11.0	mg / L	1	0.4		01-25-02	01-28-02
0201283-16A	MW.2002.125.49	7439-95-4	Magnesium	0.8	mg / L	1	0.1		01-25-02	01-28-02
0201283-16A	MW.2002.125.49	7440-23-5	Sodium	49.7	mg / L	1	0.2		01-25-02	01-28-02
SM 2340B By: MAJ										
0201283-16A	TT.2002.352.1		Hardness, as CaCO3	31	mg / L	1	0		02-06-02	02-06-02

Sample: **CDPROD1/RANCHO VIEJO**

Collected: **01-23-02 12:10:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
EPA 140.1 By: DH										
0201283-18A	TT.2002.243.2		Odor	No Odor Observed	TON	1	1		01-24-02	01-24-02

Sample: **CDPROD1/RANCHO VIEJO**

Collected: **01-23-02 12:58:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	Code	Prep Date	Run Date
EPA 150.1 By: DH										
0201283-19A	TT.2002.244.1		pH	8.7	units	1	0.1		01-24-02	01-24-02
EPA 180.1 By: NL										
0201283-19A	TT.2002.278.3		Total Dissolved Solids	182	mg / L	1	10		01-25-02	01-25-02
EPA 180.1 By: DH										
0201283-19A	TT.2002.240.2		Turbidity	1.0	NTU	1	0.3		01-24-02	01-24-02
EPA 300.0 By: SEF										
0201283-19A	MW.2002.131.35	18887-00-8	Chloride	2.64	mg / L	10	0.05		01-24-02	01-25-02
0201283-19A	MW.2002.131.35	18984-48-8	Fluoride	ND	mg / L	10	0.05		01-24-02	01-25-02
0201283-19A	MW.2002.131.35	14787-86-0	Nitrate, as N	ND	mg / L	10	0.05		01-24-02	01-25-02
0201283-19A	MW.2002.131.35	14787-56-8	Nitrite, as N	ND	mg / L	10	0.05		01-24-02	01-25-02
0201283-19A	MW.2002.131.35		Sulfate	12.2	mg / L	10	0.05		01-24-02	01-25-02
EPA 310.1 By: DH										
0201283-19A	TT.2002.344.2		Alkalinity, Total	113	mg / L	1	2		02-05-02	02-05-02

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Client: **BALLEAU GROUNDWATER**

Project:

Order: **0201283 RAN03** Receipt: **01-23-02**

Sample: **CDPROD1/ RANCHO VIEJO**

Collected: **01-23-02 12:58:00** By: **CWC**

Matrix: **AQ**

QC Group	Run Sequence	CAS #	Analyte	Result	Units	Dilution Factor	Detection Limit	By:	Code	Prep Date	Run Date
0201283-19A		SM 2120B						DH			
COL022	TT.2002.242.2		Color	ND	APHA	1	5			01-24-02	01-24-02
0201283-19A		SM 2330B						MAJ			
LANG	TT.2002.353.1		Langlier Saturation Index	0.25	N/A	1	0			02-06-02	02-06-02

Unless otherwise noted, all samples were received in acceptable condition and all sampling was performed by client or client representative. Sample result of ND indicates Not Detected, ie result is less than the sample specific Detection Limit. Sample specific Detection Limit is determined by multiplying the sample Dilution Factor by the listed Reporting Detection Limit. All results relate only to the items tested. Any miscellaneous workorder information or remarks will appear below.

APPENDIX H

**BALLEAU GROUNDWATER, INC. TECHNICAL MEMORANDUM
SIMULATION OF A ONE YEAR AQUIFER WITHDRAWAL
AND INJECTION TEST SOUTH OF SANTA FE, NEW MEXICO**

TECHNICAL MEMORANDUM

To File RANCHO VIEJO/WATER PLAN

November 6, 2007

From Dave M. Romero and Steven E. Silver

Subject SIMULATION OF A ONE-YEAR AQUIFER WITHDRAWAL AND INJECTION TEST SOUTH OF SANTA FE, NEW MEXICO

Introduction

On behalf of Rancho Viejo de Santa Fe, Inc. (Rancho Viejo), Balleau Groundwater, Inc. (BGW) designed, monitored and interpreted an aquifer-recharge demonstration project in Santa Fe County, New Mexico. The project is part of and is partly funded by Governor Richardson's Water Innovation Fund. The work involved investigating the six-month feasibility of injecting water into the Tesuque Formation aquifer by withdrawing 50 gallons per minute (gpm) from a production well and routing the water one mile away to an injection well. During the six-month test and subsequent six months of recovery, water levels were monitored at the production well site, at the injection well site and at several deep and shallow outlying wells. This technical memorandum describes a hydrogeologic model of the observed water-level response during the one-year monitoring period (August 2006 to September 2007). The project location is south of Interstate 25 near the end of Richards Avenue in the Santa Fe Embayment of the Española Basin (Kelley, 1978), as shown on Figure 1.

Purpose and Scope

This injection work was done on the joint behalf of Governor Richardson's Water Innovation Fund and Rancho Viejo to provide information on the feasibility of injecting water into the Tesuque Formation aquifer for an extended period in which the potential for well clogging could be tested, and the aquifer response could be examined. The model is nominated GOVRVInject07. The model files are available at the BGW website



<http://balleau.com/results.php?category=tools>). This memorandum describes a numerical model of the groundwater flow system that integrates available MODFLOW-2000 (Harbaugh and others, 2000) modeling techniques and geohydrologic data with data and results from previous studies. The objectives of the model are to (1) integrate the geohydrologic structure of the Santa Fe Embayment to better understand how the structure affects water-level response to groundwater withdrawal and injection, (2) simulate the observed water-level changes during the test, and (3) provide a modeling tool that describes a structure and parameterization of the hydrology of the Tesuque Formation aquifer at a local and sub-regional scale for use in long-term projections of water injection operations.

Previous Work

Hearne (1980) developed a model of the same aquifer to simulate a multi-well, multi-layer aquifer test conducted at the Pueblo of Tesuque. His three-dimensional digital model was calibrated using data from the aquifer test. The orientation of the Hearne model layers incorporated the dipping-bed structure of the Tesuque Formation and local-scale features identified from geophysical log data. The model area was within the Pojoaque River Basin approximately 12 miles north of the groundwater injection demonstration site described herein. That model was based on the program code developed by Posson and others (1980).

Hearne's aquifer-test model result was used in later regional modeling and has been converted to the MODFLOW program.

Others have studied and analyzed the hydrogeology of the Santa Fe Embayment area of the Española Basin (Hearne and Koopman, 1974; Hearne, 1985; McAda and Wasiolek, 1988; Frenzel, 1995; Core, 1996; BGW, 1997; John Shomaker & Associates, 1998; Keating and others, 1998; and Keating and others, 2003). Each of those studies focused on different areas of the Española Basin, but captured the geohydrology on a regional scale.

The analysis herein takes an approach similar to that of Hearne (1980 and 1985) for multi-well pump-test analysis, in that it incorporates the regional dipping bed structure of the Tesuque Formation while taking into account local-scale features derived from interpretation of geophysical data and lithologic logs in the wells drilled for the injection test, and others in the

area. The model uses the latest capabilities of the U.S. Geological Survey (USGS) model MODFLOW-2000 (Harbaugh and others, 2000).

Hydrologic Setting

Major tributaries of the local surface water system include the Santa Fe River and its Arroyo Hondo, La Cienega and Bonanza Creek tributaries, all of which flow intermittently from the mountain front until reaching an area near La Cienega where water-table springs perennially provide flow. The Santa Fe River then flows generally west toward the Rio Grande at Cochiti Reservoir. The water-bearing formations of the Santa Fe Embayment area include the Tesuque and Ancha Formations of the Santa Fe Group and alluvial units adjacent to perennial streams and springs (Spiegel and Baldwin, 1963, p. 38). The primary water-bearing unit is the Tesuque Formation with a thickness of about 2,000 feet at the test site in comparison to a few hundred feet of saturated where Ancha Formation and tens of feet of saturated alluvium. Along perennial streams there are tens of feet of saturated alluvium. The deeper units represented in the model are principally Espinazo and Galisteo Formations.

The springs in the La Cienega area act as a drain that discharges groundwater from the aquifer system. Groundwater generally moves southwest toward the springs and eventually toward the Rio Grande. The bedding structure and hydraulic properties of the Tesuque Formation affect the direction of groundwater flow and the hydraulic gradient of the groundwater system. The Tesuque Formation consists of inter-bedded deposits of sediments with contrasting permeability. The beds have a dip that creates a preferential pathway for groundwater flow; the ability of the formation to transmit water parallel to the beds is much greater than its ability to transmit water across the beds (Hearne, 1980). That condition creates steep hydraulic gradients in the Tesuque Formation (50 to more than 100 feet per mile) where the movement of water is across, rather than parallel to, the dipping beds (Spiegel and Baldwin, 1963, pgs. 131-132).

In the area of Agua Fria, there is a flattening of head gradient that has been mapped by Spiegel and Baldwin (1963, Plate 6) and by Johnson and others (2004, Plate 5). That flattening is consistent with the movement of water parallel to, rather than across, the dipping geologic

beds as the strike of the beds wraps around the Santa Fe Embayment as mapped by Kelley (1978) and by Grauch and Bankey (2003) at the structural base of the Santa Fe Group. Subcrop of an identifiable clay sequence and fault structure also contribute to the hydraulic-gradient pattern.

The pumping and injection wells used during the one-year test are completed in the lower 1,400 feet of the Tesuque Formation aquifer. The hydrologic properties and structure of the lower Tesuque Formation aquifer are, therefore, expected to be the dominant factor that influences water-level response during the test. The field test program is described in BGW (2001 and 2002) and BGW (2007 a, b, c and d). Field conditions provide the rate, response and well geometries for the simulation described herein.

Model Development

The model is used for analyzing data collected during the six-month injection test plus six-month recovery phase. Four components are developed: (1) a hydrogeologic framework, (2) a spatial grid, (3), a test pre-condition and (4) matching of observed data to the model response. Each of these components is described below.

Hydrogeologic Framework

We compiled data to provide information for the construction of a three-dimensional hydrogeologic unit solids model. The solids model provides a framework for specifying hydrologic parameter zones within the groundwater flow model and provides a basis for using the Hydrogeologic Unit Flow (HUF) Package that works with MODFLOW-2000 (Anderman and Hill, 2003).

The first step involved compiling data from Johnson and others (2004), Phillips (2004), Read and others (2004) and Sawyer and Minor (2006) to define the elevation of the Base of the Santa Fe Group (BSFG). The areas between data points were then interpolated to create a surface representative of the BSFG. This surface provided datum upon which shallower hydrogeologic units are constructed.

This model was constructed based on cross sections by Read and others (2004) and lithologic interpretations by Hawley (2006).¹ Above the BSFG, the solid model includes Hawley's lower (LSF), middle (MSF) and upper (USF) Santa Fe Group. Johnson and others (2004) provided a contour map of the base of the Ancha Formation (USF). We then used the land surface to define the top of the solids model above the BSFG. Along the southern edge of the Santa Fe Embayment, we used data from Grant (1998) to define the Tesuque subcrop extent beneath the Ancha Formation (USF).

At the injection test site, the solids model was defined by local structure interpreted by Hawley (2006) and Hawley and Cook (2003) based on test site drilling program data. The middle Santa Fe Group is divided into 13 separate units to capture the hydrostratigraphic unit interpretation as described below.

Below the BSFG, we constructed a hydrogeologic unit representing pre-Santa Fe Group bedrock units. We defined the unit to be about 3,250 feet thick representing basement rock including Espinazo Formation, Galisteo Formation, and Mesozoic and Paleozoic rock units near the Sangre de Cristo and Cerrillos uplifts. Volcanic rocks are also represented where they outcrop near Cerillos and the Caja del Rio.

Spatial Grid

The groundwater system is represented by a grid with 40 layers, 186 rows and 186 columns. The grid covers an area of 245-square miles and ranges in thickness from 3,000- to 8,500-feet thick. As shown on Figure 1, the model grid is oriented north. In plan view, the model grid is constructed out of cells that vary in size from squares 100 feet on a side (in the area where groundwater levels are influenced by the test) to cells constructed from squares 1,000 feet long on a side. Model grid cells are 100 feet thick in the areas where water levels are influenced by the one-year test.

¹ Dr. John Hawley of Hawley Geomatters, Inc. interpreted lithologic samples from the wells at the production and injection sites and characterized the geology of the test site (Hawley, 2006; Hawley and Cook, 2003).

The layer structure follows the idea of a dipping grid conceived by Hearne (1985). Hearne's grid represented the Tesuque Formation by incorporating geologic dip in the model grid layers. The grid developed for the model herein incorporates the dip as defined by the previously described BSFG. The grid was constructed based on this surface so that its layer structure would approximate the geologic dip of bedding (Figure 2).

Pre-Test Condition

The one-year injection test took place under years 2006 and 2007 conditions of the hydrologic system. The current hydrologic condition in the model area is one that has been altered from a natural setting by groundwater development over the past 60 years or so. The model is set up to account for current conditions so that the pre-test setting is suitable for simulation of the one-year period. Simulation of the pre-test setting integrates a specification of observed groundwater heads and specified aquifer properties.

We developed a current water-level map to specify observed heads on the boundary of the model grid in the regional groundwater system and along arroyo and aquifer channels where groundwater flux is expected to occur. During a steady-state simulation, the specified heads produce a net inflow to the aquifer wherever recharge is required to maintain observed groundwater levels and a net outflow wherever groundwater discharge is required to maintain observed groundwater levels. Areally distributed recharge is included. This flow is converted into a specified flow and the steady-state model is rerun.

The result is a distribution of regional model-area recharge and discharge at boundary rates that integrate specified aquifer parameters with water levels observed in the field. Aquifer parameters for this run are adapted from Hearne (1985). The resulting net model flows are shown on Figure 1.

The specified flow points on Figure 1 translate to recharge along arroyo axes, the mountain front, and the Santa Fe River at a rate of 17,500 acre feet per year (AFY) or 71 AF/square mile. That rate is compatible with Anderholm (1994) who estimates 80 to 107 AF/square mile for the Santa Fe area. Groundwater flow from the model area into the Middle

Rio Grande Basin is 8,200 which is compatible with McAda and Barroll (2002, Figure 10) who estimate about 10,000 AFY. These results indicate that the simulated pre-test condition provides a match to observed water levels while groundwater flow is within the range of estimates published by others.

Model Calibration

Model specification requires an understanding of the geohydrologic parameters and processes that affect the flow system. Our concept of the local-scale details regarding groundwater flow through the Tesuque Formation is related to flow dimension derived from test analysis and to genesis of the Tesuque Formation as described by Dr. John Hawley (personal communication, Fall 2006). Dr. Hawley describes sediments to have been deposited by flow from the south to the north within the Santa Fe Embayment. Flow from south to north is expected to create channel sands within finer over-bank deposits. Deposition of Tesuque Formation sediments then buries the coarse sands to form stacked paleo-stream channels inter-bedded within the fine-grained sediments. The surface flow is expected to have meandered so that the beds of coarse sand occur at a different horizontal location and elevation consistent with Tesuque Formation deposition at a later time. The resulting sediments would be composed of inter-bedded layers of gravel, sand, silt and clay, with a general south to north axial trend of buried paleo-stream channels.

The occurrence of channeled gravels in Tesuque Formation sediments is further described by Daniel J. Koning (Johnson and others, 2004, Appendix B, pg. 3). *"In the Tesuque Formation, there is an abundance of tabular (locally broadly lenticular), very thin to thick beds of silty to clayey sand (and minor sandy silt) that generally lack channel margins. These are in addition to overbank deposits of mud, silt, and very fine- to fine-grained sand that are most common in the distal alluvial slope. Unmistakable channel deposits of fine to very coarse sand and gravel (having both ribbon and sheet geometry) are scoured into this finer sediment..."*

This local-scale axial channel description of the Tesuque Formation aquifer is further supported by analysis of the one-year test data with generalized radial flow (GRF) analytical method (Walker and Roberts, 2003) that takes into account one-dimensional flow paths, which

are conceptually compatible with ribbon-style axial channels. The analysis of water-level response indicates a localized flow dimension that is representative of preferential flow through linear channels, rather than the Theis condition of entirely radial flow (BGW, 2007).

Geophysical log data at the test site indicate the presence of a persistent low-permeability clay layer with a thickness of about 150 feet stratigraphically above the zone of injection and production as shown on Figure 3. This clay layer is present above the production and injection well completions and is expected to cap the water-level response associated with the one-year test. That clay feature was added to the model.

With these factors in mind, the calibration approach involved initial Tesuque Formation aquifer properties based on Hearne (1985): Hydraulic conductivity (K) = 1.0 feet per day, Specific Storage (S_s) = 2×10^{-6} per foot and horizontal to vertical anisotropy of 1:300. Hearne (1985) chose these properties because they represent the middle of a plausible range of values estimated from aquifer testing and from his analysis of vertical gradients. With those parameters, this model was found to under-predict the observed injection test field response. We then added some ribbon-channel, sand lens and fault feature detail to the well areas. Model parameter and sensitivity analysis was performed with the MODFLOW parameter estimation process (Hill and others, 2000). After ten iterations of altering channel features and localized properties, we arrived at a set of calibrated values as shown on Figure 4. Calibrated parameters are compatible with those calculated from the field test program described in BGW (2001; 2002 and BGW 2007 a, b, c and d). The specific zonation of features is fitted to the resolution of the field response data. The general zones of outlying trends should be understood to lump other unresolved sand, clay and structural features.

The model is intended to be further adjusted where other features or scenarios are of interest, including longer-term water injection operations.

Model Comparison with Observed Data

The production and injection wells are situated about one mile apart. At the injection well site, monitoring wells are set up at distances of about 100 feet (CCD-OWA Intermediate),

500 feet (CCD-OWB) and 2,000 feet (CCD-OWC) from the injection well and at the production site (see Figures 2 and 3 for model screen zones). The simulated and observed water-level responses from the one-year test are shown on Figures 5 through 8. The simulated curve fit to observed data and statistics are posted on each chart. They range from one foot root mean squared (RMS) error to five feet RMS error, or about ten percent of buildup and drawdown across the site. Correlation coefficients are all greater than 0.95. Less than 0.5 feet of buildup is simulated at shallow piezometers, similar to the observed response. Drawdown is observed at the CCD-X1 shallow piezometer as in the injection test (BGW, 2007).

Figure 9 contours show maximum (180 day) test buildup and drawdown contours. The horizontal anisotropy caused by the axial channel trend at the injection site is visible in the buildup contour. The build up and drawdown contours overlap because of non-contiguous screen zones between the pumping and injection sites. Faults to the west of the pumping site act as a barrier to drawdown. At 180 days 6.8 square miles of aquifer has build up greater than one foot and 3.9-square miles of aquifer has drawdown greater than one foot. Residual drawdown and buildup after about six months of recovery is shown on Figure 10. Cross sections with buildup and drawdown at six months and one year are shown on Figure 11.

GRF calculations used to match test data (BGW, 2007) show that non-radial flow with leakage characterizes the response at the injection site. The slope of the pressure derivative of a modeled aquifer response curve can be related to the apparent GRF flow dimension as described in Walker and Roberts (2003). The resulting numeric flow dimension can represent aquifer heterogeneity, variable geometry, or boundaries with values less than one (a container) and greater than three (an external source). Ideally, flow dimension $n = 1$ describes parallel flow inside a one-dimensional prism, $n = 2$ describes concentric two-dimensional radial flow (well function of Theis, 1935), and $n = 3$ is spherical three-dimensional flow to a point. Flow dimensions with values between the idealized integers are considered to contain elements of various geometries.

Figures 12 through 14 display the calculated flow dimensions and the associated build up from constant injection of 50 gpm for 180 days. At CCD-OWA a low-flow dimension is indicated for less than one day, before a radial then increasingly leaky response persists to 180

days. The average flow dimension for CCD-OWA is 2.3. High (>2.5) flow dimensions are interpreted to result from periodic transmissivity (Walker and Roberts, 2003) zones within the model area. Flow dimensions less than two indicate that less than radial flow regime persists at CCD-OWB and CCD-OWC for about 100 days before near radial then leaky responses predominate. CCD-OWB has an average flow dimension of 1.7 and CCD-OWC has an average flow dimension of 1.5.

Conclusions

1. The model (GOVRVInject07) incorporates the three-dimensional hydrogeologic structure of the Tesuque Formation aquifer. The model is capable of simulating the water-level response caused by the one-year injection test and response, and can be adapted to project the response area of future water-injection operations.
2. The model analysis supports the concept of axial paleo-stream channels inter-bedded in the Tesuque Formation sediments which improves local-scale model performance. Calibrated parameters are compatible with those calculated from the aquifer-recharge demonstration project field program data.
3. The model is calibrated to reasonably match observed data at four piezometers and the water table.

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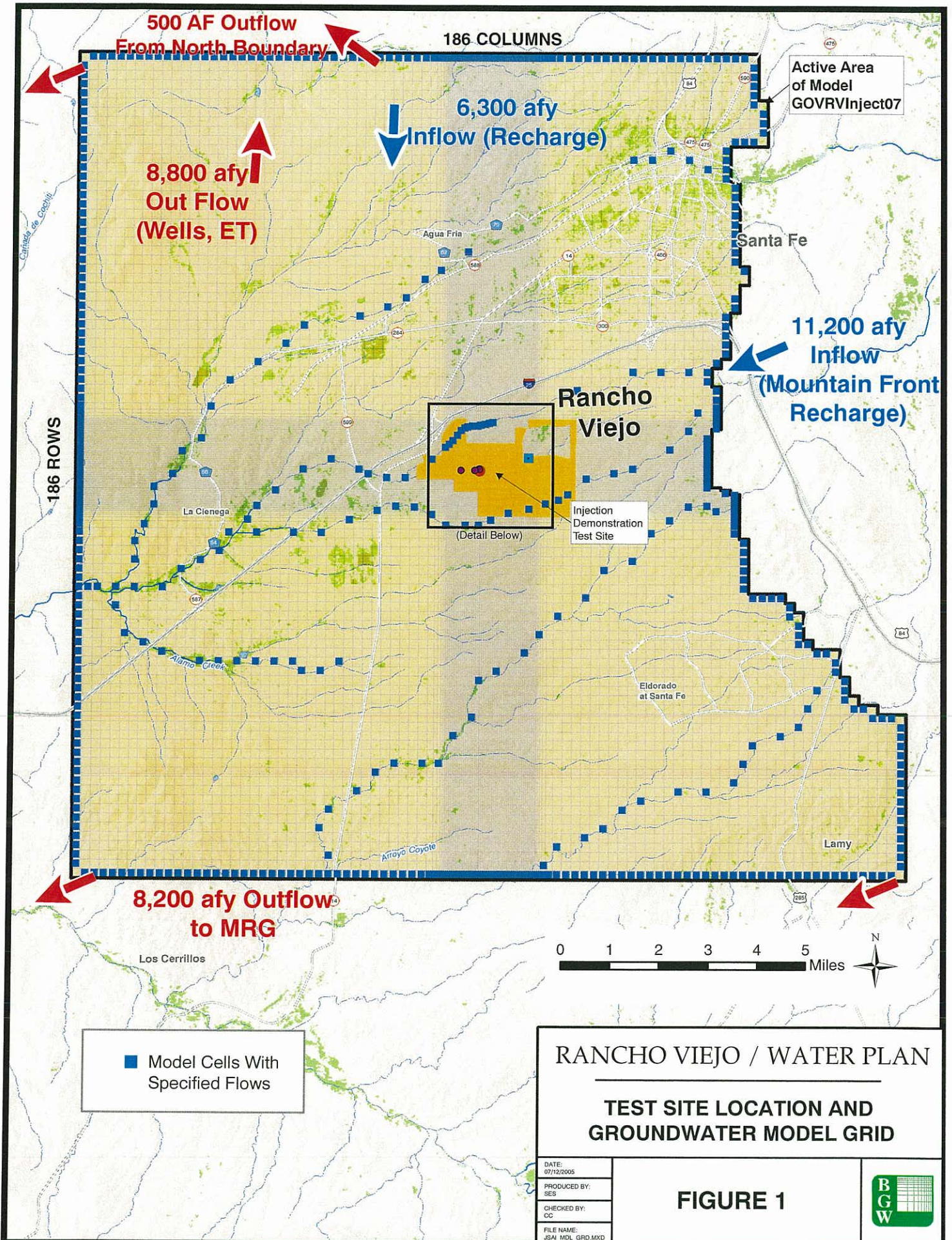
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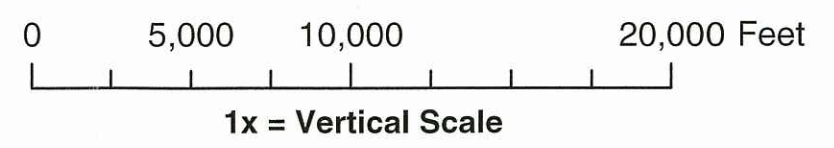
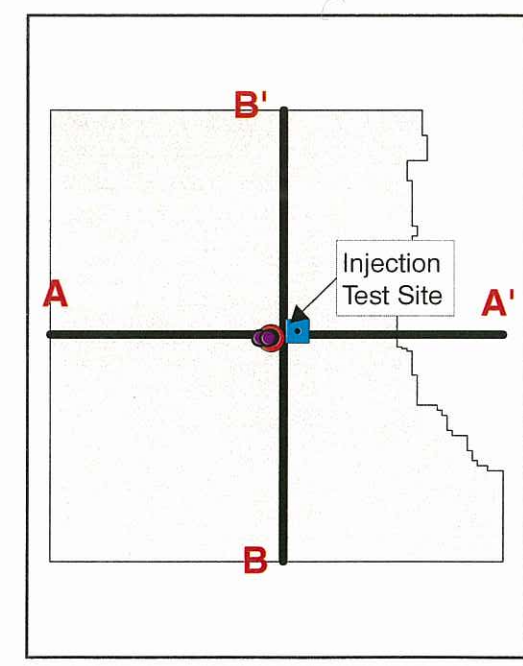
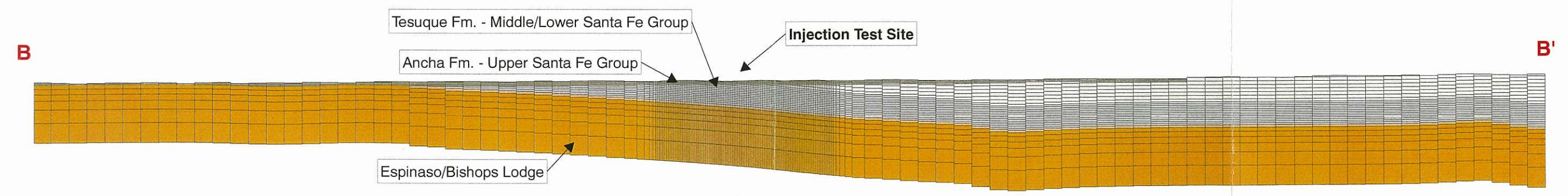
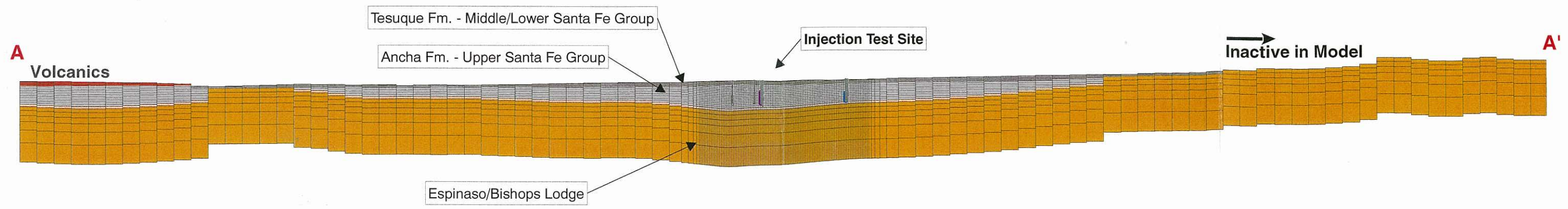
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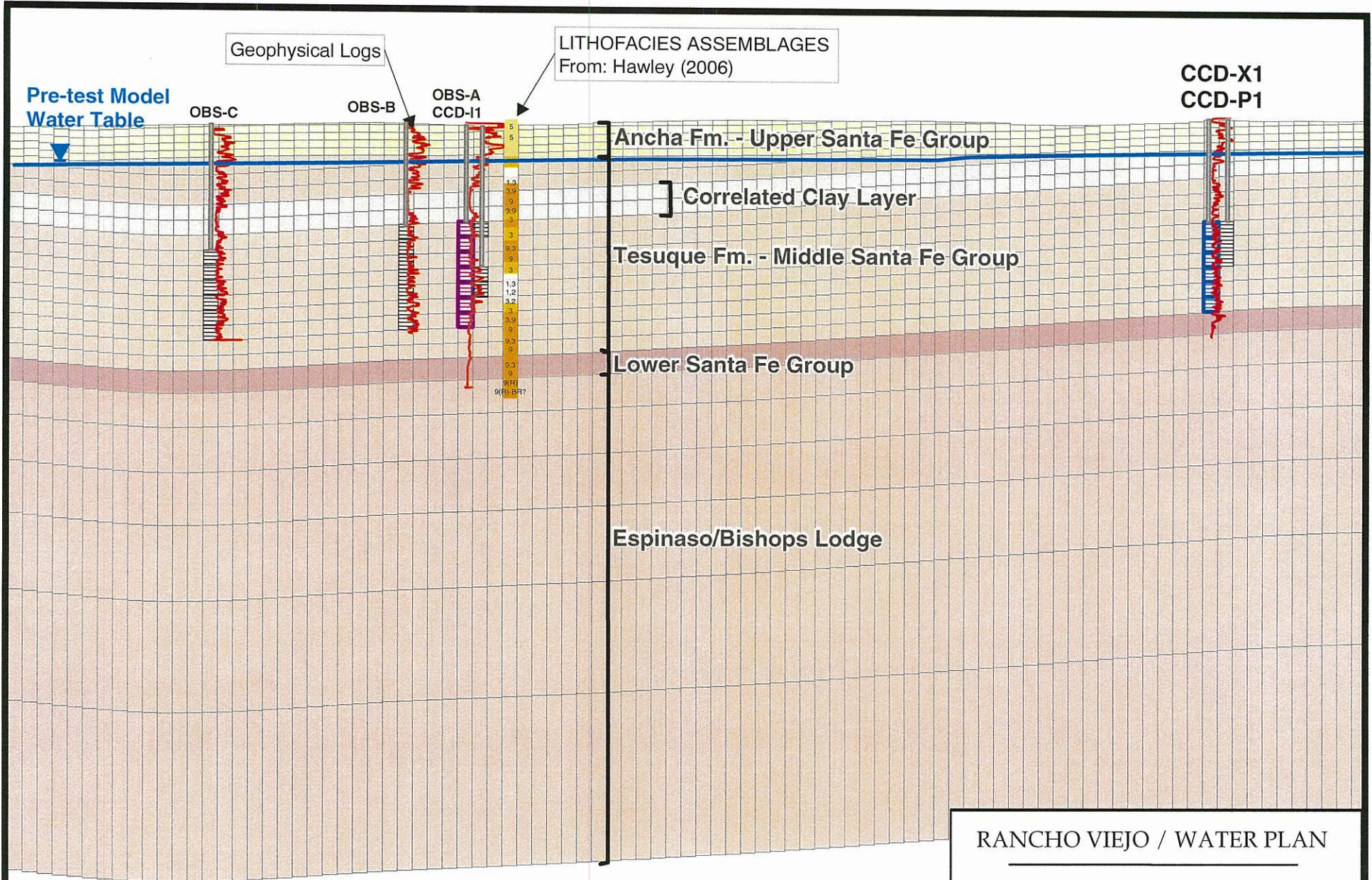
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Attachments: Figures (14)





RANCHO VIEJO / WATER PLAN	
REGIONAL MODEL CROSS SECTIONS	
DATE: 11/17/05	<p>FIGURE 2</p> 
PRODUCED BY: SES	
CHECKED BY: DB	
FILE NAME: XSEC.MXD	



Geophysical Logs

LITHOFACIES ASSEMBLAGES
From: Hawley (2006)

Pre-test Model
Water Table

OBS-C

OBS-B

OBS-A
CCD-I1

CCD-X1
CCD-P1

Ancha Fm. - Upper Santa Fe Group

Correlated Clay Layer

Tesuque Fm. - Middle Santa Fe Group

Lower Santa Fe Group

Espinaso/Bishops Lodge

0 500 1,000 2,000 Feet

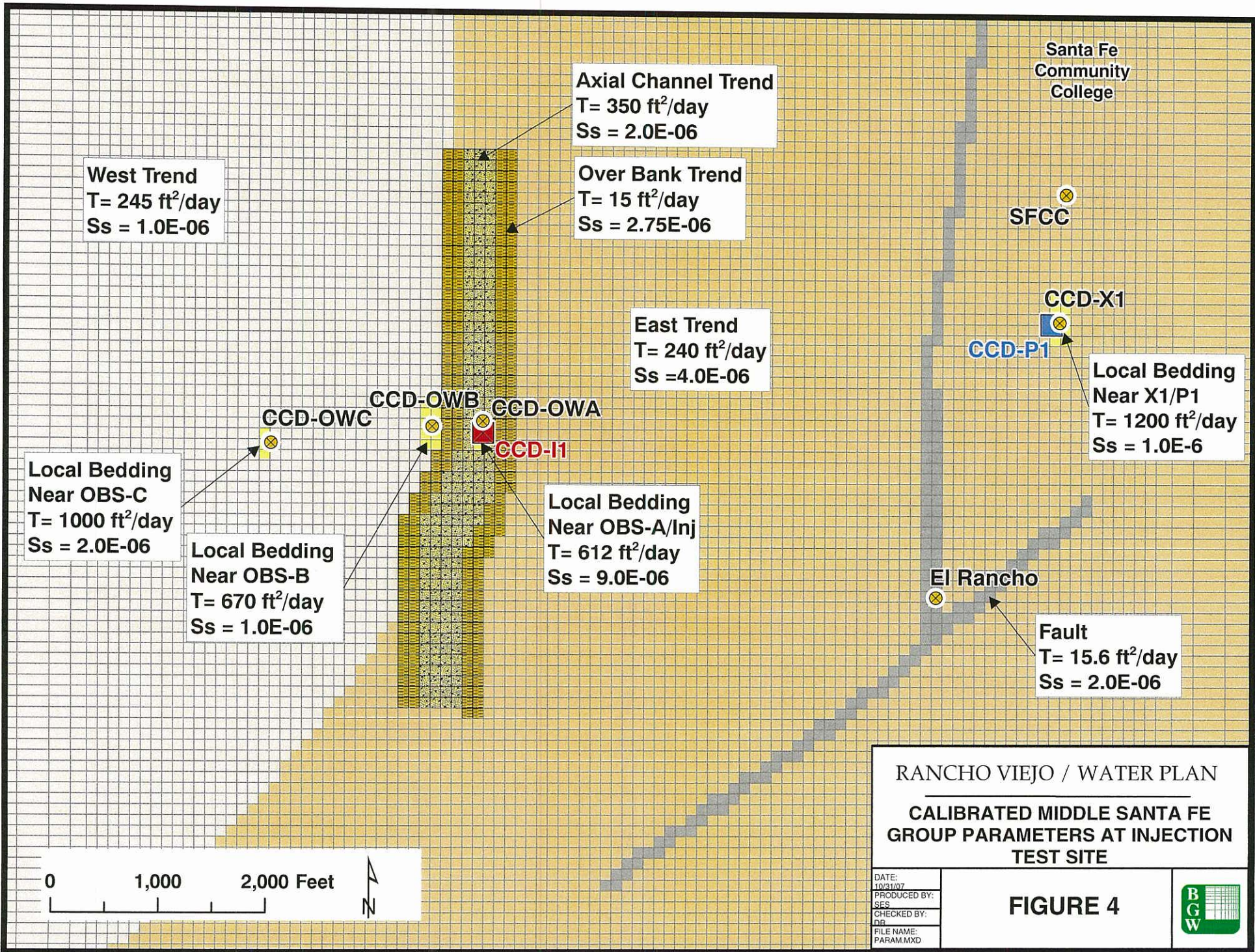
1X Vertical Scale

RANCHO VIEJO / WATER PLAN
INJECTION SITE MODEL CROSS
SECTION AND GEOPHYSICAL LOGS

DATE:
11/17/05
PRODUCED BY:
SES
CHECKED BY:
DB
FILE NAME:
XSEC.MXD

FIGURE 3





RANCHO VIEJO / WATER PLAN
CALIBRATED MIDDLE SANTA FE
GROUP PARAMETERS AT INJECTION
TEST SITE

DATE:
10/31/07
 PRODUCED BY:
SES
 CHECKED BY:
DB
 FILE NAME:
PARAM.MXD

FIGURE 4



FIGURE 5
OBSERVED AND SIMULATED BUILD-UP AT CCD-OWA

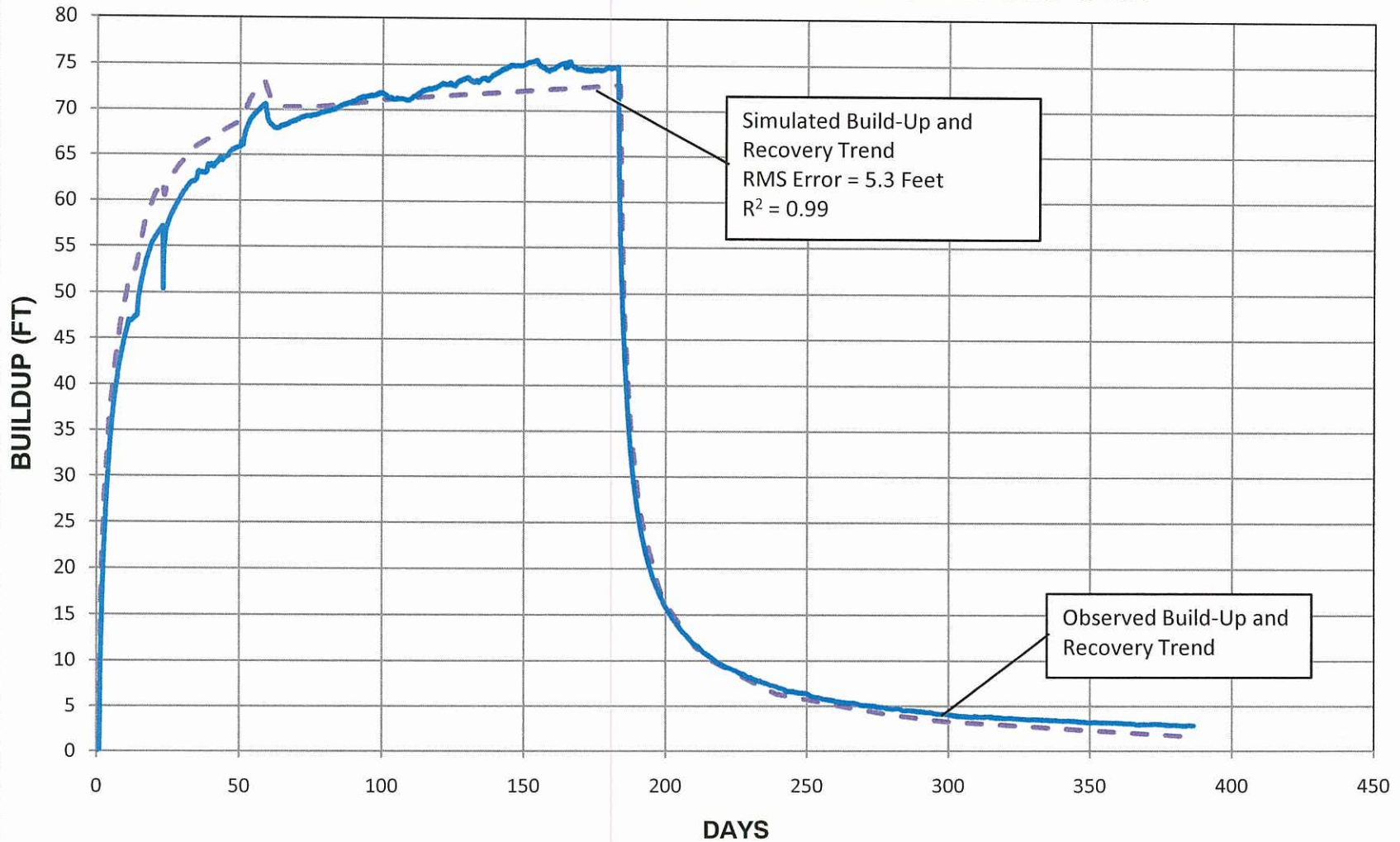


FIGURE 6
OBSERVED AND SIMULATED BUILD-UP AT CCD-OWB

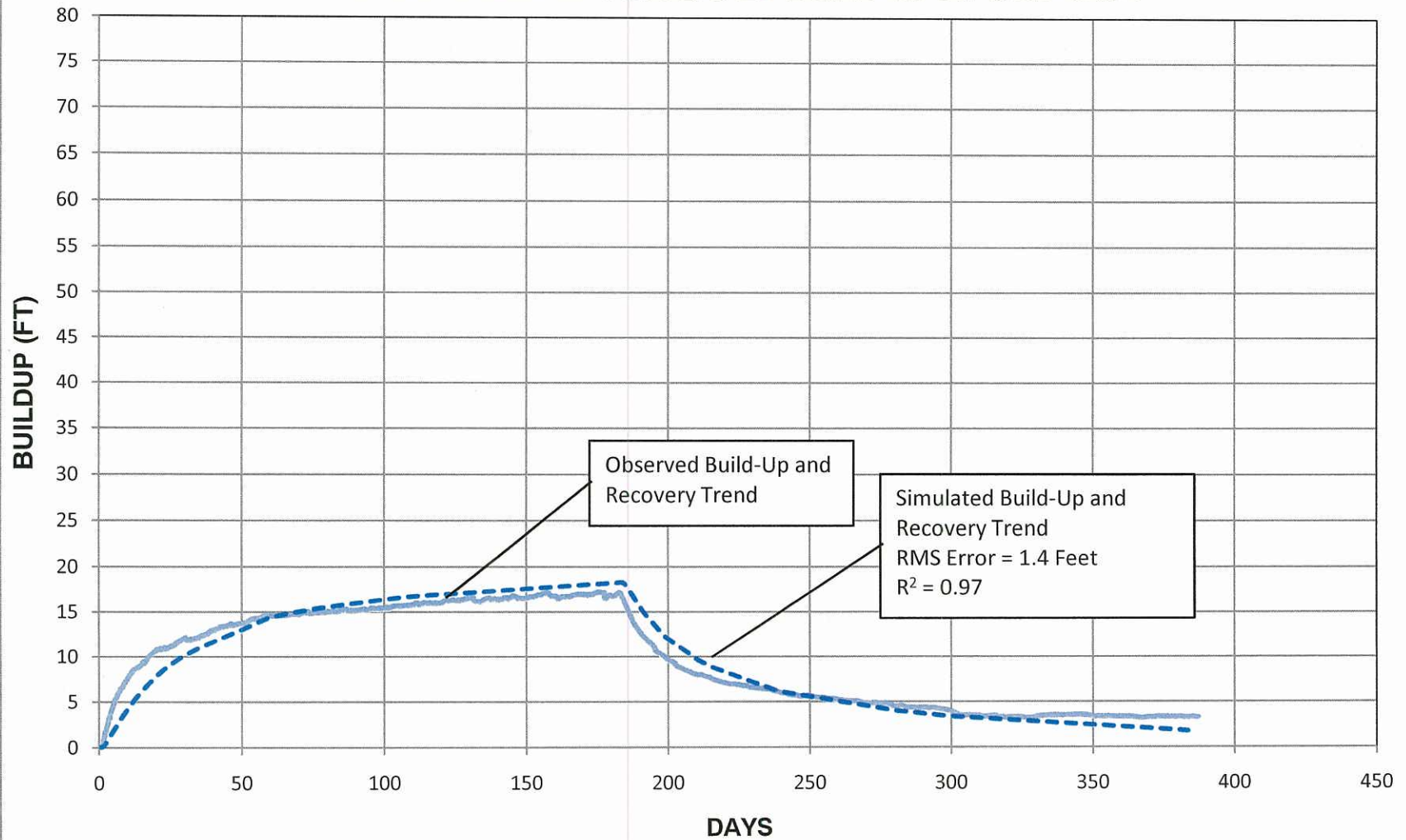
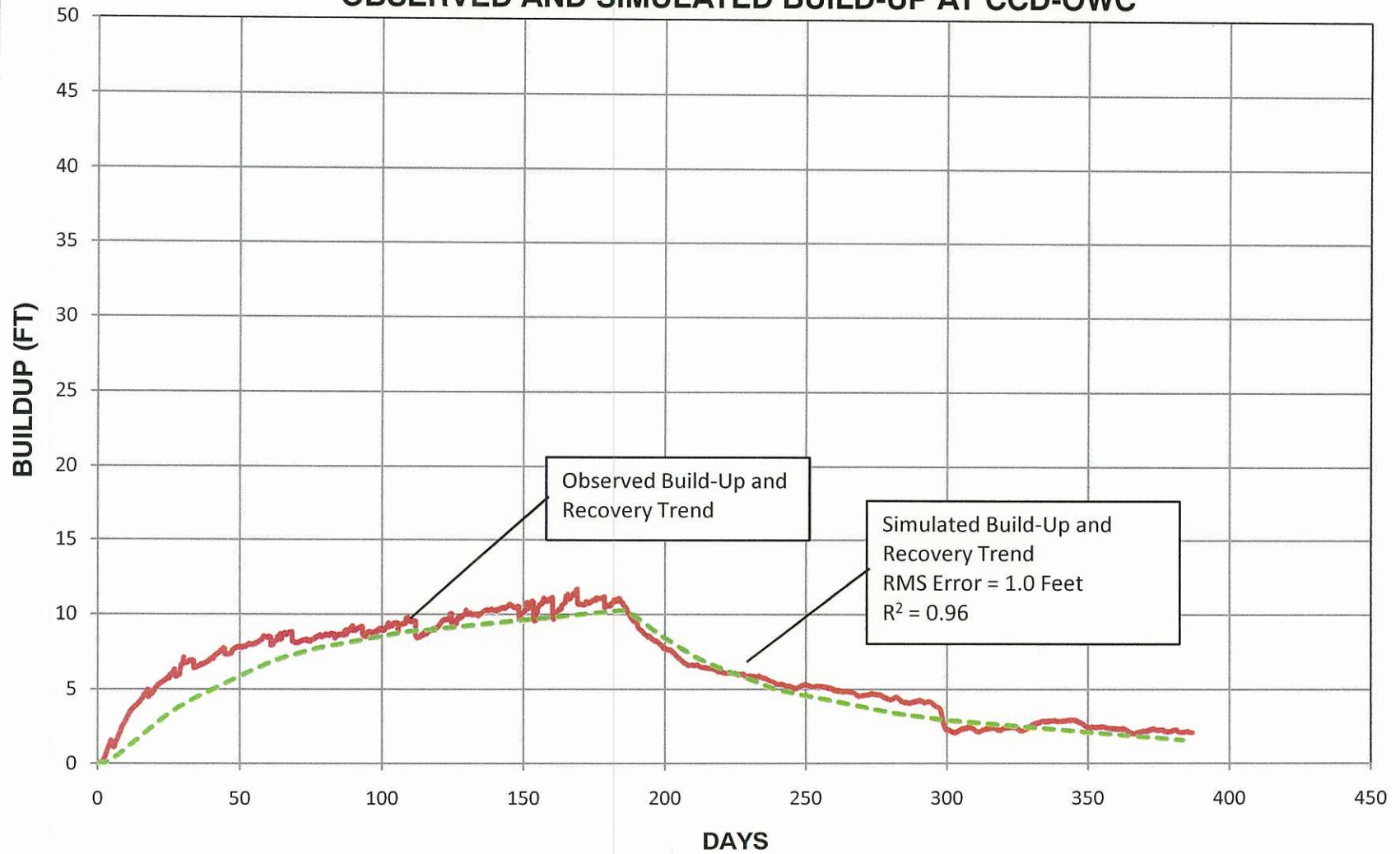
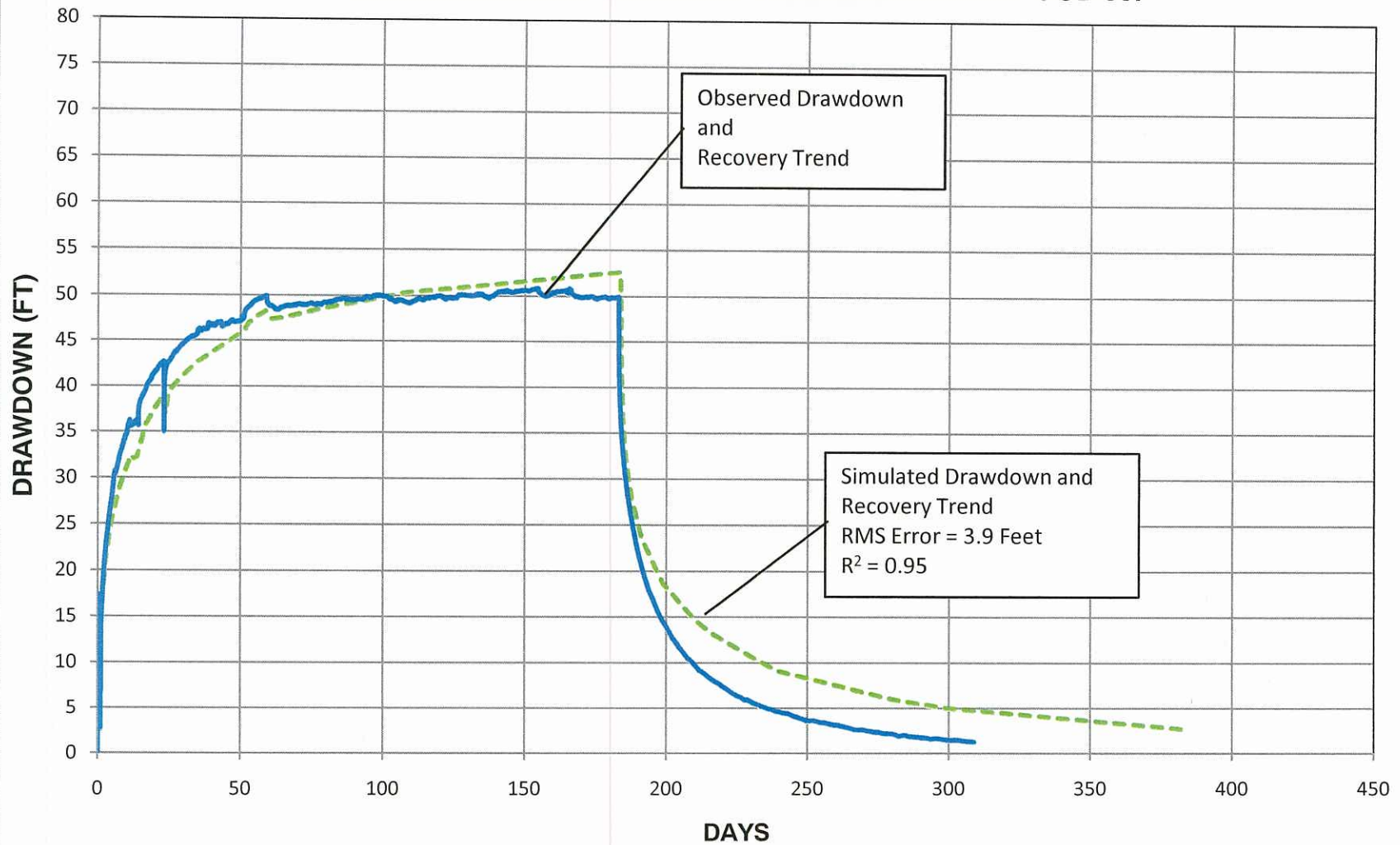


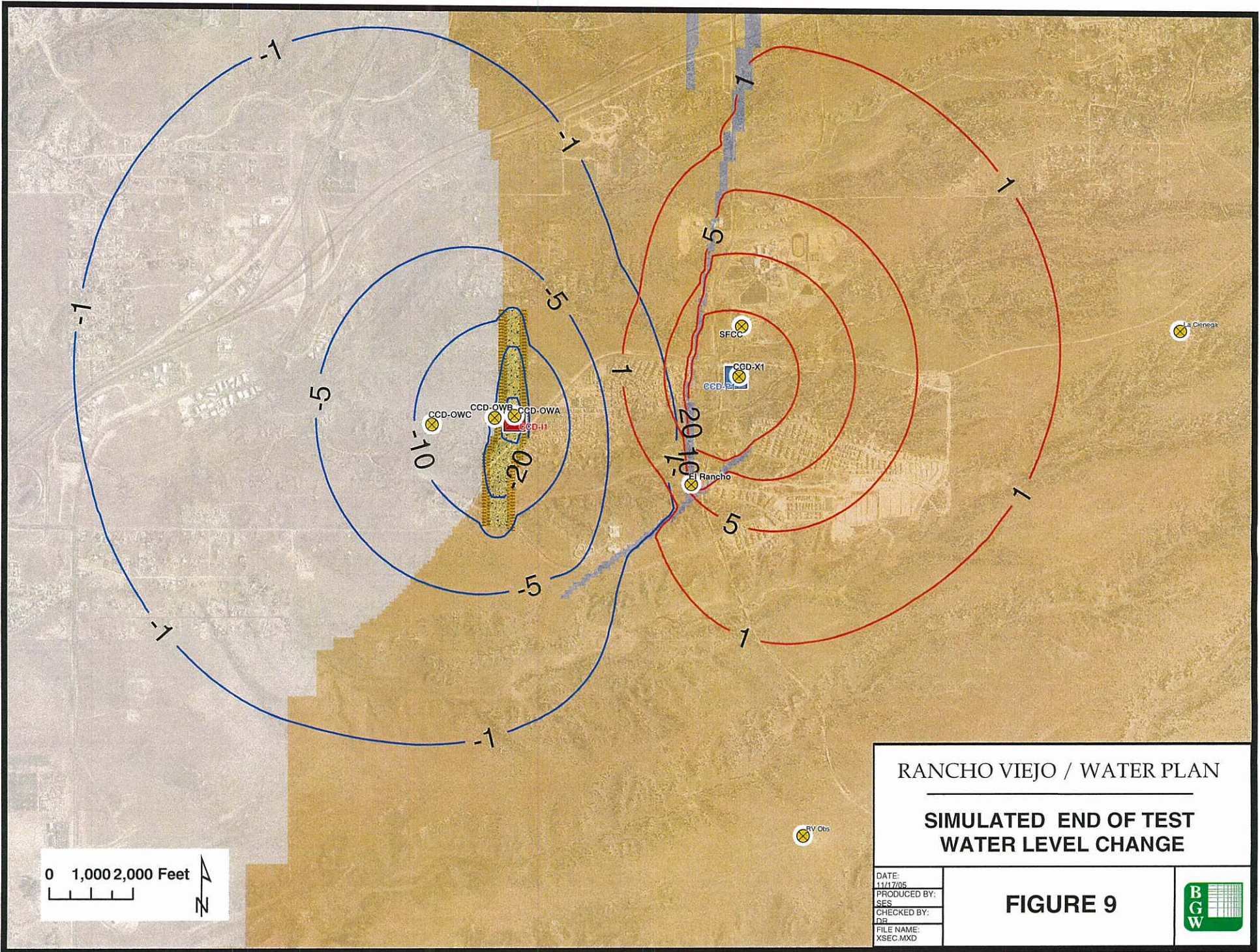
FIGURE 7
OBSERVED AND SIMULATED BUILD-UP AT CCD-OWC

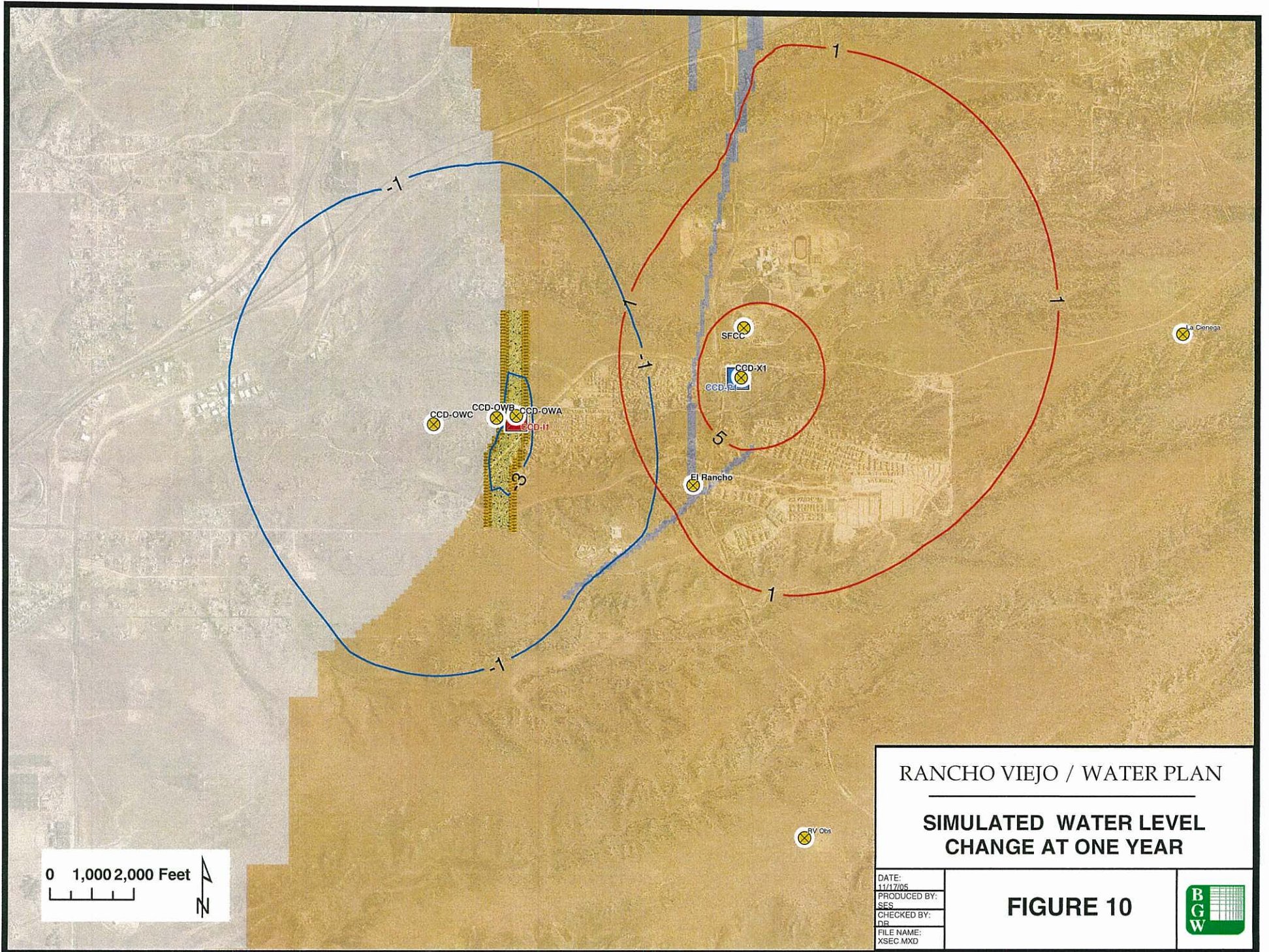


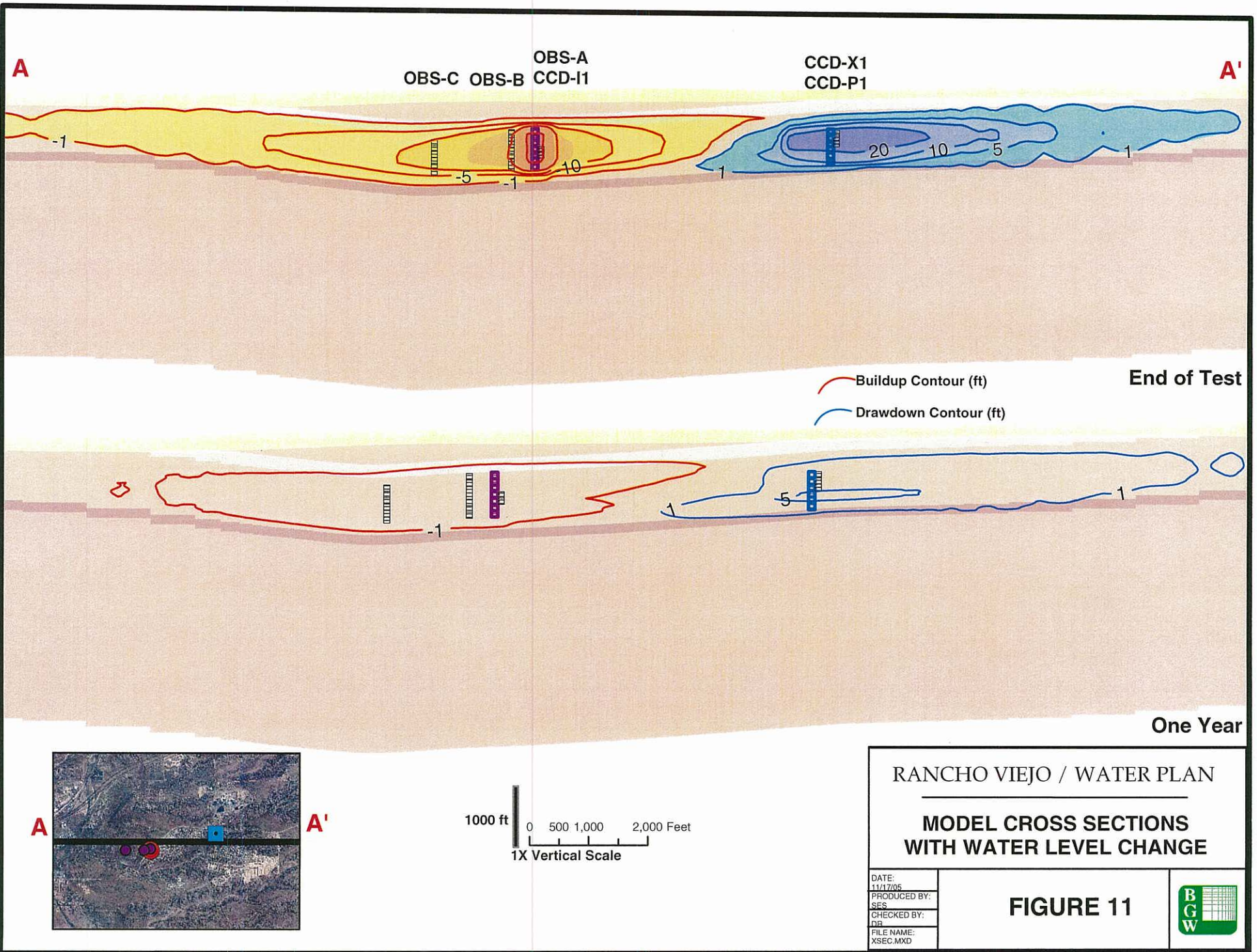
WATER PLAN

FIGURE 8
OBSERVED AND SIMULATED DRAWDOWN AT CCD-X1









RANCHO VIEJO / WATER PLAN

**MODEL CROSS SECTIONS
WITH WATER LEVEL CHANGE**

DATE:
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FIGURE 11



FIGURE 12
APPARENT FLOW DIMENSIONS FOR INJECTION TEST SIMULATION
AT OW-A

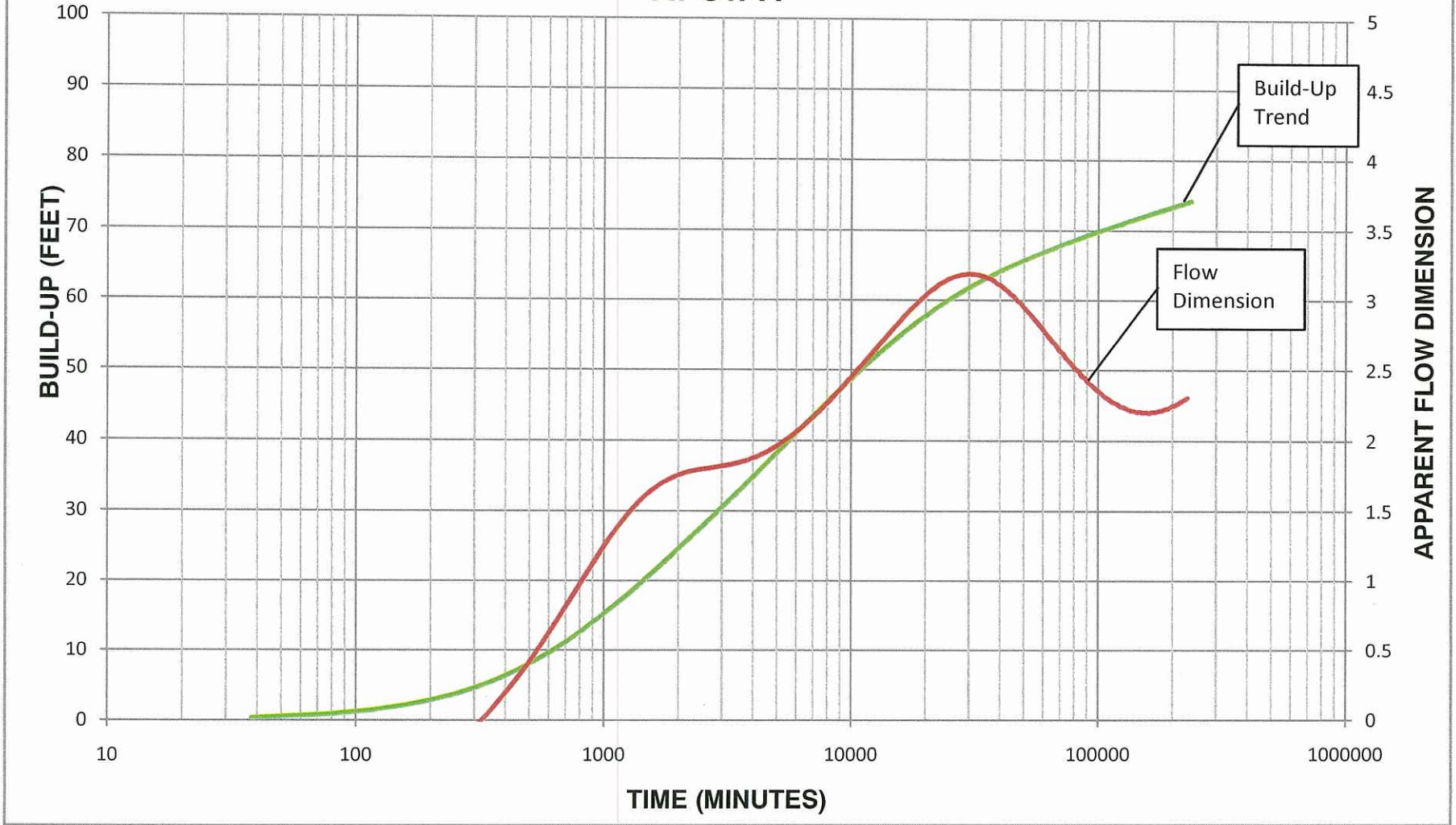


FIGURE 13
APPARENT FLOW DIMENSIONS FOR INJECTION TEST SIMULATION
AT OW-B

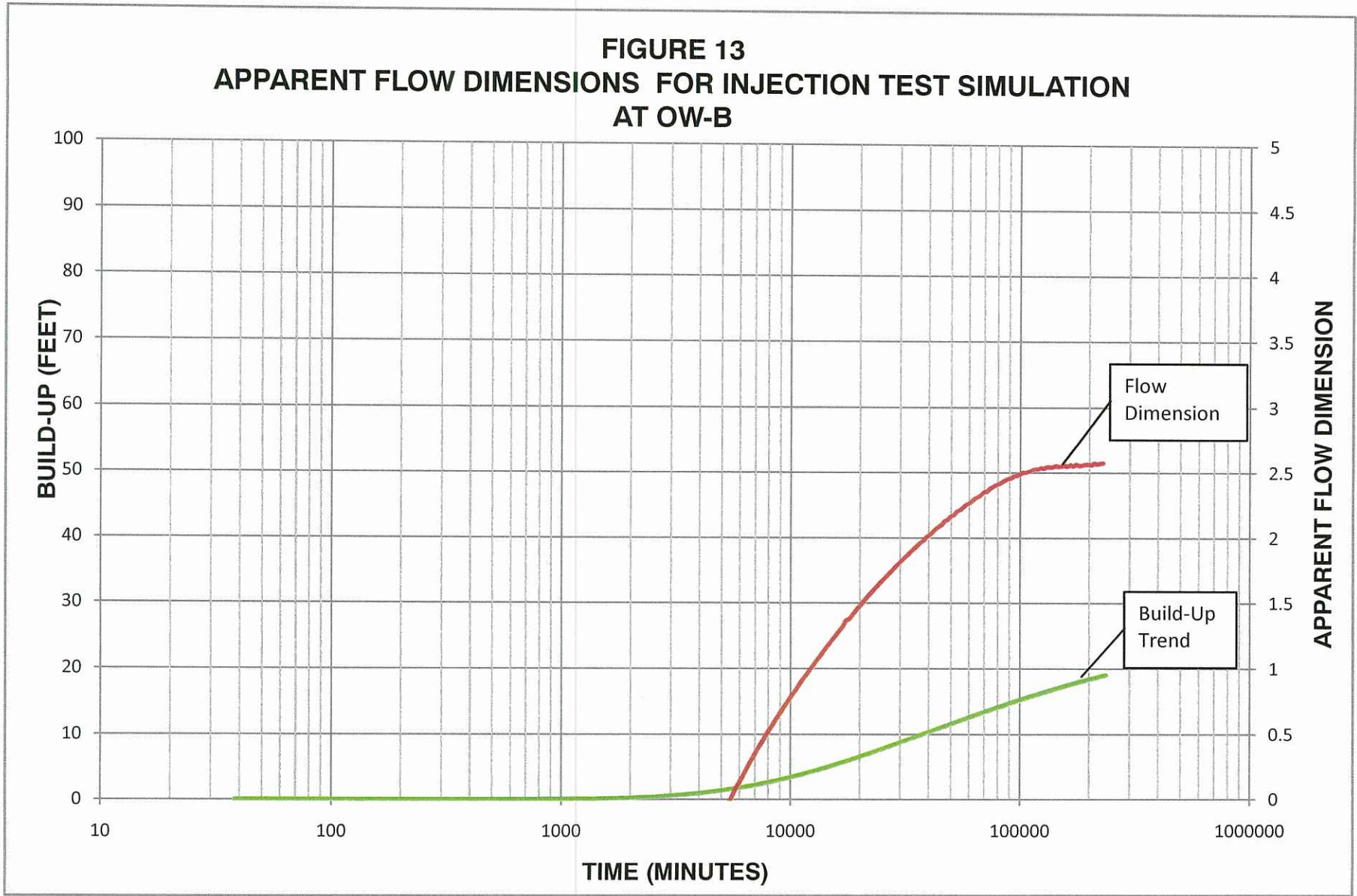


FIGURE 14
APPARENT FLOW DIMENSIONS FOR INJECTION TEST SIMULATION
AT OW-C

